DESIGN AND MANUFACTURE A PROTOTYPE OF YEMENI COFFEE HULLER MACHINE

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ABSTRACT

The design, construction and development of a huller is described in this paper. Some engineering properties were studied as important parameters affecting the design of the huller machine, and the results showed that, the highest frequency length, width and thickness of the coffee grains were 1.0, 0.7 and 0.7 cm. The medium size (from 7-10 mm) was denser than both small and large sizes of coffee as the porosity of that size was lower than those of both small and large sizes. The angle of repose increased with the decrease of coffee size. It ranged from 8.75 to 14.30 degrees on the glass surface. The huller consists basically of a drum, hopper, fan, motor, frame, belts and pulleys. It was tested at different speeds and feeding rated. The results indicated that the huller productivity increased with increasing the drum rotation speed and feeding rate. The productivity ranged from 240-360 kg/h. It could be used for hulling the coffee beans at higher rotation speeds with high efficiency.

Keyword: huller, coffee beans, peeling, productivity. <u>INTRODUCTION</u>

Peeling is an important step in the processing of most fruits and vegetables. Chemical peeling (mostly lye peeling), mechanical peeling (mainly abrasion peeling), steam peeling and freeze peeling are conventional methods for peeling in the processing of fruits and vegetables (Schlimme, Corey, & Frey, 1984; Ben-Shalom, Levi, & Pinto, 1986; Floras, Wetzstein, & Chinnan, 1987; Floras & Chinnan, 1988a, b, 1990; Bolin and Huxoll, 1991; Garrote, Coutaz, Luna, Silva, & Bertone, 1993; Setty, Vijayalakshmi, & Devi, 1993; Garrote, Coutaz, Silva, & Bertone, 1994; Bayindirli, Bayindirli, Sahin, Sumnu, & Gider, 1996; Garrote, Silva, Bertone, & Avalle, 1997). Despite providing different advantages, most of the conventional methods of peeling often cause high peeling losses and damage the flesh, affecting the quality of the fruit. Enzymatic peeling was suggested as a more recent alternative.

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Pectin, cellulose and hemi-cellulose are the polysaccharides responsible for the adherence of the peel to the fruit. Therefore, treating the fruit with the corresponding lycohydrolases provides the peeling of the fruit (Pretel, Lozano, Riquelme, & Romojaro, 1997). Since harsh treatments are not involved, the amount of broken segments and juice losses is much less than the classical methods and the peeled fruit has a better texture and appearance (Janser, 1996).

Besides the fact that there is a limited amount of work in literature regarding enzymatic peeling, almost all of these researches are about enzymatic peeling of citrus fruits (Ben-Shalom et al., 1986; Rouhana & Mannheim, 1994; Soffer & Mannheim, 1996; Pretel et al., 1997). As a result of these studies, the method was proven to be applicable and optimum peeling condition s of citrus fruits were determined. Following the researches for the enzymatic peeling of citrus fruits, trials were conducted for the enzymatic peeling of stone fruits and the feasibility of the process was shown (Janser, 1996). Better understanding of enzymatic peeling of stone fruits would probably facilitate and promote its industrial application. The objectives of this study were to investigate time–temperature–pH–enzyme concentration relations for enzymatic peeling of apricots, nectarines and peaches by using four different enzyme preparations (Peelzym I, II, III and IV) and to determine the optimum peeling conditions using response surface methodology.

Coffee is an extremely important crop in Yemen. Coffee growing started since 14th century, the Yemenis highlands can be considered as secondary center of origin of *Cafea Arabia* L (Sylvian, 1956 and Eskes and Mukred, 1989). In Yemen, coffee grows on valleys and at terraces. Coffee quality is a function of the inherent characteristics of the cultivars grown which are then modified by the influences of the environment. Bean size is the reflection on both these factors and the field husbandry practices. While the quality is already determined at harvesting and may not be subsequently improved, poor harvesting and farm processing can ruin this pre-established quality. Harvesting and farm processing have no effect on bean size.

