# THIN LAYER DRYING OF GARLIC SLICES USING CONVECTION AND COMBINED (CONVECTION -INFRARED) HEATING MODES

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#### ABSTRACT

Thin layer drying of garlic slices has been studied under convection and combined infrared-convection heating modes. Four levels of inlet air temperature 45, 55, 65, and 75°C and three levels of air velocity of 0.25, 0.75, and 1.25 m/s were used for the convection drying experiments. While, for the combined infrared-convection, three levels of radiation intensity of about 0.075, 0.15 and 0.225 W cm<sup>-2</sup> and three levels of air temperatures 45, 55 and 65°C were studied at inlet air velocity of 0.75 m/s. Three mathematical models (Page, Modified Page, and Henderson and Pabis) were examined for describing the drying behavior of garlic slices under the above mentioned experimental parameters. The results were compared to their goodness of fit in terms of coefficient of determination  $(R^2)$ , Standard deviation (SD), average percentage of error (% E), chi-square  $(\chi^2)$  and the modeling efficiency (EF). The results showed increases in drying rate, thermal efficiency, rehydration ratio, flavor strength, and colour difference, and showed decreases in drying time and specific energy consumption for the combined (infraredconvection) heating mode in comparison with convection only. The Page model satisfactorily described the drying behavior of garlic slices and predicted the changes in garlic slices moisture content as compared with the modified Page and the Henderson and Pabis models. Meanwhile, for the convection heating mode, the drying constant (k) increased with the

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increase of air temperature and air velocity while, the constant (n) decreased, while, for the combined mode, the drying constant (k) increased with the increase of radiation intensity and air temperature. However, the constant (n) decreased.

# **INTRODUCTION**

arlic (*Allium Sativum*) is a vegetable spice used for seasoning of foods because of its typical pungent flavor. It is usually used without any preprocessing operation. More recently, it has been used in its dried form, as an ingredient of precooked foods and instant convenience foods including sauces, gravies and soups, which led to a sharp increase in the demand of dried garlic (*Sharma and Prasad, 2006*). *Afzal and Abe (2000)* reported that air velocity during convective grain drying in thin layers has little influence (would normally increase although may not substantial) on the moisture removal rate, *Jayas and Sokhansanj (1989*). Contrary to convective drying, an increase in air velocity during far infrared (FIR) drying of barley decreased the drying rate. Increasing air velocity at a given radiation intensity resulted in lowering of kernel temperature and hence, the drying rate.

*Afzal et al.* (1999) dried barley in thin layers both under combined FIRconvection and convection alone. The experimental results show that the use of far infrared radiation enhances the drying rate and the energy consumption was reduced considerably. An intensity level of 0.333  $W/cm^2$  was found to be optimum for radiation drying. Air velocity showed a strong effect on energy consumption.

*Hebbar et al. (2004)* developed a combined infrared and hot air heating system for drying of vegetables. The system was designed to operate under infrared, hot air and combination mode independently. The performance evaluation studies indicated that combination drying of carrot and potato at 80 °C with air at a velocity of 1 m/s and temperature of 40 °C reduced the drying time by 48%, besides consuming less energy (63%) compared to hot air heating.

*Madamba et al.(1996)* investigated thin-layer drying of garlic slices (2-4 mm) for a temperature range 50-90 °C, a relative humidity range 8 - 24%, and an airflow range 0.5- 1 m/s. An analysis of variance (ANOVA) revealed that temperature and slice thickness significantly affected the

drying rate while relative humidity and airflow rate were insignificant factors during drying. Four mathematical models available in the literature were fitted to the experimental data, Page and the two-compartment models gave better predictions than the single-term exponential and Thompson's model. *Doymaz (2004)* investigated the effects of air temperature, air-flow rate and sample thickness on drying kinetics of carrot cubes. Convective air drying of carrot cubes were evaluated in a cabinet dryer. Drying was carried out at 50, 60, 65, 70 °C. Two mathematical models available in the literature were fitted to the experimental data. The Page model showed better prediction than the Henderson and Pabis model and satisfactorily described drying behaviour of carrot cubes.

The purpose of the present study was to test and to evaluate the effect of different levels of infrared radiation intensity and air velocity on drying characteristics and quality changes of thin layer garlic slices under convection and combined heating modes.

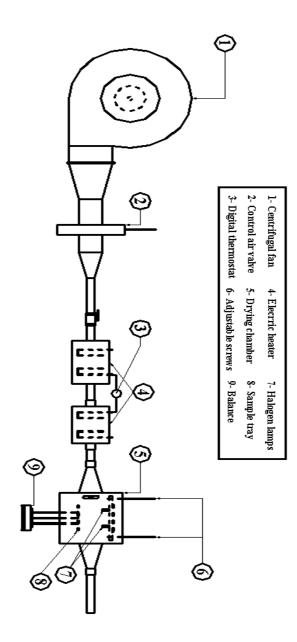
# MATERIALS AND METHODS

Freshly-harvested garlic cloves (*Allium Sativum*) used for the experimental work. The initial moisture content of the freshly harvested garlic ranged from 69 % to 72 % (wet basis) and the drying experiments for each were stopped when the final moisture content reached about 6% (w.b.).

The experimental apparatus used for the drying process is shown in Figure (1). The drying box constructed of 1.5 mm galvanized metal sheet with 40 x 28 cm cross section and 40 cm high. It was covered from inside with aluminum foil sheets. Two infrared halogen lamps (500 W) were used as a source of infrared radiation. The drying box connected with two electric heaters of 1.35 kW for each. The size of sample holding tray was 20 x 20 x 1 cm. It was placed facing the infrared lamps at a distance of 15 cm and supported on an electronic balance to enable recording the mass change of sample during the drying process.

