Methylene Blue and Crystal Violet Dyes Removal (As A Binary System) from Aqueous Solution Using Local Soil Clay: Kinetics Study and Equilibrium Isotherms

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IN THIS PAPER, local soil clay as a low cost and affordable adsorbent was employed for the successful removal of methylene blue (MB) and crystal violet (CV) dyes from an aqueous binary system. The effect of various experimental conditions like adsorbate concentrations, time, temperature, and pH has been investigated. To know the adsorption performance of the dye molecules upon soil clay, the kinetics of the adsorption data were analyzed using various models such as pseudo-first-order and pseudo-second-order. This kind of study shows that the maximum adsorption reached at 2 min and uses the pseudo- second-order kinetics. The adsorption Kinetics have been investigated in the pH range of 2, 3.7, 7, and 8.7 at 25°C and analyzed with two different models namely Langmuir and Freundlich. The interaction of dye molecules with soil clay has been investigated by SEM, EDS, FTIR, and XRD. Maximum removal of MB and CV up to 47.82 and 35.71 mg g^{-1}, respectively was achieved by dye molecules adsorption onto soil clay. This effective removal method may provide a promising solution for eliminating of CV and MB dyes from wastewater.

Keywords: Soil, Methylene blue, Crystal violet, Binary system, Dye removal, Wastewater.

Introduction

Clean water is essential for a healthy life. A non-toxic environment and fresh water are society's serious priorities. Yet, widespread pollution of fresh water and the industrial waste penetrating the ecosystem is beginning an alarming state. The development of agriculture and water system frameworks lead to more interest in water resources and especially for the treated wastewater in water system frameworks [1]. The presence of different environmental pollutants in drinking water has additionally increased worldwide health worries. Contamination of water bodies is mainly referred to the presence of toxic chemicals, including organic compounds (like dyes), and heavy metals [2]. Therefore, several techniques have been applied to treat the organics in wastewater; such as adsorption [3], nanofiltration [4], ozonation [5], and electroflotation [6]. Adsorption was found to

be a perfect technique for wastewater treatment in terms of economic cost, the simplicity of design, insensitivity of toxic substances, and ease of operation [7, 8].

Dyes are the greatest serious environmental problems which delivered into the environment from many industrial processes, such as cosmetics, textile, paper, food, printing, plastic, pharmaceutical, and leather [9]. Their presence in water bodies is unwanted as they are difficult to remove due to their tenacious and recalcitrant nature [10]. Dyes in water are undesirable even at very low concentrations - highly visible- and need to be removed before the wastewater discarded into the environment [11]. As a result, the photosynthetic phenomenon of aquatic life is greatly affected owing to the reduced light penetration [12]. However, dyes are fairly difficult to biodegrade and eliminate from dye

wastewater owing to their complex aromatic molecular structures and high solubility in water [13]. There are several dye wastewater treatment methods presented, including photo-degradation, coagulation, chemical oxidation, reverse osmosis, membrane filtration methods, biosorption, and ozonation [14-19]. However, these methods have higher operating costs or are unproductive in dye wastewater treatment. Adsorption has attracted the attention owing to its numerous advantages, for example, low cost and high efficiency related to other dye wastewater treatment methods. Several of adsorbents have been studied for dyes removal from aqueous solutions like, corncob and barley husk, cocoa pod husks, palm kernel shell, spent tea leaves, ginger waste, metal-organic frameworks (MOFs), activated carbon, peat, chitin, silica and graphene oxide [11, 20-28]. In this way, the application of soil as adsorbents of toxic dyes received significant consideration in the last time due to their low cost, available in a large amount, high surface area, and nontoxic [29].

Crystal violet (CV) and methylene blue (MB) have dangerous effects on living organisms on little periods of exposure. MB is used extensively as a colorant in the textile industry such as wool, silk, and cotton. It can cause many health problems like eye burns, cyanosis, and irritation of the skin [30]. CV (related to triphenylmethane group) is widely used as an animal drug in veterinary. Moreover, it is utilized as a biological dye to identify bloody fingerprints [31]. It is unsafe for humans and can cause cancer when consumed or inhaled [31].