The coffee fruit comprises the pulp which houses the parchment, surrounded by a layer of mucilage. The fruit of the Arabica coffee in which the pulp is removed from the ripe fruit by a pulping process, the mucilaging and washing processes and the parchments are dried on the estate where they are grown. The dried parchment and cherry are further processed by hulling, sorting and grading.

Many researches have been carried out on the physical and engineering properties of the agricultural products (Mohsenin, 1970; Abd Alla et al., 1995; Korayem and Soliman, 1983; Muir and Sinha, 1988; Kukelko et al., 1988; Irvine et al, 1992; and El-Raie et al., 1996). The information on size, density, and crushing strength are required for the development of the grading system for barriers and for the pulpers (Gosh, 1969). The physical properties such as size, friction angle, angle of repose, crushing strength and bulk density are important in the design of the handling system, grading and hulling (Chandrasekar and Viswanathan, 1999). Abd Alla et al. (1995) reported that the shape index and coefficient of contact surface had a high significant effect on the rupture force and broken percentage in milling process of rice grains

Surface areas of fruits are important in investigations related to spray coverage, respiration rate, light reflectance, color evaluation and heat transfer studies in heating and cooling processes (Mohsenin, 1970).

The characteristic flavor and aroma of coffee result from a combination of hundreds of chemical compounds produced by the reactions that occur during roasting. This process can be divided into three consecutive stages: (i) drying, (ii) roasting or pyrolysis and (iii) cooling. The first stage is characterized by a slow release of water and volatile substances, during the first half of processing. Bean color changes from green to yellow. Pyrolysis reactions take place during the second stage, resulting in considerable changes in both physical and chemical properties of the beans. Large quantities of CO2, water and volatile substances are released and the beans turn brown, due to sugar caramelization coupled to Maillard reactions. At this point cooling is required in order to avoid burning the coffee (Sivetz & Desrosier, 1979; Rodrigues, Borges, Franca, Oliveira, & Correa, 2003).

Roasting is a complex process from a chemistry point of view, since hundreds of chemical reactions take place simultaneously. Some examples include Maillard and Strecker reactions, degradation of proteins, polysaccharides, trigonelline and chlorogenic acids (De Maria, Trugo, Aquino Neto, Moreira, & Alviano, 1996). Sugars and trigonelline will act as aroma precursors, originating several substances (furans, pyrazines, pirroles, pyridines, etc.) that will affect both the flavor and aroma of the beverage. Thermal degradation of chlorogenic acids will result on phenolic substances that will contribute to bitterness (Clifford, 1985). Even though caffeine does not take part in any reaction, it should also contribute to bitterness, besides its known pharmacological effects (Macrae, 1985). Thus, evaluation of trigonelline, chlorogenic acids and caffeine, in both green and roasted coffee, could be of relevance in establishing coffee quality. Furthermore, a few studies have proposed the use of these substances for determination of the degree of roast (Stennert & Maier, 1996), as genotype selection criteria (Guerrero & Suárez, 2001) and for species differentiation (Martín, Pablos, & González, 1998; Ky et al., 2001). The quality of coffee is commonly evaluated according to criteria such as bean size, color, shape, processing method, crop year, flavor and presence of defects (Banks, McFadden, & Atkinson, 1999). Among those, flavor (cup quality) and presence of defects (type classification) are the most important criteria employed worldwide in coffee trading.

The high labour demand of coffee production and processing, Coffee peeling is the most labour intensive operation in coffee processing, involving tedious time-consuming manual labour. The main objective of this study was to design and manufacture a prototype of coffee huller machine which assure good quality and saving energy.

EXPERIMENTAL PROCEDURES

The coffee used in the study was obtained from a local market. The study was carried out on the most common variety namely, Esmaely. The coffee berries were cleaned manually by hand removal of all foreign matter such as stones, dirt and broken seeds. The engineering parameters of this variety were studied.

