

Thermal, Mechanical and Electrontransport Properties of Irradiated Rapidly Solidified Pb-Sn-Zn Alloy

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The effect of gamma irradiation on the thermal, mechanical parameters and electrical properties of Pb-5wt.% Sn-0.5 wt.% Zn alloy rapidly solidified from the melt was investigated. The results showed irregular behaviour of the parameters measured for samples irradiated with doses up to 200 KGy. Above 200 KGy a clear trend of variation took place. The values of the specific heat under constant pressure C_p and the activation energy of ordering, U , showed opposite behaviours above 200KGy, up to 1 MGy. The deterioration of the elastic modulus and internal friction properties caused by irradiation appear to have a bad potential for using the present alloy as structural material soldering alloy in nuclear structures. The increased resistivity with irradiation was rendered to the increased scattering of transport electrons caused by the created scattering centres induced by gamma-rays.

1 - Introduction:

The wide use of lead-tin base alloys justifies their further investigations. Rapid solidification from the melt produces solid tapes of amorphous and fine microstructure suitable for investigating the mechanical properties[1]. These tapes show improved ductility, formability, stress corrosion life and fracture toughness [2].

Sn content in Pb-Sn alloys used in acid-battery applications was found [3] to increase the electronic conductivity sharply when alloying tin content is increased from 0.8 to 1.5 wt.%. The electrical resistivity variations of rapid solidified Pb-10 wt.% Sn soldering alloy were used to estimate the solid mass fraction as a function of temperature [4]. The equilibrium phase diagram of the Pb-Sn system was investigated using differential thermal analysis (DTA) technique [5]. The results show a clear eutectic effect within ± 2 K of the eutectic temperature, 456K. By using the mechanical analogue model [6], it was found that the width of the sliding-no sliding transition is governed by a power law. An estimate of the interphase diffusivity based on the sliding viscosity provides a value that is 1-2 orders of magnitude higher than that based on the boundary diffusion data.

In spite of the tremendous progress that has been made in the discipline of irradiated ingots rapidly solidified from melt, there still remains lack of information about the development of even more sophisticated and specialized soldering materials [7, 8, 9].

The aim of the present work is to investigate the effect of γ -irradiation on the mechanical, thermal and electrical properties of rapidly solidified Pb-5 wt.% Sn-0.5 wt.% Zn. alloy at different temperatures.

2 - Experimental Procedure:

2.1 - Sample preparation:

Samples of Pb-5 wt.% Sn-0.5 wt.% Zn alloy rapidly solidified from the melt were obtained by using a single aluminium roller (20 cm in diameter at a constant speed of 30.4 m s⁻¹). In such technique the cooling rate is assumed to be very high, about 10⁶K s⁻¹, due to the small thickness of the produced ribbons and the high velocity of roller. Full details of sample preparation, procedure and techniques are published elsewhere [10]. The prepared samples were irradiated to different doses up to 1 MGy. Irradiation of specimens was carried out in air, at room temperature and with a dose rate of 0.9 Gy s⁻¹ by using a Co⁶⁰ source from a gamma-rays chamber.

2.2 - Mechanical properties:

According to the improved measuring system suggested previously [11], a modified dynamic resonance vibrator as that published elsewhere [12] was used to study the mechanical behaviour of the investigated samples. The amplitude of vibration against the frequency of vibration, around the resonance frequency F_0 , gives the resonance curve which characterizes the mechanical resonance of the sample. From the resonance curve, the internal friction, Q^{-1} , and the dynamic elastic modulus, E , were obtained from the following relations [13]:

$$Q^{-1} = 0.5773 \frac{\Delta F}{F_0} \quad (1)$$

where ΔF is the full width at half maximum amplitude, and

$$\left(\frac{E}{\rho}\right)^{\frac{1}{2}} = \frac{2\pi L^2 F_0}{KZ^2} \quad (2)$$

where ρ is the density of the sample under test, L is the length of the vibrating part of the sample, K is the radius of gyration of cross section perpendicular to its plane of motion, and Z is a constant depends on the mode of vibration and assumes the value of 1.851 [14].

2.3 - Differential thermal analysis :

The differential thermal analysis (DTA) data were obtained by using Shimadzu thermal analyzer, DT-30. The heating cell was two platinum crucibles one of which contained the reference material while the other contained the specimen under test. The specimen weight was about 20mg. The heating rate was kept constant at 10K min^{-1} in the temperature range 300-600 K.