Most of the reports in the literature study the adsorption of single adsorbate from the solution onto solids. Limited studies deal with binary or ternary blends adsorption on the solid surfaces. So the intention of this study has investigated the use of local soil to remove of MB and CV dyes from the binary system. In addition, we also thoroughly studied the kinetics of different aspects affecting the adsorption procedures such as dye concentration, soil dose, pH, and temperature.

Materials and Methods

Materials

Methylene blue (MB) and Crystal violet (CV) are purchased from Sigma-Aldrich (Germany) and used as received. Soil samples were obtained from Shoubk Ekrash village, Sharkia, Egypt.

Methods

Preparations of s-soil

The soil samples were dispersed in the lab. Briefly, 250 g of the presource soil (pr-soil) are added in 2.5 L distilled water with stirring at 500 rpm for 2 h to reach a high dispersion degree for the soils. The shaking sieve with a pore size (1, 2 mm, 45, 63, 125, 250, and 500 μm) was used to separate the suspension to its different size. The suspended particles are divided into two different layers as seen in scheme 1. After that, the solid- after removing excess water- was dried at 90 °C for 24 h. The lower layer (s-soil) was separated and used for dye removal experiments.

Samples characterization

Fourier transform infrared spectroscopy (FT-IR) (Shimadzu FTIR-8400 S, Japan) was used to record the IR spectra of the soil. For all spectra, thirty scans were collected with a 4 cm^{-1} resolution.

X-ray diffraction analysis of soil was done using Shimadzu X-ray diffraction (7000, USA, Cu-Kα radiation). The radiation wavelength was 1.5406 Å. The data were collected in the form of 2θ versus intensity (a.u) chart.

The surface morphology of the soil was analyzed using a scanning electron microscope (SEM) (JEOL, model JSM-6460LV, Tokyo, Japan) operated at an acceleration voltage of 20 kV. For this purpose, the soil pieces were coated with gold by JFC-1100E sputter (JOEL Ltd., Tokyo, Japan). Finally, elemental analysis was done using EDX.

Adsorption Process

The dye adsorption (by s-soil) was studied by determining the color change of the binary dye system (MB & CV) in the aqueous solution. The binary dye solution stock was prepared by using 0.2 % of MB and CV (1:1) in distilled water. Many experimental parameters were studied in a kinetic manner with stirring speed 500 rpm and the volume of the dye solution used was 20 mL such as dye concentrations (100, 200, 300, 400 and 500 ppm), amounts of s-soil (25-100 mg), and pH (2, 3.7, 7, 8.7) in addition to the temperature (25, 40, 55, and 70 °C). Finally, 0.5 mL of the suspension was removed and centrifuged. After that, of 0.1 mL of the centrifuged solution diluted with distilled water to 10 mL for further measurement. MB and CV concentration were measured at 662 and 590 nm, respectively, using UV/Vis Spectrophotometer (Double beam) (T80+, PG Instruments Ltd., UK.) [32-34].

The dye removal efficiency (R %) is defined by Eq.1:

$$R\% = \frac{(C_o - C_t)}{C_o} \times 100 \quad \text{.......} \quad (1)$$

Where C_t is the concentration of dye at time t, and C_o is the initial concentration.

Experimental parameters
  Effect of dye concentration
  The effect of dye concentration (100, 200, 300, 400, and 500 ppm) on the removal percent (R %) was studied. The adsorbent dose was 5 g L^{-1}, the solution pH was 7 and the temperature was 25 °C.

Effect of soil clay dosage
  The effect of soil dosage was done in the concentration range of 1.25 –5.0 g L^{-1}. The study was achieved at pH 7, at 25 °C for 10 min, and the initial dye concentration was 300 ppm.

Initial pH effect on the dye removal
  The effect of pH range (2, 3.7, 7, and 8.7) on the CV and MB dye adsorption was studied. The study was achieved with an initial dye concentration of 300 ppm, at 25 °C for 10 min, and the adsorbent dose was 5 g L^{-1}.

Effect of the temperature on dye removal
  The temperature ranges effect (25, 40, 55, 70 °C) on the adsorption of CV and MB dyes was studied. The study was done with initial dye concentration of 300 ppm, the adsorbent dose was 5 g L^{-1} and pH was 7.