Coffee bean huller machine:

The constructional drawings of the huller is shown in fig. 1. The main parts of the huller are frame, hopper (made of iron sheet with 2mm thickness), an abrasive drum (cylindrical in shape made of stainless steel with a diameter of 17.5cm, fixed on it a blades with a thickness of 1.25 cm with total diameter of 20cm), drum case, motor, blower, air reflector and sieve (made of iron sheet thickness 0.5mm with 10mm hole diameter). The drum was fixed on a horizontal shaft supported by two ball bearings fixed over a frame size 80X60cm. The drum is rotated by means of belts and pulleys connected to 0.75 hp single phase electric motor (1450 rpm and 220 V).

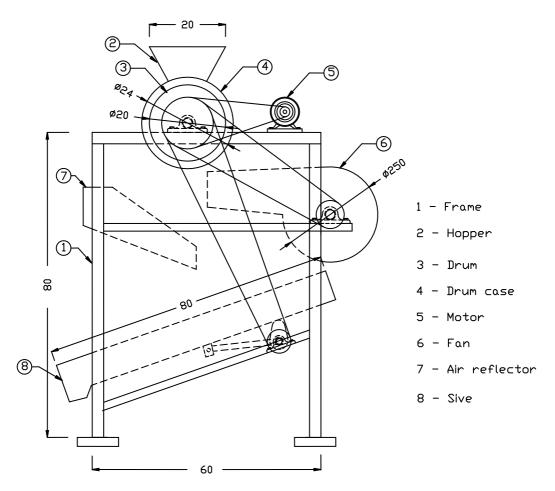


Fig. 1. Coffee bean huller machine.

The machine was set for the experiment, a sample of 4,5, 6 kg of coffee grains was weighed and fed into the machine drum, the drum was rotated at speeds of 150, 200 and 250 rpm. The speed was varied by changing the pulley of the drum shaft. Each experiment was carried out in triplicate and average values are reported:

Apparatus and Procedure Linear Dimensions:

One hundred berries were randomly selected from the remainder of the 10 kg sample. The three linear dimensions, namely, length L, width W, and thickness T, of each the 100 berries were measured with a caliper reading to 0.01 mm. The geometric mean diameter, arithmetic diameter, volume, frontal surface and cross-sectional of areas of the grains were calculated using the relationships given by **Mohsenin (1970)**, as follows:

Sphericity = 100
$$\frac{(LWT)^{0.333}}{L}$$
,% (1)

Volume =
$$\frac{\pi}{6}$$
 LWT, mm³ (2)

Geometric diameter =
$$(LWT)^{0.333}$$
, mm (3)

Arithmetic diameter =
$$\frac{(L + W + T)}{3}$$
, mm (4)

Frontal surface area
$$=\frac{\pi}{4}$$
 LW, mm² (5)

Cross - sectional of area =
$$\frac{\pi}{4} \frac{(L + W + T)^2}{3}$$
, mm² (6)

Shape Index:

Shape index is used to evaluate the shape of the coffee berries and calculated according to the following equation (**Abd Alla, 1993**):

Shape Index =
$$\frac{L}{\sqrt{W*T}}$$
 (7)

The coffee berry is considered an oval if the shape index > 1.5 on the other hand it is considered spherical if the shape index ≤ 1.5 .

Coefficient of Contact Surface:

The coefficient of contact surface is very important parameter to evaluate the contact surface between the berry and the other surfaces such as milling machine's surface. This coefficient can be calculated using the following equation (**Abd Alla, 1993**):

Coefficient of contact surface
$$= \frac{A_f - A_t}{A_f} * 100$$
 (8)

Where:

A_f is the frontal surface area $= \pi/4 * L*W$, mm² A_t is the transverse surface area $= \pi/4 * T*W$, mm²

Determination of Bulk Density of the Coffee Berries:

The bulk density of the coffee berry was measured by filling a circular container of 1L volume and weighing the contents. It was calculated from the mass and volume.