The experiments of the convection mode were conducted at three levels of inlet air temperature (45, 55, 65, and  $75^{\circ}$ C) and three levels of air velocity which are of about (0.25, 0.75, and 1.25 m/s). However, the

Figure. (1): Schematic diagram of the experimental setup.



experiments of combined infrared-convection mode were conducted at three levels of radiation intensity of about 0.075, 0.15 and 0.225 W/cm<sup>2</sup>, three levels of air temperatures of about (45, 55 and 65°C) and constant inlet air velocity of 0.75 m s<sup>-1</sup>. The observations on mass loss changes were recorded until the product reached about 6 % (w.b) without removing the sample from the drying box. A sample size of 100 g garlic slices was used in each drying run. The peeled cloves were sliced to the desired thicknesses of ( $2.5 \pm 0.5$  mm). The mass of the samples was recorded using a digital balance with an accuracy of 0.01 g. The balance used for determining the initial and the final mass of sample, and the mass changes through out the experimental runs. The mass changes measurements were used for calculating the change of samples moisture content in wet bases. While, the initial moisture content of garlic were determined on a wet basis by the method described by A.O.AC. (1995) using a vacuum oven at 70°C and gauge pressure of 85 kPa for 24 h.

#### The Examined Drying Models for Simulating the Drying Data:

To find the most convenient drying model describing the drying behaviour of garlic slices, as shown in Table (1) the three different drying models were examined for fitting the drying data. The moisture ratio is usually expressed as (6M  $-M_e$ ) / (M $_o - M_e$ ). However, it could be simplified to  $M / M_0$ , due to the continuous fluctuation of the relative humidity of the drying under the tested drying conditions (Yaldiz and Ertekin, 2001). Also, Me value was relatively small compared to M and M<sub>0</sub> (Sacilik and Unal, 2005). Regression analysis was done by using the statistical routine. The results were compared to their goodness of fit in terms of coefficient of determination  $(R^2)$ , Standard deviation (SD), the average percentage of error (%E), Chi-square ( $\chi^2$ ) and the modeling efficiency (EF). A model is considered to be good when the correlation coefficient (R<sup>2</sup>) and modeling efficiency (EF) are higher and the standard deviation (SD), the average percentage of error (%E), chi-square ( $\chi^2$ ) are lower (Ramesh (2000). The regression analysis was also used to develop mathematical relationships between the experimental parameters and predicting the moisture content.

Model	Equation	References
Page	$MR = \exp(-kt^n)$	Page (1949)
Modified Page	$MR = \exp\left(-\left(kt\right)^n\right)$	Overhults et al. (1973)
Henderson and Pabis	$MR = a \exp(-kt)$	Henderson and Pabis (1961)

**Table** (1): The examined mathematical models used for describing the drying data.

where:

MR = Moisture ratio;

M = Moisture content, %(w.b.) at time t;

Mo = Initial moisture content at zero time, %(w.b.);

Me = Equilibrium moisture content,% (w.b.) and

K, n, a = Drying constants.

#### **Energy Requirement:**

The energy consumption during the drying process is the sum of the energy required for heating the ambient air and the net infrared energy supplied. For each experimental run the power, consumption was calculated using the following relationship (*Afazl et al., 1999*):

power = $I \times V \times PF$  .....(1). Where:

vilere.

Power = Power consumption, (W);

V = Voltage, (v);

I =Amperage, (A) and

*PF* = Power factor, assumed to be one.

The consumed energy was also related to the quantity of lost water and expressed as energy consumption rate (specific energy consumption) in MJ/kg of water.

#### **Thermal Efficiency:**

The thermal efficiency was calculated using the following relationship according to (*Reys and Jindal, 1986*)

$$E_t = \left(W_W \times \frac{Lh}{Q}\right) \times 100 \dots (2).$$

Where:

 $E_t$  = Thermal efficiency, %;  $W_W$  = Water evaporated from the product, kg; Lh = Latent heat of evaporation of water, kJ/kg; and

Q = Total energy consumption, kJ.

Latent heat of product was calculated according to the following formula (*Hall*, 1970):

Latent heat of proudct =  $1+23e^{-0.4M}$  .....(3). Latent heat of free water Where:

M = Moisture content %, (d.b.).

# **Rehydration ratio measurement:**

Rehydration ratio of the dried garlic slices was determined in triplicate. The rehydration capacity was evaluated by immersing 5 g of dried samples into 250 ml laboratory glass containing 150 ml of distilled water and then boiled for 3 min. Sample was taken out, blotted with paper towel to eliminate surface water and then reweighed (Sacilik and Unal, 2005). The rehydration ratio was calculated using equation (8).

Rehydration ratio = 
$$\left(\frac{W_t - W_d}{W_d}\right)$$
 .....(4).

where:

 $W_t$  = Weight of the rehydrated sample, (g), and  $W_d$  = Weight of the dried sample, (g).

## **Flavor strength measurement:**

The volatile oil comprising of sulfur compounds which are responsible for pungency of the garlic was determined by Chloramine-T method (Shankaranarayana et al., 1981). The volatile oils in the samples were expressed as mg oil/g dry matter.

# **Colour of the dried garlic:**

The appearance of both fresh and dehydrated slices was assessed by a colour-difference meter using a Hunter Lab Colorimeter. The colorimeter was calibrated against a standard calibration plate of a white surface with L, a, b values of 91.10 -0.64 and -0.43 respectively. (Sharma and Prasad, 2006).

Colour difference  $\Delta E$  and hue angle H were determined using the following equations:

where:  $\Delta E$  is the colour difference; H is the hue angle in degree; L<sub>0</sub>, a<sub>0</sub> and b<sub>0</sub> are the colour lightness, green-red and blue-yellow chromaticity of raw garlic; and L<sub>f</sub>, a<sub>f</sub> and b<sub>f</sub> are the colour lightness, green-red and blue-yellow chromaticity of dehydrated garlic, respectively. The raw garlic slices were used as the reference and a higher  $\Delta E$  stand for greater colour change from the reference material. The values of 0, 90, 180 and 270° for H represent red, yellow, green and blue, respectively.

#### **RESULTS AND DISCUSSION**

#### Drying behavior of garlic slices under different heating modes:

Figure (2) presents the garlic slices temperature increased with the increase of drying time. Increasing the air temperature and the air velocity tended to increase the garlic slices temperature. This is due to fast and more addition of heat to the garlic slices. At the minimum air velocity of 0.25 m/s the overall average slices temperatures during the drying process were 29.9, 38.7, 51.1 and 52.1 °C at the minimum air temperature of 45 °C, while, at the maximum air velocity of 1.25 m/s the corresponding slices temperature were 35.2, 44, 56.3 and 66.2 °C at maximum air temperature of 75 °C.