Adsorption kinetics
  Two well-known kinetic models were investigated. Pseudo-first-order presented by Lagergren equation [35] Eq. 2.

$$\log(q_e - q_t) = \log q_e + \frac{K_{ads}t}{2.303} \quad (2)$$

Where q_e (mg g^{-1}) is the amount of sorption at equilibrium time, q_t (mg g^{-1}) is the amount of sorption at time t, and K_{ads} (min^{-1}) is the rate constant of pseudo-first-order sorption. $Q_{e \text{ and }} q_t$ can be calculated by Eq. 3 and 4.

$$q_e = \frac{(C_o - C_e)V}{1000w} \quad (3)$$

Where C_e is the dye concentration at equilibrium time (mg L^{-1}), C_o is the initial concentration (mg L^{-1}), V is the volume of dye solution (mL), and W is the mass of adsorbent (g)

$$q_t = \frac{(C_o - C_t)V}{1000w} \quad (4)$$

Where C_t is the dye concentration at different time (mg L^{-1})

Pseudo-second-order expressed by Ho equation [36] the equation developed in a linear form as Eq. 5.

$$\frac{t}{q_t} = \frac{1}{K_2 \, q_e^2} + \frac{t}{q_e} \quad (5)$$

Where K_{ads} (g mg^{-1}min^{-1}) is the rate constant of pseudo-second-order reaction.

Adsorption isotherm
  The adsorption isotherm model was used to clarify the interaction between the adsorbate and the adsorbent. The most famous models used for the description of it are Langmuir (Eq. 6) and Freundlich (Eq. 7).

$$\frac{C_e}{q_e} = \left(\frac{1}{bq^o}\right) + \left(\frac{1}{q^o}\right)C_e \quad (6)$$

$$\text{Log } q_e = \text{ Log } K_f + \frac{1}{n}\text{ Log } C_e \quad (7)$$

Where C_e is the equilibrium concentration (mg L^{-1}), q_e is the amount adsorbed at equilibrium time (mg g^{-1}), q° is the maximum dye species uptake per unit mass of adsorbent (mg g^{-1}), and b is Langmuir constant (L mol^{-1}). K_f (mg g^{-1}) and "n" are Freundlich constants.

Whereas R_L designates the shape of the isotherm and can be obtained from Eq. 8:

$$R_L = \frac{1}{1 + bC_o} \quad (8)$$

Where the R_L is the separation parameter ($R_L > 1$ unfavorable, $R_L = 1$ linear, $0 < R_L < 1$ favorable, $R_L = 0$ irreversible)

Results and Discussion

UV-Vis-spectrum
  Figure 1a exhibits the characteristic reflections of the MB, CV, and binary system dyes (MB&CV) using UV-Vis-spectrum. In the individual system, MB and CV dyes show maximum peak absorption at 662 and 596 nm, respectively. On the other hand, MB&CV dyes in binary system exhibit two maximum absorption peaks in the visible spectral region (662 and 596 nm) and three other small peaks in the UV region (294, 248 and 208 nm), which confirm the existence of both dyes in the solution. Those results agree with previous other work [32-34].

