# VORTEX DYNAMICS AND CRITICAL CURRENTS IN YBACUO SINGLE CRYSTAL WITH UNIDIRECTIONAL TWINS IN TILTED MAGNETIC FIELDS

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# ABSTRACT

We have measured resistive transitions and current-voltage characteristics for two samples having unidirectional twins oriented parallel and perpendicular with respect to transport current vector in tilted relatively to the c-axis magnetic fields. We observed glass-like behavior of the resistance at small transport currents for current vector oriented perpendicular to twin planes. The observed features of resistive behavior of both samples may be explained by special vortex dynamics in tilted fields.

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# **1. Introduction:**

Investigation of resistive transitions R(T)of YBaCuO superconductor in the presence of an external magnetic field H shows the existence near some temperature T<sub>sh</sub> of a downturn referred to as a shoulder. Current-voltage characteristics (CVCs) for H<sub>c</sub> are linear above  $T_{sh}$  and nonlinear below  $T_{sh}$ . The temperature  $T_{sh}$  is well below the mean-field transition temperature T<sub>c2</sub> and well above the irreversibility line T<sub>irr</sub>. To date, it is supposed that above T<sub>sh</sub> an unpinned vortex fluid and below T<sub>irr</sub> a vortex glass phase exists respectively. Theoretical investigations in weak<sup>(1)</sup> and intermediate<sup>(2)</sup> pinning regime show that below T<sub>sh</sub> then exist a partially pinned vortex-fluid phase. An alternative model<sup>(3)</sup> interprets the shoulder as phase boundary between high-temperature isotropic and low temperature hexatic vortex liquid states.

The aim of this paper is to investigate the phase state and dissipation of vortex system in YBaCuO single crystals tilted relatively to the twins magnetic fields. We will present resistive transitions R(T) and current-voltage characteristics CVCs of a bridge (see inset in Fig. 1) cut out from YBaCuO single crystal having a cross section of  $0.2 \times 0.015$  mm<sup>2</sup>. Measurements were made in a magnetic field H = 15kOe. Transport current vector I was parallel to ab-plane, and was parallel to twin boundaries (TBs) in sample 1 (potential contacts 1 and 2) and perpendicular to TBs in sample 2 (potential contacts 3 and 4). The bridge could be rotated in the field around two axes and desirable orientation of H with respect to TBs could be achieved.

#### 2. Experimental procedures:

Single crystals were prepared, as in a previous study<sup>(4)</sup> grown in a bold crucible by the solution-melt technique with a low temperature gradient along the crucible. This method makes it possible to grow crystals with a size up to  $5 \times 5 \text{ mm}^2$  in the ab-plane and with a thickness 0.02-0.05 mm. The compounds Y<sub>2</sub>O<sub>3</sub>, BaCO<sub>3</sub>, CuO, were used as initial components. The crystals were saturated with oxygen by annealing in oxygen flow for three days at 430 °C. The resistivity of

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the samples subjected to such a thermal treatment was  $\simeq 2 \times 10^{-6} \Omega$ .m and a transition temperature  $T_C = 92.5$  K with a transition width  $\Delta T_c \approx 0.4$ K.

Electrical contacts were prepared by depositing silver paste on the crystal surface, followed by connecting silver wire and 3-h annealing in oxygen at 200°C. The leads for current contacts were fabricated from foil of thickness 0.1 mm and width 3-4 mm, while potential contacts were made of wire having a diameter of 0.05 mm. Such a technology made it possible to obtain a low junction resistance in the contact and to carry out resistive measurements with a transport current up to 1.5 A without ohmic superheating in current contacts, a bridge was cut of a crystal of thickness 0.02 mm as shown in Fig. (1). The bridge width was 0.2 mm, and the separation between potential contacts was 0.3 mm. Twin boundaries in the bridge were oriented in the same direction. The bridge was cut so that the transport current vector I was parallel to twinning planes.