Figure (3) presents the garlic slices temperature increased with the increase of drying time. Increasing the air temperature and radiation intensity tended to increase the garlic slices temperature. At the minimum air temperature of 45 °C the overall average slices temperatures during the drying process were 74.6, 83.1 and 88.3 °C at the minimum radiation intensity of 0.075 W/cm2, while, at the maximum air temperature of 65 °C m/s the corresponding slices temperature were 86.7, 97.6 and 108.1 °C at maximum air temperature of 0.225 W/cm<sup>2</sup>.

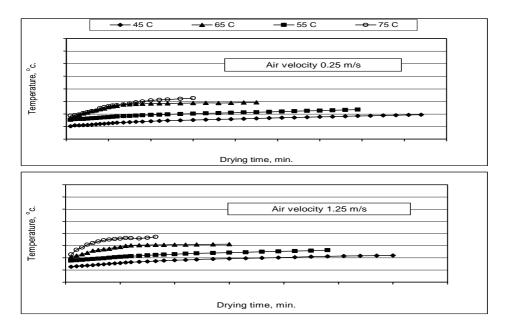


Figure (2): Slices temperature at different air temperature and air velocity.

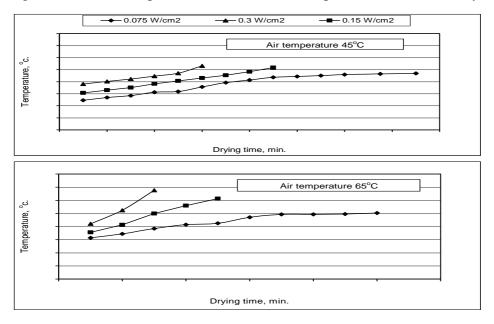


Figure (3): Slices temperature at different radiation intensity and air temperature.

Figure (4) and (5) present the change in moisture ratio of garlic slices as related to drying time for the convection and the combined heating modes. For the convection mode, the moisture ratio decreased with the increase of drying time and the reduction rate of moisture increased with the increase of drying air temperature and air velocity. However, for the combined infrared-convection mode, the moisture ratio decreased with the increase of drying time and the reduction rate was higher for the samples treated with higher radiation intensity and higher air temperature. In general, the reduction of moisture ratio was higher for the samples dried under the combined heating as compared to convection alone. For the convection drying mode, changing the air temperature from 45 to 75 °C at the minimum air velocity of 0.25 m/s decreased the drying time from 840 to 300 min. While, at the maximum air velocity of 1.25 m/s the drying time decreased from 600 to 165 min. While, for the combined heating mode at the minimum air temperature of 45 °C changing the radiation intensity from 0.075 to 0.225 W/cm<sup>2</sup> decreased the drying time from 135 to 40 min. While, at the maximum air temperature of 65 °C the drying time decreased from 100 to 25 min.

## **Evaluation of the examined drying models:**

In order to predict the changes in moisture content of garlic slices as a function of drying time, Page, modified Page and Henderson and Pabis models were examined.

To visualize the suitable mathematical expressions, the three models were linearized as follows:

 $\ln[-\ln(MR)] = \ln k + n \ln t ....(7).$   $\ln[-\ln(MR)] = n_m \ln k_m + n_m \ln t ....(8).$  $\ln(MR) = \ln a - k_h t ....(9).$ 

The multiple linear regression analysis was used to develop relationships between the parameters of each model and the drying treatments.

Drying constants of Page and the modified page models were obtained by applying linear regression analysis to the values ln(-ln(MR)) and the corresponding drying time (Equations 7 and 9). For the page model, the slope of the fitted line represented the constant (n), while the intercept represents the value of constant (k). While, for the modified page model,

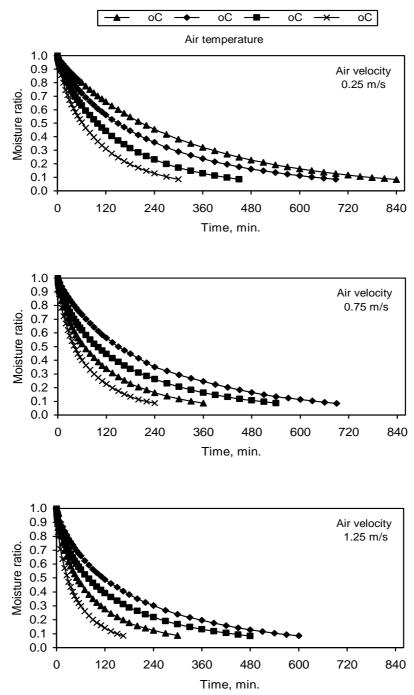


Figure (4): Moisture ratio as related to drying time for the convection mode at different air temperature and different air velocity

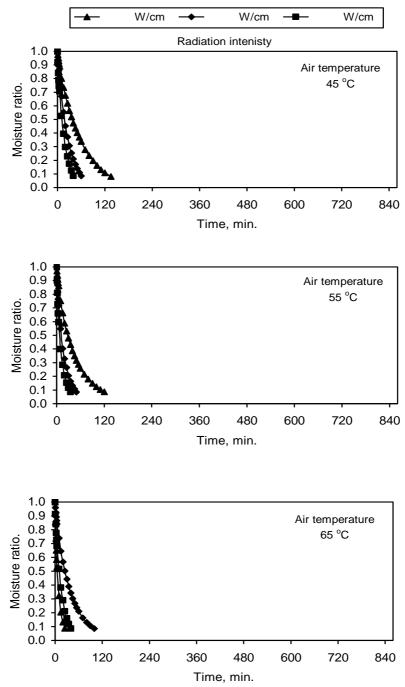


Figure (5): Moisture ratio as related to drying time for the combined mode at different radiation intensity and different air temperature.

the slope of the fitted line represented the constant  $(n_m)$ , while the intercept represents the value of the constant  $(k_m)=(n_m \ln k_m)/n_m$ .