The specific heat under constant pressure (C_p) obtained from the DTA thermograms by using the relation [15]:

$$C_p = \frac{Q}{MT_m} \quad (3)$$

where the energy Q dissipated through the sample is proportional to the area under the DTA curve deviated from the base line, M is the mass of the sample and T_m is the melting temperature of the sample.

2.4 - Electrical measurements:

The electrical measurements at different temperatures for the investigated samples were made by using the four probe Kelvin Double-Bridge method. The variation of the temperature, was carried out by a step-down transformer connected to a constructed temperature controller. The heating rate was kept constant at 10Kmin^{-1} . The specimen temperature was measured by Beckman Industrial TP850 digital thermometer.

3 - Results and Discussion:

The irradiation dose dependence of the elastic modulus of the investigated samples is demonstrated in Fig. (1a). A sharp drop of the dynamic Young's modulus at 20KGy is followed by an increase to a peak value at 100KGy irradiation dose. Further increase of irradiation dose decreases the modulus and above 200KGy it shows slight increase. Clustering of the initially irradiation induced defects may take place and this reduces the number of dislocation pinning points leading to the observed decrease of the dynamic Young's modulus (E), and the increase of the internal friction (Q^{-1}).

At 100KGy , the free induced defects increase the number of dislocation pinning points which harden the alloy, and this, as shown in Fig.1, increases the dynamic Young's modulus (E) and decreases the internal friction (Q^{-1}). To fit the experimental data of Fig.1, it is assumed that the probability of clustering of the defects produced by the 200KGy dose, is higher than that produced at 20KGy , This decreases the density of the

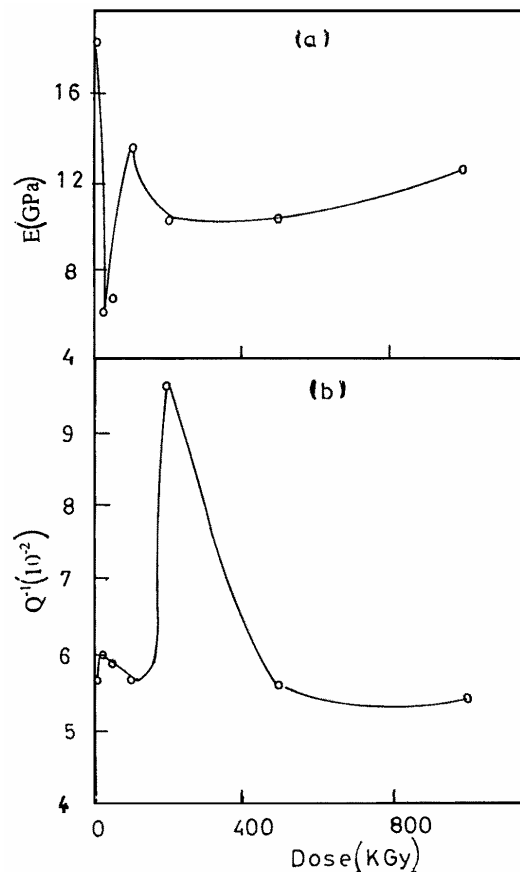


Fig. (1) Dependence of:
 a) dynamic elastic modulus (E).
 b) internal friction (Q^{-1}).
 on the irradiation dose of γ -rays

pinning points for dislocations and consequently decreases the stiffness of the alloy and decreases E and increases Q^{-1} values. The increased density of the induced irradiation defects (above 200 KGy) increases dislocation pinning as indicated by the relative increase of (E) and the decrease in (Q^{-1}) values.

Figure 2 shows the temperature dependence of the specific heat under constant pressure, C_p , for samples irradiated with different doses. The irradiation dose dependence of the maximum specific heat under constant pressure C_p^{max} , as obtained from Fig. (2), is given in Fig. 3a. Both the liquidus temperature T_L and the solidus temperature T_s are displayed, in Fig. (3b,c). Two peaks are observed in Fig. (3a), an initial sharp peak at 50 KGy followed by a drop to nearly the original value, then a peak at 200 KGy, followed by a continuous decrease with irradiation dose up to 1 MGy. At 200 KGy, T_s increases to a high value and T_L reaches its maximum value. The change of specific heat ΔC_p with increasing temperature obeys the experimental law [16].