Upon the dilution of the dye solution, the intensity of the peaks decreases in both UV and Vis-regions as illustrated in Fig. 1b. This confirms that the dilution cause concentrations
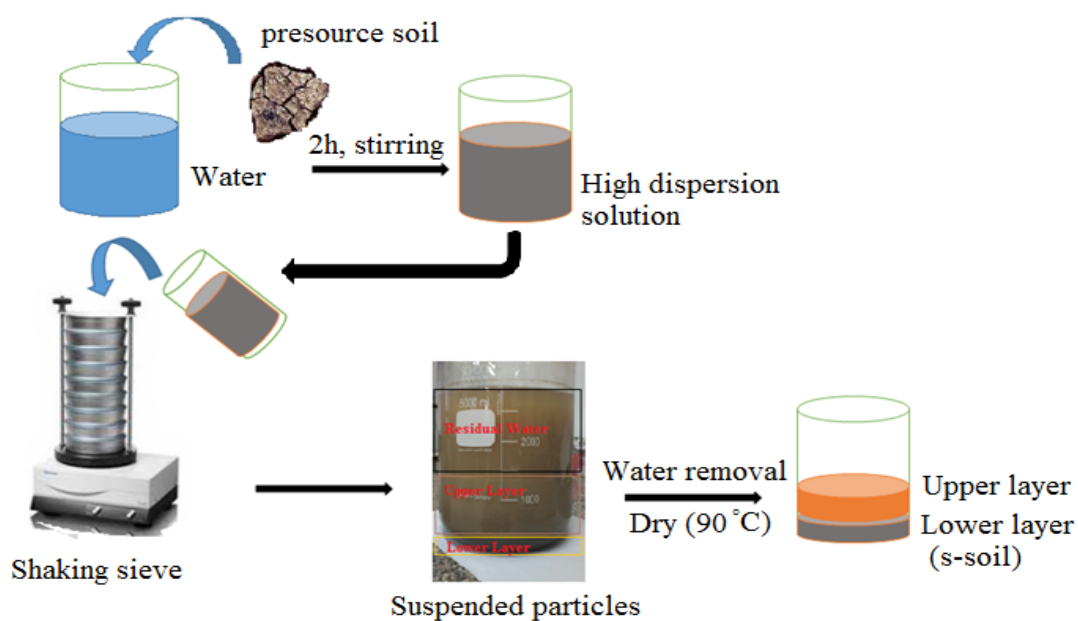
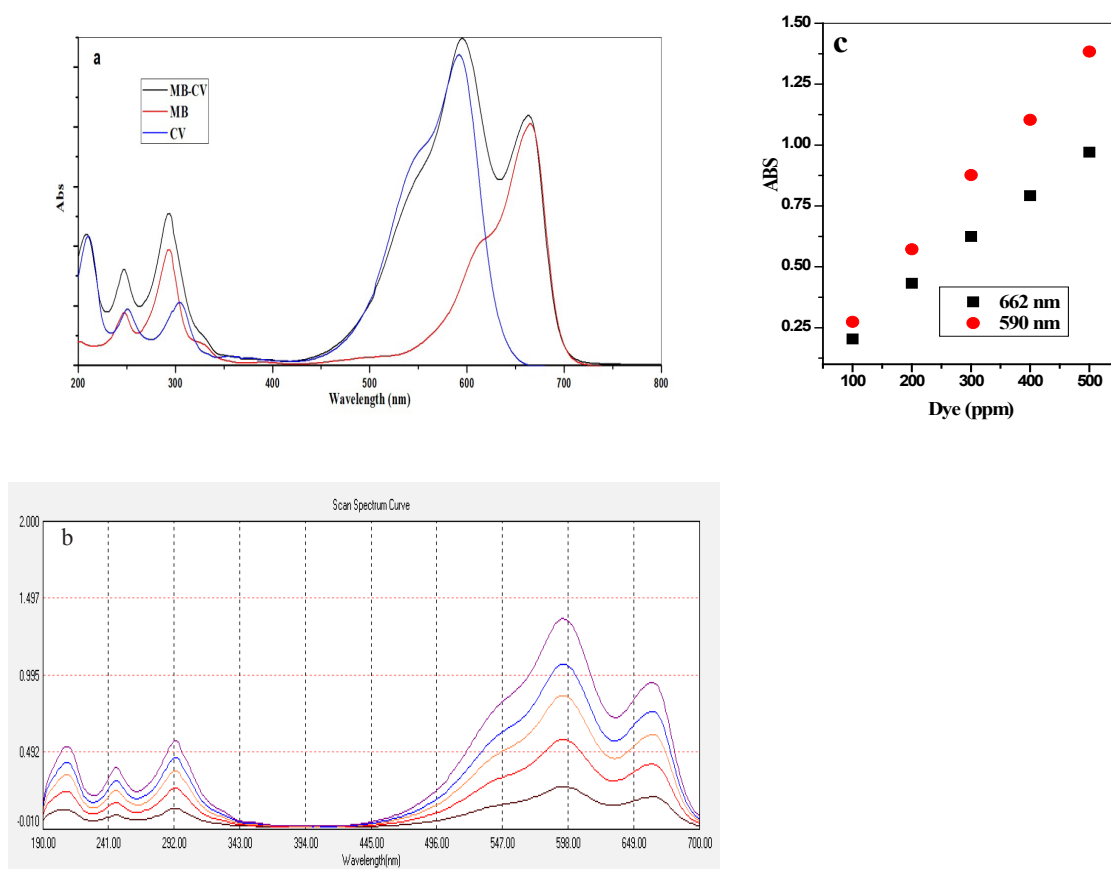**Scheme 1. The schematic diagram of the experimental process.**