However, the value of the drying constant of the modified Henderson and Pabis model  $(k_h)$  and (a) was obtained by applying linear regression analysis to the values ln(MR) and the corresponding drying time (Equation 9). The slope of the fitted line represented the constant  $(k_h)$ , while the intercept represents constant (a).

#### **Convection heating mode:**

The statistical analysis used for data fitting for the three models are summarized in Table 2. As shown in this table, all the studied models gave consistently high coefficient of determination ( $\mathbb{R}^2$ ) in the range 0.9887 – 0.9997. This means that all the three models could satisfactorily describe the drying behaviour of garlic slices under convection heating mode. However, among the three models, Page model showed the highest coefficient of determination ( $\mathbb{R}^2$ ) of 0.9997 and the highest modeling efficiency (EF) of 0.9998 and the lowest standard deviation (SD) of 0.0034, the lowest average percentage error (E) of 0.0144 and the lowest Chi-square ( $\chi^2$ ) of 0.000014. The experimental and predicted values of moisture ratio as related to drying time for different studied models are shown in Figure 6. As it can be seen from the figure, the Page model provided a good agreement between the experimental and the predicted data in comparison with other studied models.

On the other hand, as shown in Figures (7) and (8), the drying constants of page model (k) increased with the increase of air temperature and air velocity, while, the constant (n) decreased. A simple regression analysis was employed to relate the drying parameters with the drying constants (k) and (n). The obtained relationships were as follows:

$$k_{Page} = -0.065 + 2.47 \times 10^{-2}V + 1.22 \times 10^{-3}T \qquad (10).$$
  

$$R^{2} = 0.8968$$
  

$$n_{Page} = 1.09 - 0.115V - 3.67 \times 10^{-3}T \qquad (11).$$
  

$$R^{2} = 0.8804$$

## The combined heating mode:

The statistical analysis used for data fitting for the three models are summarized in Table (3). As shown in the table, all the studied models gave consistently high coefficient of determination ( $\mathbb{R}^2$ ) in the range of

_	constants for convection drying.									
	Drying condition			Constant and statistical parameters						
Model	Air velocity ,m/s	Temperature, °C	Radiation intensity, watt /cm <sup>2</sup>	R²	SD	E	× <sup>2</sup>	EF	n	k, min <sup>-1</sup>
	0.25	45 55 65		0.9997853 0.9998295 0.9998298	0.0025882 0.0008380 0.0033531	0.0084533 0.0028465 0.0146959	0.0000070 0.0000007 0.0000119	0.9999428 0.9999925 0.9998710	0.9255881 0.8313240 0.8166381	0.0049197 0.0107908 0.0164820
Page		75 45		0.9997416 0.9998007	0.0038900 0.0056012	0.0185861 0.0188888	0.0000161 0.0000330	0.9998199 0.9996078	0.8067868 0.8618829	0.0248300 0.0090123
	0.75	45 55 65 75	0	0.9995326 0.9995429 0.9999277	0.0030012 0.0043264 0.0021410 0.0028199	0.0180888 0.0184449 0.0097659 0.0137514	0.0000330 0.0000197 0.0000049 0.0000085	0.99997825 0.9999432 0.9999038	0.7603343 0.7307115 0.7299388	0.0210129 0.0329941 0.0454354
e	1.25	45 55 65		0.9996712 0.9994770 0.9998075	0.0047565 0.0054823 0.0028659	0.0194252 0.0245671 0.0143331	0.0000238 0.0000317 0.000088	0.9997557 0.9996425 0.9998972	0.7864004 0.7370196 0.7013631	0.0163126 0.0252208 0.0445560
		75		0.9997679	0.0020265	0.0085825	0.0000044	0.9999495	0.6963960	0.0698224
	Mean Standard dev.			0.9997 0.0001	0.0034 0.0014	0.0144 0.0058	0.000014 0.000010	0.9998 0.0001	0.7820 0.0664	0.0268 0.0179
		45	v. 	0.9997853	0.0266519	0.0818041	0.0007434	0.9939350	0.9255881	0.0032091
	0.25	55 65 75		0.9998295 0.9998298 0.9997416	0.0589156 0.0649838 0.0710750	0.2029293 0.2806055 0.3594410	0.0036325 0.0044642 0.0053884	0.9631166 0.9515457 0.9398832	0.8313240 0.8166381 0.8067868	0.0043048 0.0065565 0.0102471
Modifie	0.75	45 55 65	0	0.9998007 0.9995326 0.9995429	0.0537895 0.0892218 0.0983871	0.1912616 0.3599836 0.4898685	0.0030456 0.0083795 0.0102850	0.9638313 0.9074958 0.8800963	0.8618829 0.7603343 0.7307115	0.0042374 0.0062189 0.0093851
Modified Page	1.	75 45 55		0.9999277 0.9996712 0.9994770	0.0972086 0.0805457 0.0941003	0.5707357 0.3082185 0.4142204	0.0101245 0.0068291 0.0093468	0.8856748 0.9309007 0.8946895	0.7299388 0.7864004 0.7370196	0.0144764 0.0053335 0.0067839
	1.25	65 75		0.9998075 0.9997679	0.1083727 0.1050744	0.5985216 0.6524528	0.0125276 0.0119607	0.8530692 0.8642186	0.7013631 0.6963960	0.0118472 0.0218785
	Mean		0.9997	0.0790	0.3758	0.0072	0.9190	0.7820	0.0087	
	Standard dev.			0.0001	0.0235	0.1691	0.0036	0.0427	0.0664	0.0051
				R <sup>2</sup>	DS	E	<b>x</b> <sup>2</sup>	EF	a	k, min <sup>-1</sup>
	0.25	45 55 65	0	0.9989931 0.9946651 0.9943463	0.0176148 0.0354938 0.0344817	0.0489118 0.1065789 0.1256029	0.0003247 0.0013184 0.0012569	0.9973507 0.7304881 0.9863573	0.9587468 0.9069799 0.9064527	0.0029513 0.0035702 0.0055010
Henderson and Pabis		75 45		0.9914936 0.9947194	0.0428113 0.0373823	0.1880762 0.1187573	0.0019550 0.0014710	0.9781889 0.9825310	0.8847266 0.9144887	0.0082184 0.0035709
	0.75	55 65 75		0.9853685 0.9844187 0.9817300	0.0563904 0.0553308 0.0605539	0.1963498 0.2298779 0.3015378	0.0033472 0.0032528 0.0039287	0.9630486 0.9620781 0.9556375	0.8477484 0.8405994 0.8253387	0.0045261 0.0068038 0.0101968
	1.25	45 55 65		0.9900597 0.9891911 0.9798159	0.0501771 0.0483850 0.0609377	0.1667602 0.1761022 0.2803526	0.0026503 0.0024712 0.0039610	0.9731837 0.9723845 0.9535437	0.8702423 0.8603561 0.8192429	0.0040768 0.0051310 0.0082033
		75 Moon	L	0.9800652	0.0622891	0.3366564	0.0042033	0.9522832	0.8067418	0.0147044
	Mean Standard dev.		0.9887 0.0061	0.0468 0.0130	0.1896 0.0819	0.0025 0.0012	0.9506 0.0677	0.8701 0.0436	0.0065 0.0033	
	Standard dev.			0.0001	0.0130	0.0019	0.0012	0.0077	0.0430	0.0033