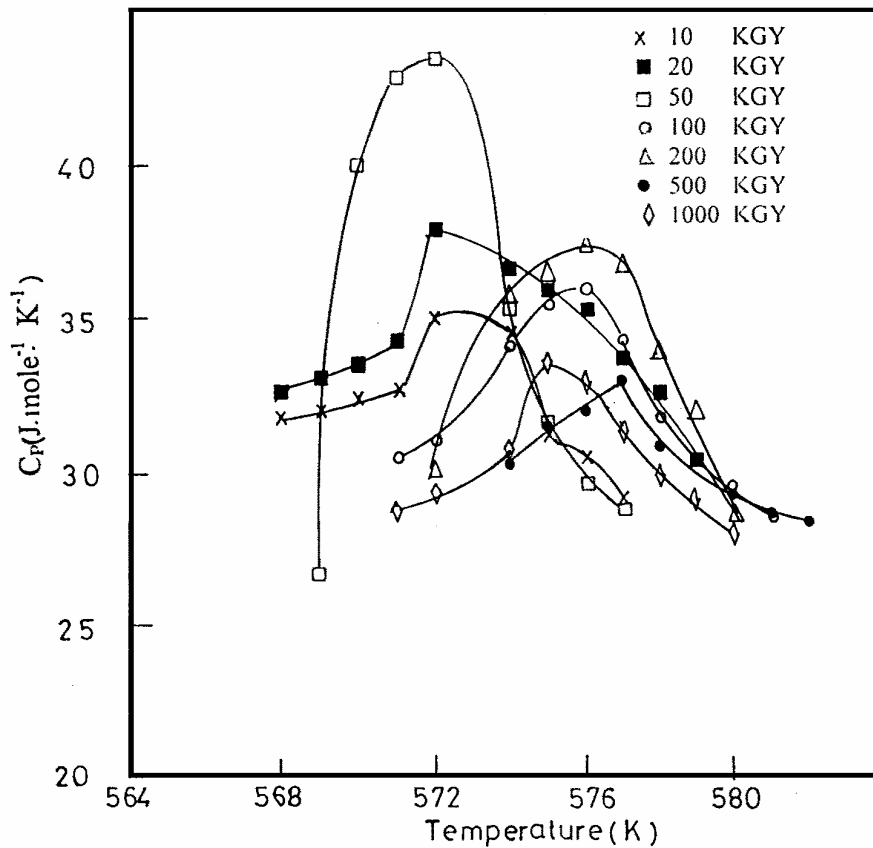


Fig. (2): Temperature dependence of specific heat at constant pressure C_p .
 $\Delta C_p = A (NU^2/RT^2) \exp (U/RT)$ (4)

where N is the number of atoms displaced from the equilibrium position, U is the activation energy of ordering transition, R is the universal gas constant and A is the coordination number. Irrespective of the value of the pre-exponential term the relation between $\ln(\Delta C_p T^2)$ and $1/T$ for the alloy samples irradiated to different doses should give straight lines as those shown in Fig.4. The slopes of the straight lines of Fig. (4), give the activation energy of ordering. The irradiation dose dependence of the activation energy U is given in Fig. (5a). It is clear that the value of the energy of ordering U, increases at 50 KGy, then decreases at 100KGy and gradually increases again up to 1 MGy. From Figs(3a) and (5a), the decrease of C_p^{\max} above 200KGy corresponds to an increase in the energy U. The variation of the relative change of the activation energy of ordering $\frac{\Delta U}{U_o}$, where U_o is the value of the activation energy of ordering for the sample irradiated to 10kGy dose, with the irradiation dose is shown in Fig. 5b.

It is clear that $\frac{\Delta U}{U_o}$ increases at 50 KGy then drops to a minimum at 200 KGy after which it increases again gradually up to a maximum value at 1MGy.