Determination of Angle of Repose

The repose angle of the three categories of the coffee varieties was determined by allowing the parchment to flow on a plate to form a pile and the angle of repose is measured by fixing a protractor on the side of the plate.

Determination of Coefficient of Static Friction:

The need for knowledge of the coefficient of friction of the agricultural materials on various surfaces has long been recognized by engineers concerned with rational design of grain bins, silos and other storage structures. Coefficient of static friction is the ratio of the force required to slide grain over a surface divided by the normal force pressing the grain against the surface. Coefficients of friction were determined for grain on four surfaces: galvanized steel, plywood, tin plate and glass. The material surface was fastened to tilting table. A frame made with square wooden bars was placed on the surface. The frame was filled with berries. The table was tilted slowly manually until movement of the whole gain mass and frame was detected by the operator. The coefficient of friction was

the tangent of the slope angle of the table measured with a protractor (**Oje** and **Ugbor**, **1991**).

RESULTS AND DISCUSSIONS

Engineering properties:

Figure 2 shows the frequency distribution of the coffee berries length, width and thickness, it can be noticed that the highest frequency distribution (30 %) was at 10 mm length.

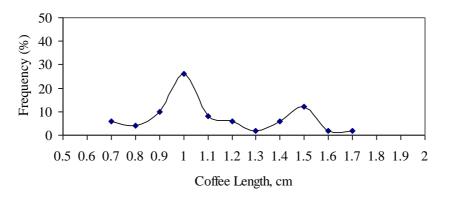


Fig. 1. Frequency distribution of coffee length (L).

Shape Index and Coefficient of Contact Surface:

The average and standard deviation of the shape index and coefficient of contact surface were estimated for the three sizes of the coffee berries of three different varieties and the data is shown in Table (1). It seems that there were no significant differences between the shape indices and coefficient of contact surface for all the coffee sizes under study.

Variet y		Shape index	Coefficient of contact surface, %				
	< 7	From 7–10	> 10	< 7	From 7–	> 10	
	mm	mm	mm	mm	10 mm	mm	
Esmae ly	1.15	1.43	1.32	16.7	33	28.6	

Table (1): Shape index and coefficient of contact surface.

It indicates also that all the coffee berries are spherical in shape according to Abd Alla (1993).

Volume, Geometric and Arithmetic Diameters, Frontal and Cross Sectional of Areas and Sphericity Percentage:

Table (2) shows the mean and standard deviation of volume, geometric and arithmetic diameters, frontal and cross sectional of areas and sphericity percentage for three categories of the coffee berries for three different varieties. The overall mean volume, geometric diameter, arithmetic diameter, frontal surface, cross-sectional of surface area, sphericity % were 138±34.7 mm³, 6.40±0.54mm, 6.42±0.56mm, 42.10±6.06mm², 112±13.58mm², and 85.7±4.28%, respectively for the small size category for all varieties. The overall mean volume, geometric diameter, arithmetic diameter, frontal surface, cross-sectional of surface area, sphericity % were 249±32.42mm³, 7.79±0.36mm, 7.90±0.36mm, 55.5±5.3mm², 147.03±13.58mm², and 80.80±1.87%, respectively for the medium size category for all varieties. The overall mean volume, geometric diameter, arithmetic diameter, frontal surface, cross-sectional of surface area, sphericity % were 772.33±109.57 mm³, 11.35±0.57mm, 11.45±0.57mm, 119.47±10.27mm², 310.73±29.96mm², and 84.27±1.49%, respectively for the large size category for all varieties.

Table (2): Volume (V), geometric mean diameter (GMD), arithmetic mean diameters (AMD), frontal surface area (A_f), cross-sectional of area (A_{cs}) and sphericity percentage of coffee berries.