Fig. 1. a) UV-spectrum, b) The dilution of the dye solution in the binary system and c) The calibration curve of MB and CV dyes.

reduction of both dyes in the binary system.

Figure 1c illustrates the calibration curve in the UV-Vis spectrometer for MB&CV dye in the binary system. The figure indicated that there is a relationship (linear) between the absorbance and the concentration for the two dyes in the binary.

Characterization

Figure 2 (a-c) illustrates the SEM image for surface morphology and the approximate size of the s-soil. The soil particles appear distributed inhomogeneously with irregular shape particles which leads to increase of the absorption surface area. Table 1 shows the composition of pr-soil and s-soil by EDX analysis. The data show the presence of Al, O, Si, Na, K, Mg, Ca, Fe and Ti, elements were confirmed in both pr-soil and s-soil with a small variation in Al % values.

Figure 2d show the FTIR spectra of pr-soil, s-soil, MB, CV, and s-soil adsorbed dye. The pr-

soil and s-soil show characteristic M-O vibration peaks at 1024 and 764 cm^{-1} (M = Si, Fe, Mg, Ti, Al and Ca). The gotten peak values have a good agreement with the literature [37]. Furthermore, the absorption peak at 467 cm^{-1} is related to the M–O–M [38]. The wide absorption peak in the range of 3431 cm^{-1} corresponds to –OH group and this designates the presence of water (absorbed) on the nanoparticles' surface [38, 39]. Furthermore, the figure shows the characteristic bands for both MB and CV dyes in its solid state. But, the typical bands of those dyes have been overlapped with the M-O bands of the adsorbent. Those results have been reported [40].

Figure 2e illustrates the XRD patterns of the pr-soil and s-soil. Pr-soil exhibited fine and intense peaks at 2θ = 21.1° and 27.4°, which are characteristic of crystallized material with more noise along X-ray diffractogram. Moreover, the XRD pattern of s-soil represents sharp, intense peaks at 2 θ = 21.5°, 27.4°, and 50.8° with more

TABLE 1. EDX analysis of pr-soil and s-soil.

	pr-soil					s-soil					
Element	(keV)	mass%	Error%	At%	Cation K	Element	(keV)	mass%	Error%	At%	Cation K
O K	0.525	36.53	0.49	53.60	33.8111	O K	0.525	42.67	0.45	59.18	44.5712
Na K	1.041	1.50	0.30	1.53	1.2518	Na K	1.041	1.09	0.33	1.06	0.8860
Mg K	1.253	2.07	0.24	2.00	1.5381	Mg K	1.253	2.76	0.25	2.52	1.9975
Al K	1.486	9.20	0.21	8.00	8.1292	Al K	1.486	10.58	0.23	8.70	8.9799
Si K	1.739	29.16	0.23	24.37	28.0032	Si K	1.739	27.14	0.25	21.44	24.5741
K K	3.312	1.49	0.26	0.89	1.9440	K K	3.312	1.26	0.28	0.72	1.5749
Ca K	3.690	6.18	0.29	3.62	8.5767	Ca K	3.690	3.52	0.32	1.95	4.6710
Ti K	4.508	2.15	0.36	1.06	2.5319	Ti K	4.508	1.13	0.40	0.52	1.2773
Fe K	6.398	11.73	0.64	4.93	14.2140	Fe K	6.398	9.86	0.70	3.92	11.4680
Total		100.00		100.00		Total		100.00		100.00	

smoothing diffractogram. The X-ray diffraction spectrum of pr-soil displays the existence of the two main strong peaks at 21.00° and 27.00° that match two respective (004) and (202) images of calcium aluminum silicate phase in the samples [41].