**Table(2):** Statistical results obtained from different thin layer drying models and the drying constants for convection drying.

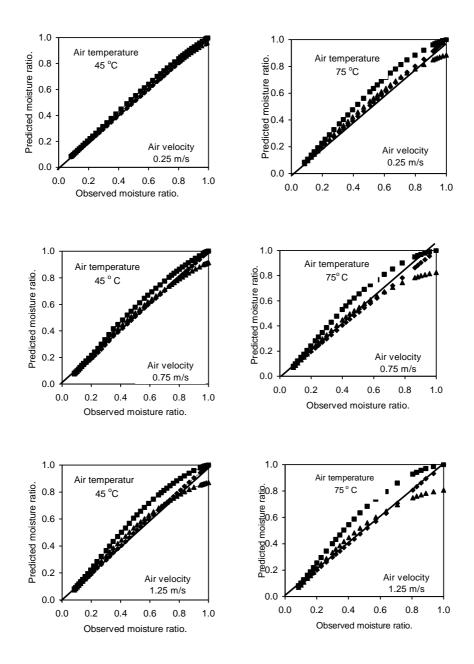


Figure (6): Observed and predicted moisture ratio of the convection heating mode for different studied models.

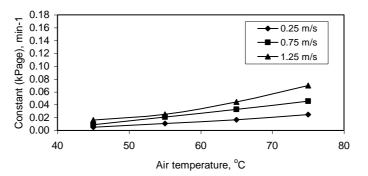


Figure (7): The drying constant (k<sub>page</sub>) as related to air temperature and air velocity.

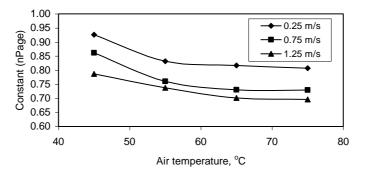


Figure (8): The drying constant (n<sub>page</sub>) as related to air temperature and

0.9972–0.9988. This means that all the models could satisfactorily describe the drying behaviour of garlic slices using the combined infrared – convection heating mode. However, among the three studied models, the Page model showed the highest coefficient of determination ( $\mathbb{R}^2$ ) of 0.9988, the highest modeling efficiency (EF) of 0.9934, the lowest standard deviation (SD) of 0.0154, the lowest average percentage of error (E) of 0.1479 and the lowest chi-square ( $\chi^2$ ) of 0.0007. Plots of the experimental and the predicted data of the moisture ratio with drying time obtained by the three models are shown in Figure (9). As it can be seen from this figure, the Page model provided a good agreement between the experimental and the predicted data in comparison with other studied models. On the other hands, as shown in Figures (10) and (11), the drying constant (k) increased with the increase of radiation intensity and air temperature while, the constant (n) decreased. A simple regression analysis was employed to relate the drying parameters with