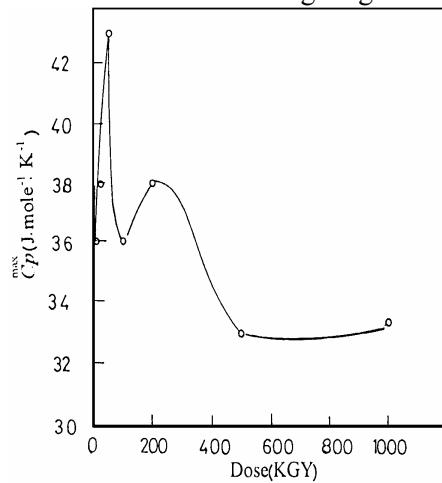


Fig. (3a) : The maximum specific heat at constant pressure C_p^{\max} dependence on irradiation dose.

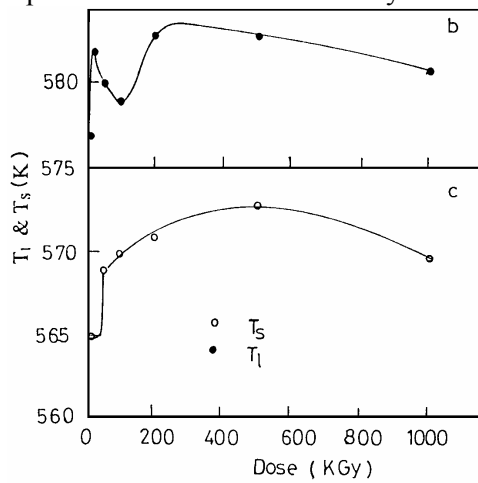


Fig. (3 b,c): Variation of liquidus temperature T_L and solidus temperature T_S with irradiation dose.

The softening at 50 KGy observed in Fig. 1, showing itself as a decrease in E and increase in Q^{-1} consists with the increased absorbed energy, Fig (5a), required to activate the dislocation movements taking place in this state. The reduction of such movements at 100 KGy agrees with the observed increase of E shown in Fig. 1, and refers to the minimum energy required as shown in Fig. (5a).

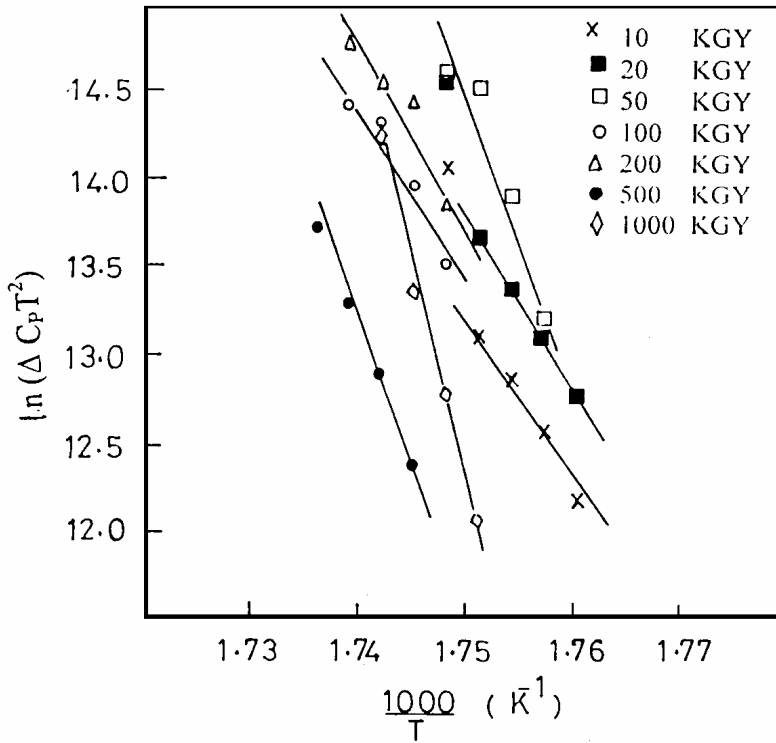


Fig. (4): The $\ln(\Delta C_p T^2)$ Value against $1/T$ at different irradiation dose.

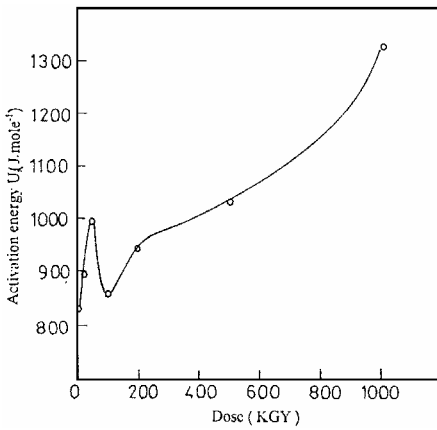


Fig. (5a) The variation of activation energy of ordering U with irradiation dose.