Adsorption parameters

Dye concentration effect

Figure 3(a, d) represent the removal percent (%R) variation versus the contact time. The results show that %R (for both dyes) increased quickly during the first two minutes of contact between the two phases. This refers to the plentiful accessibility of active sites on the sorbent. After that, the %R reaches steady state after 10 min and the sorption process becomes

less effective due to the regular occupancy of the active sites [42].

Each the constants and model parameters values were calculated and provided in Tables (2, 3) and Fig. 3(c-f). The information obtained shows that the pseudo-first-order fail to represent this test because of the low agreement between experimental & theoretical adsorption capacity q$_e$, additionally, the low values of R^2. This confirms that the model was unsuitable for determining the s-soil kinetics. On the other hand, pseudo-second-order model R^2 values declare that the adsorption procedure followed the kinetics of pseudo-second-order model at initial dye concentrations. Moreover, the data demonstrate that the adsorption of dyes onto the adsorbent surface following
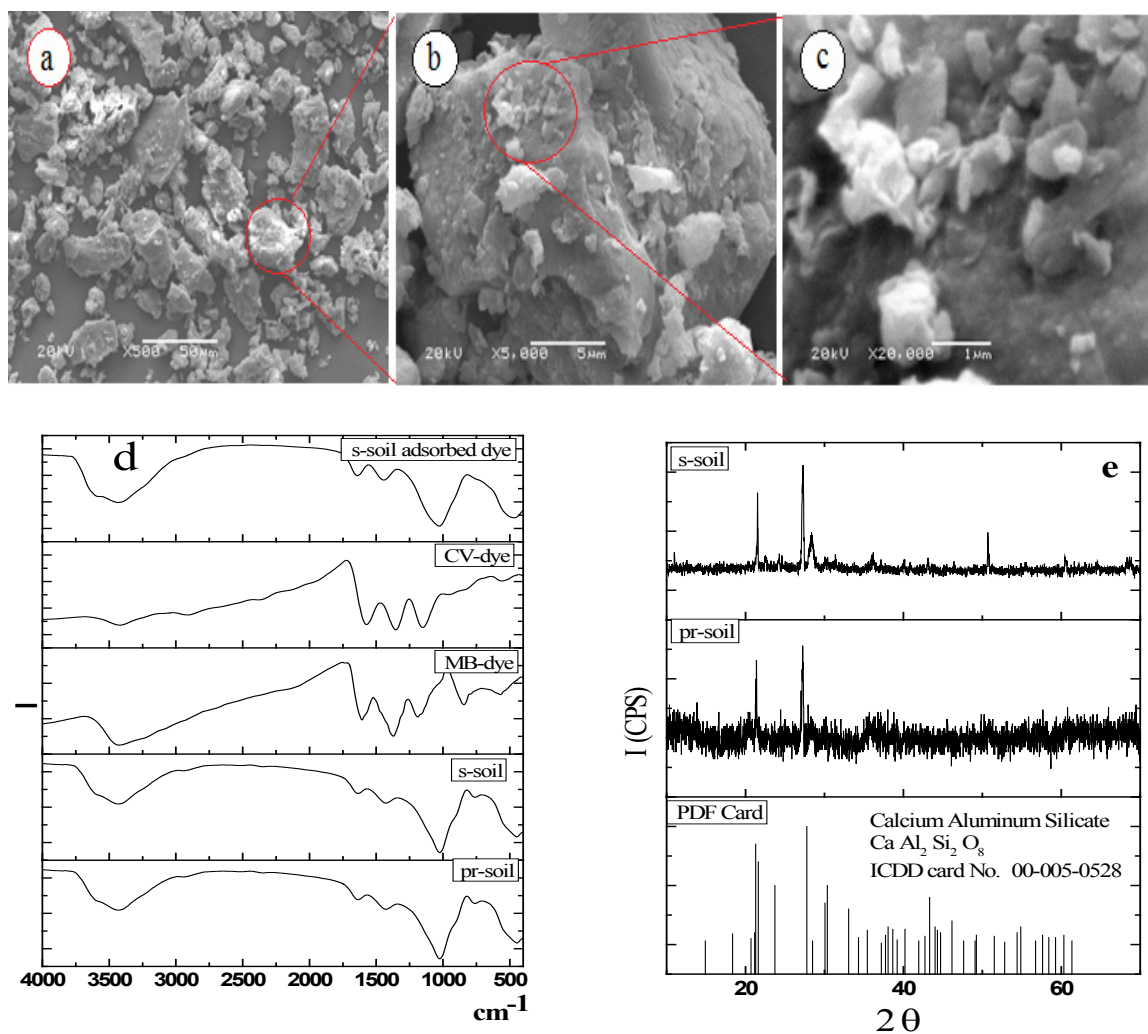
Fig. 2. SEM images of s-soil (a-c) at different magnification, (d) FTIR spectrum of pr-soil and s-soil, and (e) XRD diffraction patterns of pr-soil and s-soil.