# 3. Results and Discussion:

Fig. (1) shows resistive transitions of the sample 1 measured tilted magnetic fields (curves 1-4). Below  $T_{sh} \approx 88K$  the downturn toward zero resistance is observed. Curve 5 displays the resistive transition of sample 2 in the field H || c. Above  $T_{sh}$ , CVCs were linear for both samples indicating unpinned state of vortices.

Fig. (2a) shows CVCs of sample 1 measured at temperatures below  $T_{sh}$  for  $\Theta = 7^{\circ}$ ,  $\Phi = 0.0$  (curves 1-5) and for  $\Theta = \Phi = 0$  (curve 6). CVC for  $\Theta = 0$  is strongly nonlinear and hence vortices aligned parallel to TBs are in a pinned state. For  $\Theta = 7^{\circ}$  CVCs are linear but the resistance  $R_1 = dV/dI$  is much smaller than the Barden-Stephen flux flow resistance  $R_{BS} = R_N B/B_{c2}$  (here  $R_N$  is the normal state resistance and  $B_{c2}$  is the induction of the upper critical field). In magnetic fields tilted with respect to TBs, the vortex has the structure<sup>(5)</sup> shown in Fig. (2b). Since the part of vortex r aligned with TBs is pinned, the resistance  $R_1$  may arise due to movement of the part

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of the vortex s placed out of TBs. In this case the part of vortex s may be considered as unpinned vortex fluid which possesses torsional rigidity due to pinning of the vortex parts r aligned with TBs. Torsional rigidity associated with preserving orientation order may be the reason of linear resistance decreasing with the temperature decreasing.

Fig. (3a) shows CVCs of the sample 2 measured at temperatures below  $T_{sh}$  for  $\Theta = 0$ . Curves 1-5 were obtained for  $\Phi = 9^{\circ}$  and curves 6 and 7 were obtained for  $\Phi = 0$ . The full set of CVCs for  $\Phi = 0$  is presented in Ref. 5. Initial parts of the curves are nonlinear due to thermally activated flux creep that occurs when the Lorentz force  $F_L$ =I.B is smaller than the pinning force  $F_P = I_{ed}B$ , which is defined by the depinning critical current  $I_{cd}$ . At higher values of I linear or almost linear I – V curves are observed indicating the flux flow regime for  $F_L>F_p$  or  $I>I_{cd}$ . In this regime, the derivative dV/dI defines the flux flow resistance and extrapolation of linear parts of CVCs to V=0 defines  $I_{cd}$ . Near T  $\approx$  84.3 K we have obtained  $R_f(\Phi = 0) \approx 4$  ohm.m and  $\approx 4.5$  ohm.m, which are in good agreement with  $R_{BS} \approx 4.1$ m.Ohm. The depinning critical current for  $\Phi = 0$  is about 1.8 times smaller than for  $\Phi = 9^{\circ}$ . For  $\Phi = 9^{\circ}$ , the initial parts of CVCs are adequately described by the equation<sup>(6)</sup>.

$$V = A \exp(-C/\sqrt{I}) \tag{1}$$

Where A and C are constants. Such dependence is predicted for vortex-glass phase for small currents. Initial parts of CVCs for  $\Phi = 0$  are best presented by Anderson-Kim flux creep model<sup>(7)</sup>.

$$V = \text{Dexp} (-U_o/T) \sinh (U_o I/I_c T)$$
 (2)

Where  $I_c$  is the critical current,  $U_o$  is the pinning potential, and D is phenomenological parameter. Since for vortex-glass phase initial parts of CVCs are described by Eq.1, we think that this dependence may indicate existence of the vortex-lattice phase at low temperatures for H strictly parallel to c-axis<sup>(2)</sup>. The rotation of magnetic field off TB planes gives rise to vortex-glass phase and enhances the value of  $T_{cd}$ .