	<b></b>	conotanto	101	combind infrared and convection drying.						
	Drying condition			Constant and statistical parameters						
Model	Air velocity ,m/s	Radiation intensity, watt /cm <sup>2</sup>	Temperature, K (°C)	R <sup>2</sup>	SD	E	× <sup>2</sup>	EF	n	k, min <sup>-1</sup>
		0.075		0.9993392	0.0194325	0.1278583	0.0004120	0.9957001	0.9159103	0.0261972
		0.15	45	0.9967611	0.0669808	0.6286754	0.0050846	0.9487650	0.8974792	0.0566806
		0.225		0.9985549	0.0090970	0.1118720	0.0000978	0.9991477	0.8822242	0.0880953
		0.075		0.9995429	0.0051748	0.0329973	0.0000293	0.9997152	0.8921305	0.0350570
Γ	0.25	0.15	55	0.9996990	0.0059530	0.0440519	0.0000409	0.9996546	0.8840292	0.0783789
Page		0.225		0.9971041	0.0120772	0.1680020	0.0001750	0.9985087	0.8658837	0.1185686
l"		0.075		0.9995723	0.0061302	0.0459524	0.0000415	0.9996030	0.8805241	0.0418994
		0.15	65	0.9991250	0.0085451	0.0917423	0.0000863	0.9992548	0.8743155	0.0936095
		0.225		0.9990771	0.0051432	0.0800022	0.0000331	0.9998257	0.8394703	0.1649085
	Mean		0.9988	0.0154	0.1479	0.0007	0.9934	0.8813	0.0782	
	St	Standard dev.		0.0010	0.0187	0.1749	0.0016	0.0158	0.0201	0.0419
		0.075		0.9993392	0.0247098	0.1793288	0.0006661	0.9933317	0.9159103	0.0187514
		0.15	45	0.9967611	0.0986544	1.0591712	0.0110304	0.9039254	0.8974792	0.0408355
		0.225		0.9985549	0.0365544	0.4671106	0.0015792	0.9774140	0.8822242	0.0636942
Mo	.0	0.075	55	0.9990827	0.0328961	0.2337016	0.0011852	0.9884900	0.8921305	0.0238150
difi	0.75	0.15		0.9996990	0.0394205	0.4268592	0.0017931	0.9848560	0.8840292	0.0561223
Modified Page		0.225		0.9971041	0.0539760	0.7152605	0.0034961	0.9702122	0.8658837	0.0852192
Pac		0.075	65	0.9995723	0.0360709	0.3078308	0.0014381	0.9862532	0.8805241	0.0272433
Je		0.15		0.9991250	0.0402945	0.5090531	0.0001902	0.9833727	0.8743155	0.0665954
		0.225		0.9990771	0.0612226	0.9646486	0.0046853	0.9577294	0.8394703	0.1168310
	Mean			0.9988 0.0010	0.0471 0.0209	0.5403 0.2939	0.0029 0.0032	0.9717 0.0260	0.8813	0.0555
	Standard dev.			0.0010 R <sup>2</sup>	0.0209 DS	0.2939 E	0.0032 x <sup>2</sup>	0.0260 EF	0.0201 a	0.0302
		0.075	45	к 0.9993807	0.0079428	0.0502113	× 0.0000688	0.9993110	a 0.9843853	<b>k, min<sup>-1</sup></b> 0.0182052
		0.075		0.9993807	0.0079428	0.1020793	0.0000888	0.9993110	0.9893929	0.0182052
Henderson and Pabis		0.13	01	0.9981857	0.0101970	0.1641015	0.0001178	0.9526025	0.9695929	0.0589130
		0.225	_	0.9960040	0.0293437	0.1937349	0.0002403	0.9908417	0.9240671	0.0204076
	0.75	0.15	55	0.9968115	0.0269167	0.0334044	0.0008360	0.9929394	0.9240071	0.0204070
	vi			0.9900113	0.0209107	0.5175501	0.0008300	0.9929394	0.8918234	0.0489899
anc		0.075		0.9986533	0.0158813	0.1004542	0.0002788	0.9973352	0.9479160	0.0247651
Pa		0.15	5 6	0.9992707	0.0180010	0.1690519	0.0003875	0.9966540	0.9475969	0.0599555
abis		0.225		0.9952887	0.0387376	0.5038120	0.0018758	0.9830769	0.8954837	0.0958163
l ″		Mean		0.9972	0.0227	0.2038	0.0008	0.9881	0.9410	0.0485
	Standard dev.		v.	0.0022	0.0117	0.1716	0.0007	0.0140	0.0328	0.0242

 Table(3): Statistical results obtained from different thin layer drying models and the drying constants for combind infrared and convection drying.

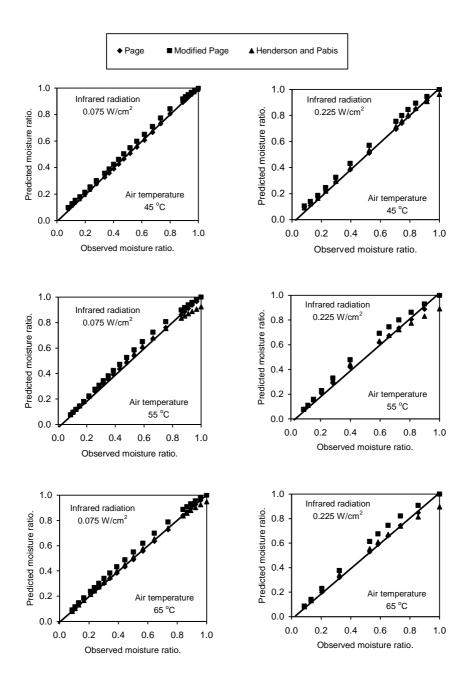


Figure (9): Observed and predicted moisture ratio of the combined heating mode for different studied models.

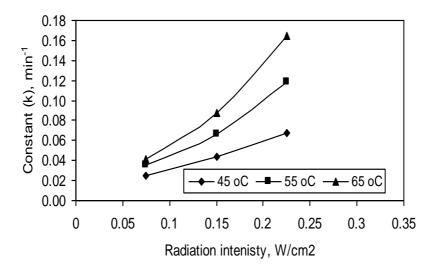


Figure (10): Drying constant (k) as related to radiation intensity and air

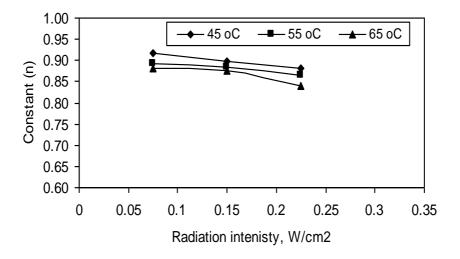


Figure (11): Drying constant (n)as related to radiation intensity and air

the drying constants (k) and (n). The obtained relationships were as follows:

 $k = -0.72 + 0.6I + 2.16 \times 10^{-3} T$ , (R<sup>2</sup>=0.9349).....(12).  $n = 1.47 - 0.224 I - 1.69 \times 10^{-3} T$ , (R<sup>2</sup> = 0.9415)....(13).

#### **Energy consumption:**

Figure (12) presents the effect of air temperature and air velocity on the specific energy consumption of the covection heating mode. As shown in the figure, the specific energy consumption decreased with the increase of air temperature and the increase of air velocity. Changing the air temperature from 45 to 75 °C at the minimum air velocity of 0.25 m/s decreased the specific energy consumption from 41.37 to 17.78 MJ/kg water. While, at the maximum air velocity of 1.25 m/s the specific energy consumption decreased from 73.8 to 50.91 MJ/kg water.

For the combined heating mode, Figure (13) shows that the specific energy consumption decreased with the increase of radiation intensity and the decrease of the air temperature. Changing the radiation intensity from 0.075 to 0.225 W/cm<sup>2</sup> at the minimum air temperature of 45 °C decreased specific energy consumption from 8.34 to 5.16 MJ/kg water. While, at the maximum air temperature of (65 °C) the specific energy consumption decreased from 14.58 to 5.37 MJ/kg water.