TABLE 2. Pseudo-First-order and Second-order kinetic models for dye various concentration.

Dye	Concentration (ppm)	$q_{e\,exp}$ (mg g⁻¹)	First-order kinetic parameter			Second-order kinetic parameter		
			K_{ads} (min⁻¹)	$q_{e\,cal}$ (mg g⁻¹)	R^2	K_{ads} (g mg⁻¹min⁻¹)	$q_{e\,cal}$ (mg g⁻¹)	R^2
MB	100	19.80	-6.90	3.60	0.866	4.53	20.00	0.997
	200	36.03	-0.51	12.88	0.952	0.20	37.03	0.990
	300	45.02	-0.32	16.60	0.852	0.12	45.45	0.993
	400	44.24	-0.51	17.00	0.805	0.14	45.45	0.992
	500	46.86	-0.28	13.80	0.695	0.13	47.62	0.994
CV	100	19.6	-2.23	3.80	0.880	0.71	20.00	0.996
	200	32.24	-0.46	33.88	0.910	0.24	33.33	0.995
	300	35.7	-0.37	11.22	0.710	0.56	35.71	0.999
	400	32.97	-0.44	14.45	0.570	0.37	34.48	0.996
	500	37.28	-0.12	9.77	0.170	0.19	37.04	0.997

TABLE 3. Calculated equilibrium constants for adsorption of MB and CV on s-soil.