Variet	V	GMD	AMD	A _f ,	A _{cs}	Sphericity		
У	(mm^3)	(mm)	(mm)	(mm^2)	(mm^2)	(%)		
Category < 7 mm								
Esmae ly	146	6.55	6.56	36.7	101	91.0		
Category from 7 – 10 mm								
Esmae ly	255	7.88	8.00	57.3	150.7	78.80		
Category > 10 mm								
Esmae ly	820	11.6	11.7	123.0	324.2	82.97		

Mass, Bulk Density and Angle of Repose:

Table (3) shows the mass of 1000 grains, bulk density and angle of repose for three diameters of coffee. It shows that the mass increased with the increase of coffee diameter for all varieties. The bulk density of the coffee berries at the three sizes were 751, 801 and 747 kg/m^3 for less than 7 mm, from 7-10 mm and more than 10 mm, respectively. It seems also that the medium size was denser than both small and large size of coffee as the porosity of that size was lower than those of both small and large sizes. This was maybe due to the smaller size has many berries were not fully ripened which make them lighter than they would be.

Table (3): Mass, bulk density and angle of repose.									
	Mass of 1000	Density	Angle of repose (°)						
	berries (g)	(kg/m^3)	Angle of Tepose ()						
	Esmaely variety								
< 7 mm	170	773	14.3						
From 7–10 mm	265	825	12.4						
> 10 mm	810	800	11.2						
Mean	415.00	799.33	12.63						
SD	345.36	26.01	1.56						

The angle of repose increased with the decrease of coffee grain size. It ranged from 8.75 to 14.3 degree on the glass surface.

1.5 Coefficient of Static Friction:

Table (4) shows the coefficient of static friction of three sizes of coffee on four different surfaces, plywood, galvanized steel, glass and tin plate for the variety under study. The results showed that the coefficient of static friction decreased with the increase of coffee grain size at all surfaces. The highest value was 0.25 for the small size and the lowest value was 0.2 for the large size. The maximum coefficient of static friction was offered by plywood surface followed by galvanized steel, tin plate, and glass for all categories of the coffee grains, these results agreed with those obtained by Helmy (1995).

	Friction Coefficient							
	< 7 mm	< 7 mm From 7–10 mm		Mean				
Surface type								
		Esmaely variety						
Plywood	0.30	0.29	0.26	0.28				
Galvanized steel	0.27	0.24	0.22	0.24				
Glass	0.25	0.22	0.20	0.22				
Tin plate	0.22	0.20	0.19	0.20				
The mass $a_{1} = a_{1} = a_{2} = a_{1} = 0.27$, 0.22 , 0.20 , $a_{2} = 1.0$, 10 , $f_{2} = 4.1$, $a_{2} = a_{2}$, $a_{1} = a_{2}$, $a_{2} = a_{2}$, $a_{2} = a_{2}$, $a_{3} = a_{3}$, $a_{4} = a_{2}$, $a_{4} = a_{4}$, a_{4}								

Table (4): Coefficient of static friction.

The mean values were 0.27, 0.22, 0.20, and 0.19 for the surfaces in the same pervious order.

Huller performance and its tests:

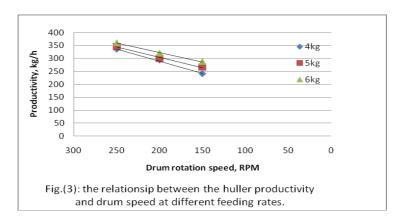
The huller was tested at different feeding rates (4, 5, and 6 kg), and rotation speeds (150, 200, and 250 rpm). Machine productivity was determined at the previous operation conditions. From Table (5), it could be seen that the productivity increased with increasing the drum rotation speed where, it recorded as high as 360 kg/h at 250 rpm rotation speed and 6 kg feeding quantity, whereas, it recorded 287 kg/h at the low rotation speed (150 rpm) at the same feeding rate (6 kg). regarding, the fractions of both grain and peels, it seems that the percentage of grain ranged from 65-70%, while peels percentage ranged from 25-35%. The results showed that there was no grain breakage during hulling process at 150 rpm rotation speed, while above these speed, the breakage percentage increased with increasing both speed and feeding rate.