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**Fig. (1):** Arrhenius plot of the resistive transitions of sample 1 (curves 1-4) and sample 2 (curve 5). Curves 1-4 correspond to  $\Theta = 0$ , 3°, 7° and 11° respectively ( $\Phi = 0$ ). Curves 5 was obtained for  $\Theta = \Phi = 0$ . Inset shows the bridge which we have used and geometry of the experiment.



**Fig. (2):** (a) I-V curves of sample 1 measured for  $\Phi = 0$  and  $\Theta = 3^{\circ}$  at temperatures T = 87.34, 87.03, 86.65, 86.07 and 85.47 K (curves 1-5 respectively). Curves 6 measured for  $\Theta = \Phi = 0$  and T = 87.31 K. (b) The geometry of the vortex in tilted field, bold arrow shows the direction of the vortex movements.

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**Fig. (3):** Current-voltage characteristics of sample 2 measured for  $\Phi = 9^{\circ}$  and  $\Theta = 0$  at temperatures T = 86.82, 86.46, 86.04, 85.41, 84.21 K (curves 1-5 respectively) and for  $\Theta = \Phi = 0$  at temperature T = 84.29 and 81.81 K (curves 6 and 7 respectively). Solid curves in panel (b) are interpolation of initial parts of CVCs by Eq. 1 (for curves 2-5) and Eq. 2 (for curves 6 and 7).

The best fit of experimental curves with Eq. 2 at temperatures  $T \le 82K$  was obtained for  $U_o \approx 1900K$  and  $D \approx 10^{-4}$ . For thermally activated hopping of flux lines or bundles over a pinning barrier we may write,<sup>(8)</sup>  $D = 2aNV_oBl$  and  $U_o=BLV_cI_c/s$  where a is the jumping distance, N is the number of vortices in a cascade,  $V_o$  is the attempt frequency,  $l \approx 0.2$  mm is the length of the sample, L is the dimension of the pinning well, and  $V_c$  is the activation volume. Supposing  $L \approx \xi 40A$  ( $\xi$  is the Ginzburg-Landau coherence length), we obtain  $V_c = 10^{-19}$  m<sup>3</sup> which is about 5 times greater than the volume of the flux line V  $\approx 2.10^{-20}$  m<sup>3</sup>. Supposing a = a<sub>o</sub>  $\approx 360A$  (a<sub>o</sub> is the separation between vortices) and N  $\approx 5$  we obtain  $V_o \approx 10^6$ Hz. This value is much smaller than the phonon frequency which we estimate to be about  $10^{11}$ Hz.

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الملخص

ديناميكية الدوامات والتيارات الحرجة في البلورة الأحادية YBaCuO ذات تنائيات حدود متمايلة مع المجال المغناطيسي

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تم قياس المقاومة النوعية الانتقالية والمنحيات المميزة للجهد والتيار للبلورة الأحادية تم قياس المقاومة النوعية الانتقالية والمنحيات المميزة للجهد والتيار الناقل فى وجود مجال YBaCuO التى بها ثنائيات حدود موازية ومتعامة مع متجة التيار الناقل فى وجود مجال مغناطيسى متمايل مع ثنائيات الحدود بالنسبة للمحور C . تم قطع قنطرة من البلورة كما فى شكل (1) حيث المقطع المستعرض لها يساوى  $^{2}$ mm 20.05 mm 20.0 × 0.0 . تم مشاهدة السلوك الزجاجى للدوامات عند التيارات الصغيرة لمتجه التيار المتعامد على مستوى ثنايات الحدود. الزجاجى للدوامات عند التيارات الصغيرة لمتجه التيار المتعامد على مستوى ثنايات الحدود. ويكون متعامداً مع تنائيات الحدود فى العينة رقم (1) (جهد التلامس ۱ ، ۲) موازيا للمستوى متائيات الحدود فى العينة رقم (1) (مهد التلامس ۱ ، ۲) القيامي متعامداً مع ثنائيات الحدود فى العينة رقم (1) (مهد التلامس ۱ ، ۲) المقاومة الانتقالية باستخدام الزحف التدفقى لموديل اندرسون . كيم.

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