## **Thermal Efficiency:**

Figure (14) presents the effect of different air temperature and air velocity on the thermal efficiency of the convection heating mode. As shown in the figure, the thermal efficiency increased with the increase of air temperature and the decrease of air velocity. Changing the air temperature from 45 to 75 °C at the minimum air velocity of 0.25 m/s increased the thermal efficiency from 6.35 to 14.26 % While, at the maximum air velocity of 1.25 m/s it was increased 3.45 to 5.04 %. For the combined heating mode, Figure (15) shows that, thermal efficiency increased with the increase of radiation intensity and the decrease of air temperature.

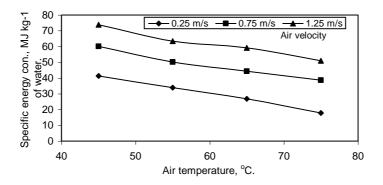


Figure (12): Effect of the air temperature on specific energy consumption of the convection mode at the different air velocity.

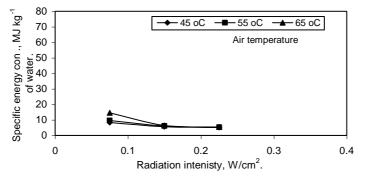


Figure (13): Effect of the radiation intenisty on specific energy consumption of the combined mode at the different air temperature.

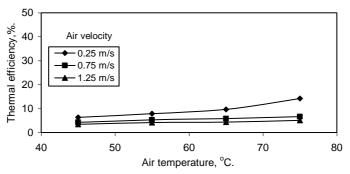


Figure (14): Effect of air temperature on the thermal efficiency of the convection mode at different air velocity.

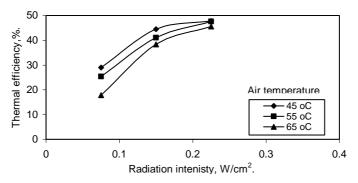


Figure (15): Effect of radiation intenisty on the thermal efficiency of the combined mode at different air temperature.

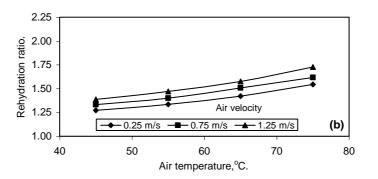


Figure (16): Effect of air temperature on the rehydration ratio of the convection mode at different air velocity.

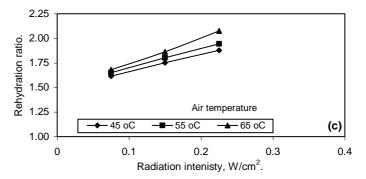


Figure (17): Effect of radiation intenisty on the rehydration ratio of the combined mode at different air temperature.

At the minimum air temperature of 45  $^{\circ}$ C changing the radiation intensity from 0.075 to 0.225 W/cm<sup>2</sup> increased the thermal efficiency from 28.97 to 47.8 %. While, at the maximum air temperature of 65  $^{\circ}$ C the thermal efficiency increased from 17.76 to 45.53 %.

# **Quality of garlic slices:**

## **Rehydration ratio:**

Figure (16) shows the effect of air temperature and air velocity on the rehydration ratio of garlic slices dried by the convection heating mode. The rehydration ratio increased by the increase of air temperature and air velocity. Changing the air temperature from 45 to 75 °C at the minimum air velocity of 0.25 m/s increased the rehydration ratio from 1.272 to 1.543. On the other hand, at the maximum air velocity of 1.25 m/s the rehydration ratio increased from 1.387 to 1.638. The increase of rehydration ratio with the increase of air temperature and air velocity may be due to less shrankage of the garlic slices. Meanwhile, for the combined heating mode, Figure (17) shows that, the rehydration ratio increased with the increase of radiation intensity and air temperature. Changing the radiation intensity from 0.075 to 0.225 W/cm<sup>2</sup> at the minimum air temperature of 45 °C increased the rehydration ratio from 1.616 to 1.879. While, at the maximum air temperature of 65 °C the rehydration ratio increased from 1.681 to 2.197.

## **Flavor strength:**

Figure (18) presents the effect of air temperature and air velocity on the flavor strength of garlic slices dried by the convection heating mode. The flavor strength increased with the increase of air temperature and the decrease of air velocity. Changing the air temperature from 45 to 75 °C at the minimum air velocity of 0.25 m/s increased the flavor strength from 3.2 to 3.51 mg/g dry matter. While, at the maximum air velocity of 1.25 m/s the flavor strength increased from 3.01 to 3.39 mg/g dry matter. Decreasing the flavor strength by the increase of air velocity, may be due to fast and more addition of heat to the garlic slices. Meanwhile, for the combined mode Figure (19) shows that, the flavor strength decreased with the increase of radiation intensity and air temperature. At the minimum air temperature of 45 °C changing the radiation intensity from 0.075 to 0.225 W/cm<sup>2</sup> decreased the flavor strength from 4.56 to 4.21

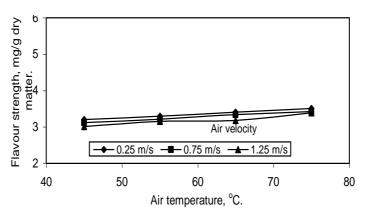


Figure (18): Effect of air temperature on the flavour strenght of garlic slices dried under the convection mode at different air velocity.

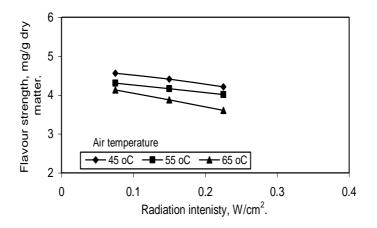


Figure (19): Effect of infrared radiation on the flavour strenght of garlic slices dried under the combined mode at different air temperature.

mg/g dry matter. While, at the maximum air temperature of 65  $^{\circ}$ C decreased the flavor strength from 4.13 to 3.61 mg/g dry matter.