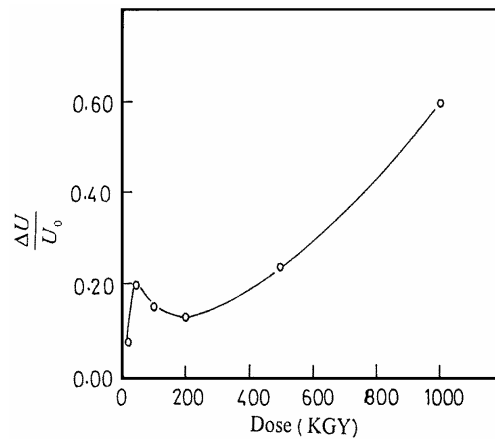


Fig. (5b) The relative change of activation energy of ordering $\frac{\Delta U}{U_0}$ as a function of irradiation dose.

Figure 6, shows the temperature dependence of the electrical resistivity of the alloy samples irradiated with different doses. In general, continuous increase of resistivity is observed with increasing temperature and/or irradiation

dose. The increase in resistivity may be due to the increase of the existing defects, and their thermally activated diffusion in the alloy components.

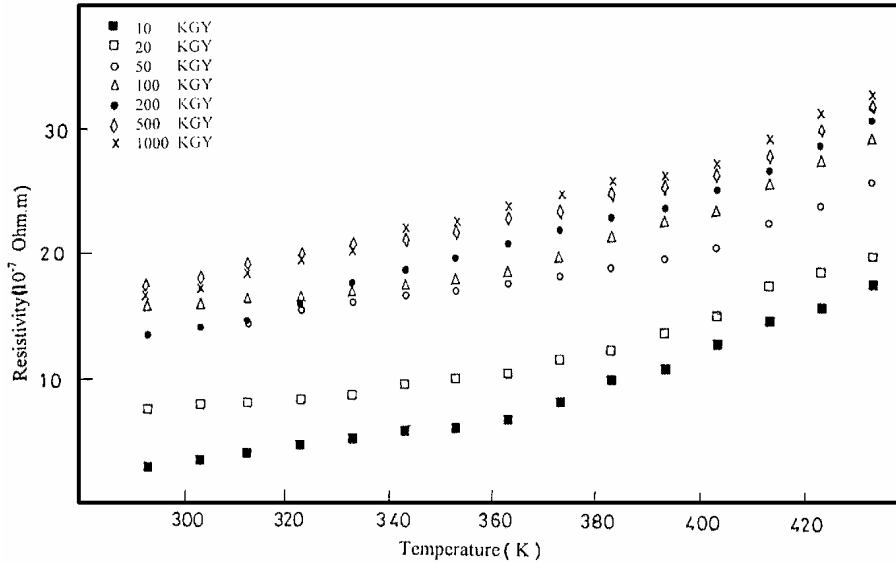


Fig. (6): The electrical resistivity as a function of the temperature at different irradiation doses.

The influence of gamma-rays irradiation on the studied thermal, mechanical and electrontransport properties can be attributed to the creation of defect centres with inhomogeneous distribution. Low density of these centres is created at low gamma-ray irradiation dose. This density increases with the increase of irradiation dose, which creates more defect centres.

Conclusions:

From the foregoing analysis of the results obtained for the rapidly solidified Pb-5 wt%- Sn 0.5 wt.% Zn alloy, the following conclusion may be drawn:

- 1 - Thermal, mechanical and electrontransport properties are very sensitive to ionizing radiation.
- 2 - The deterioration of the elastic modulus and internal friction properties caused by irradiation appears to have a bad potential for using the present alloy as structural material soldering alloy in nuclear structures.
- 3 - The activation energy of ordering U and specific heat under constant pressure C_p are inversely affected above 200KGY irradiation dose.

- 4 - The electrical resistivity of the studied alloy depends on irradiation dose due to the increase of the disordered scattering of transport electrons caused by the Scattering created by gamma-rays irradiation.

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