Rotation speed, RPM	150			200			250		
Feeding, kg	4	5	6	4kg	5	6	4	5	6
Productivity,	240	266	287	293	300	320	335	346	360
kg/h									
Coffee	168	172	188	200	210	224	236	241	252
grain, kg									
Peels, kg	72	94	99	93	90	96	99	105	108
Breakage, %	none	none	none	0.01	0.03	0.035	0.05	0.07	0.1

Table (5): the productivity, coffee grain, peels and breakage percentage of the tested coffee beans huller machine.

Regression analysis was carried out on the relationship between the productivity (P1, P2, P3) and rotation speed, at different feeding rates (X1, 150 rpm, X2, 200 rpm, X3, 250), the best fit for this relationship was as follows:

$$P1 = 23.5(X1) + 217.3$$
 $(R^2 = 0.995)$ $P2 = 13.5(X2) + 277.3$ $(R^2 = 0.996)$ $P3 = 12.5(X3) + 322$ $(R^2 = 0.928)$



CONCLUSIONS

- The highest frequency length, width and thickness of the coffee grains were 10.0, 7.0 and 7.0 mm.
- Shape index and coefficient of contact surface revealed that the coffee grains are spherical in shape.
- The medium size (from 7-10 mm) was denser than both small and large size of coffee as the porosity of that size was lower than those of both small and large sizes.
- The angle of repose increased with the decrease of coffee size. It ranged from 8.75 to 14.3 degrees on the glass surface.
- The coefficient of static friction decreased with the increase of coffee size at all surfaces.
- The maximum coefficient of static friction was offered by plywood surface followed by galvanized steel, tin plate, and glass for all categories of the coffee grains.

- The huller productivity increased with increasing the drum rotation speed and feeding rate.
- The productivity ranged from 240-360 kg/h.
- It could be used for hulling the coffee beans at higher rotation speeds with high efficiency.
- It is recommended to be a part of a line processing of coffee hulling.
- The author recommend for further studies by establishment a research center concerning all engineering processing of coffee.

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<u>المنخص العربى</u> تصميم وتصنيع نموذج لالة تقشير البن اليمنى

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ان دراسة الخصائص الهندسية للمنتجات الزراعية له اهمية قصوى فى عمليات الاعداد والتداول وجودة المنتج وتخزين المنتجات الزراعية وكذلك فى تصميم آلات التجفيف والترطيب والنقشير وايضا عمليات الفرز والتدريج التى تسبق ذلك. من أجل ذلك كان الهدف من البحث هو تصميم وتنفيذ نموذج لتقشير البن اليمنى صنف الاسماعيلى بحيث تحافظ على الجودة وتقلل من التكاليف واستهلاك الطاقة. وتتركب الالة من خزان ، ودرفيل وموتور وبكر وسيور واطار يحمل الالة. تم اختبار الالة عند سر عات دورانية مختلفة للدرفيل عند معدلات تلقيم مختلفة. وكانت النتائج

ويمكن تلخيص النتائج المتوصل اليها في ان النسبة العظمى من الحبوب لها الطول ١٠مم ، والسمك والعرض كانوا متساويين (٧مم). معامل الشكل والتلامس يكشف ان الحبوب كروية لها نسب تلامس صغيرة. فئة الحبوب التي قطر ها من ٧-١٠ مم كانت لها كثافة اعلى من الفئتين الاقل والاعلى. ترواحت زاوية التكويم للحبوب من جميع الفئات مابين ٨.٧٥-١٤.٣٠ درجة.

الانتاجية للالة تزايدت مع زيادة سرعة دوران الدرفيل عند معدلات التلقيم المختلفة. كانت كفاءة الالة عالية جدا بحيث لم تترك اي من حبوب القهوة دون تقشير او مقشرة جزئيا. وترواحت الانتاجية بين ٢٤٠-٣٦٠ كجم/ساعة.

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