# **Colour of dried garlic slices:**

Figures (20 and 21) present the effect of air temperature and air velocity on the colour difference and the hue angle of garlic slices dried by convection heating mode. The colour difference increased and the hue angle decreased by the increase of air temperature and air velocity.

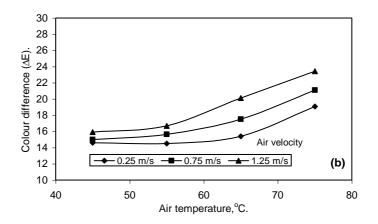
While, the colour difference increased and the hue angle decreased with the increase of radiation intensity and air temperature as shown in Figures (22 and 23).

#### CONCLUSIONS

Analysis of the results of the present research led to the following conclusions:

- 1- Drying rate, thermal efficiency, rehydration ratio, flavour strength and the colour difference were higher for the combined heating mode in comparison with the convection mode.
- 2- Drying time and specific energy consumption for the combined mode were lower than the convection mode.
- 3- Page model satisfactorily described the drying behaviour of garlic slices and predicted the changes in garlic slices moisture content.

For the combined heating mode, the drying constant (k) increased with the increase of radiation intensity and air temperature and the constant (n) decreased. While, for the convection heating mode, the drying constant (k) increased with the increase of air temperature and air velocity and the constant (n) decreased.



(20): Effect of air temperature on the colour difference at different air velocity.

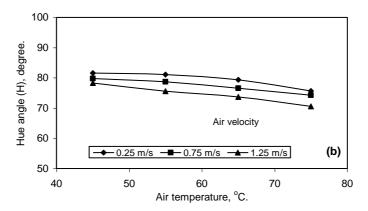


Figure (21): Effect of air temperature on the hue angle at different air velocity.

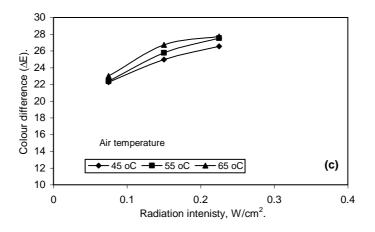


Fig. (22): Effect of infrared radiatiin on the colour difference of garlic slices dried under convection mode.

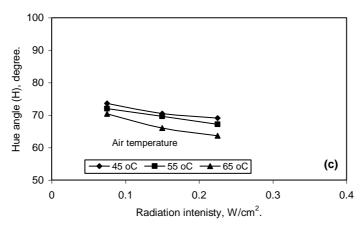


Fig. (23): Effect of radiation intenisity on the hue angle at different air temperature.

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#### الملخص العربي

اجري هذا البحث بقسم الهندسة الزراعية – كلية الزراعة- جامعة كفر الشيخ لدراسة سلوك عملية التجفيف لشرائح الثوم باستخدام طريقتين مختلفتين تمثلت في طريقة التسخين بالحمل وطريقة التسخين المختلط بين الحمل والأشعة تحت الحمراء وتأثير ها علي زمن التجفيف ،التغير في المحتوي الرطوبي، الطاقة المستهلكة، الكفاءة الحرارية وجودة المنتج النهائي. وشملت المعاملات التجريبية لطريقة التسخين المختلط ثلاث مستويات مختلفة لشدة الإشعاع (٠,٠٠٥ درجة مئوية) مع ثبات سرع مرعة الهواء عند ٥٠,٠٠٥ ، في حين شملت المعاملات التجريبية درجة مئوية) مع ثبات سرعة الهواء عند ٥٠,٠٥ ، في حين شملت المعاملات التجريبية الخاصة بنظام الحمل فقط ثلاث مستويات مختلفة لدرجة حرارة الهواء ( ٤٥ – ٥٥ – ٥٥ مئوية) وثلاث مستويات من درجة حرارة هواء التجفيف ( ٤٠ - ٥٥ – ٦٥ مئوية) وثلاث مستويات من سرعة هواء التجفيف ( ٢٠,٠٠٥ - ١٥,٠٥ مئوية) وثلاث مستويات من المعاملات التجريبية مئوية) وثلاث مستويات من سرعة هواء التجفيف ( ٢,٠٠ - ٥٠,٠٥ م مئوية) وثلاث مستويات من درجة حرارة هواء التجفي التحريبية عريبة أول ورئيس قسم الهندسة الزراعية - كلية الزراعة - جامعة كفر الشيخ جيزة ٣- مدرس بقسم الهندسة الزراعية - كلية الزراعة - جامعة كفر الشيخ جيزة ٣- مدرس بقسم الهندسة الزراعية - كلية الزراعة - جامعة كفر الشيخ عريزة ٣- مدرس بقسم الهندسة الزراعية - كلية الزراعة - مامعة كفر الشيخ ميزة

Misr J. Ag. Eng., January 2009

تم أيضا مقارنة ثلاث نماذج رياضية لوصف عملية التجفيف في طبقة رقيقة لاختيار الأفضل لوصف عملية التجفيف في كلا الطريقتين. أظهر ت النتائج ما يلي:

- ١- كان معدل التجفيف، الكفاءة الحرارية، نسبة إعادة التشرب والتغير في اللون اعلي لطريقة التسخين المختلط ( الأشعة تحت الحمراء – الحمل) مقارنة بطريقة الحمل.
- ٢- انخفاض زمن التجفيف، الاستهلاك النوعي للطاقة، وكمية الزيت العطري بالنسبة لطريقة التسخين المختلط مقارنة بطريقة الحمل.
- ٣- أمكن للنموذج الرياضي Page وصف عملية التجفيف والتنبؤ بالتغير في المحتوي الرطوبي في كلا من نظام الحمل والنظام المختلط بشكل مرضي مقارنة بالنماذج الأخري موضوع الدراسة.
- ٤- بالنسبة لنظام الحمل، ارتفعت قيم ثابت التجفيف (k) بينما انخفضت قيم الثابت(n) للنموذج المختار (page) وذلك بزيادة درجة حرارة الهواءو سرعته بينما في حالة النظام المختلط ارتفعت قيم ثابت التجفيف (k) بينما انخفضت قيم الثابت (n) وذلك بزيادة شدة الإشعاع ودرجة الحرارة.