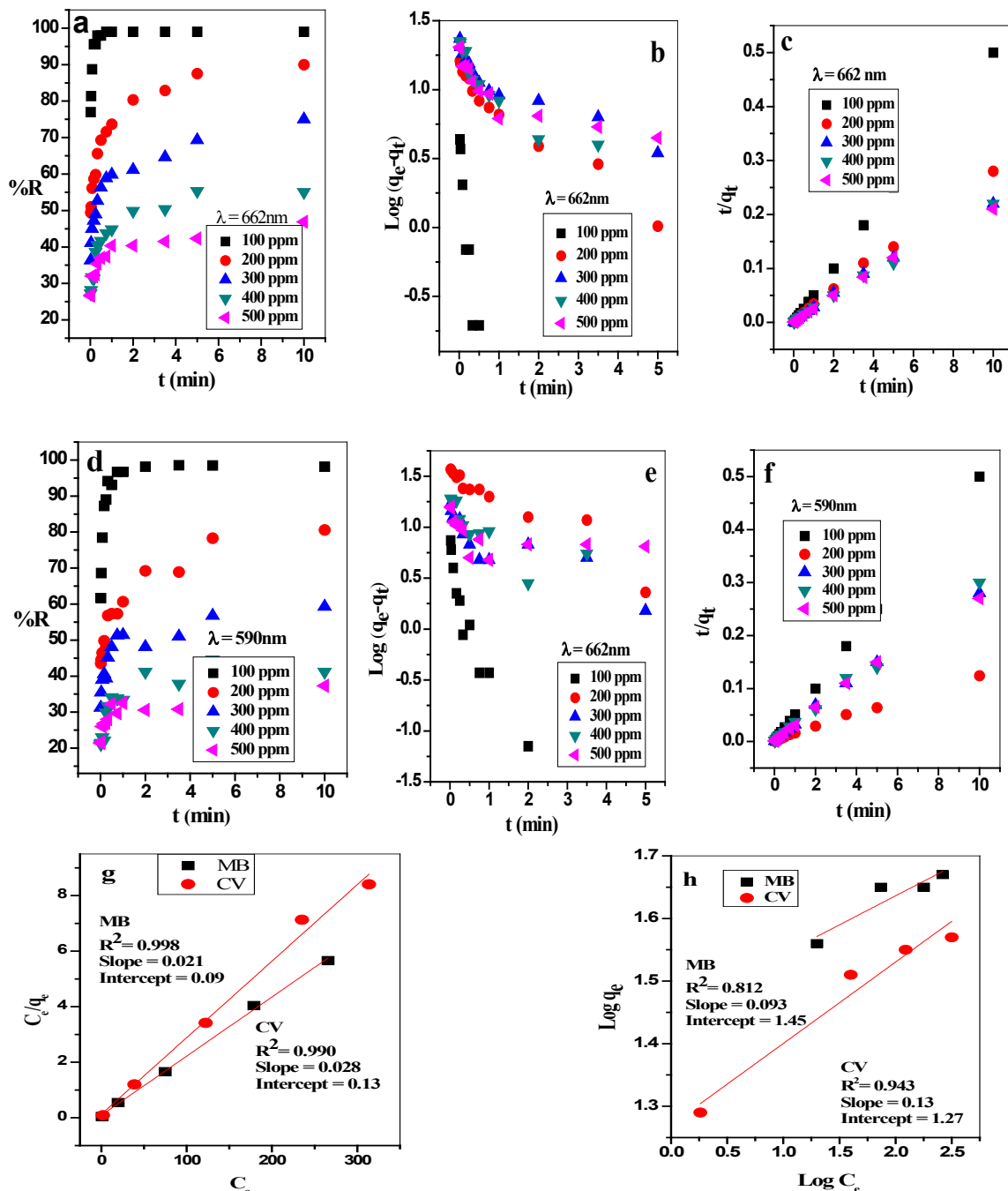| Dye	Langmuir isotherm model				Freundlich isotherm model		
	q^o (mg g^{-1})	b (mg^{-1})	R_L	R^2	1/ n	K_f (mg g^{-1})	R^2
MB	47.62	0.23	0.042	0.99	0.093	4.26	0.97
CV	35.71	0.22	0.043	0. 99	0.13	3.56	0.99

Fig. 3. Effect of MB and CV dyes concentration on (a, d) dye removal percent (%R); (b, e) pseudo-First-order kinetic model; (c, f) pseudo-Second-order kinetic model, respectively; (g) Langmuir and (h) Freundlich model (s-soil dose = 0.1g/20 ml, pH = 7 and T = 25 °C).

a pseudo-second-order reaction as q_e values (experimentally) are in conformity with the q_e values (calculated). Furthermore, the k_{ads} values (pseudo-second-order rate constant) were reduced by increasing concentration of absorbing dye in solution suggesting an absorption rate decreasing. This is apparently owing to the fast growth of positive charge on the surface - for initial uptake- of the dye on the surface of adsorbent, which prevents more dye uptake at the subsequent steps of reacting by columbic repulsion force. Almost these results designated that s-soil can be utilized to eliminate the dye successfully from solutions through monolayer mechanism.

Moreover, the dyes adsorption equilibrium isotherm was calculated (Tables 2, 3). The tables illustrate that the ultimate adsorption for MB and CV onto s-soil from binary solution were 47.62 and 35.71 mg g^{-1}, respectively. Also, the

adsorption process of these dyes was founded to be fitted by the Langmuir model. In conclusion, the monolayer adsorption process happens onto the adsorbent surface and these agree with other work [43].

The R_L (separation parameter) was: 0.042 (for MB) and 0.043 (for CV) for the initial concentration of dyes (100–500 ppm). Those values are designating their favorable adsorption upon adsorbent as it is within the range of 0–1. The $1/n$ numerical values are 0.13 and 0.09 for CV and MB, respectively. However, those values are less than the unit, which strongly supported favorable adsorption by the adsorbent overall studied adsorbent concentration.

Soil dose effect
CV&MB removal percent from the water solution in the binary system form was also investigated using different amounts of adsorbent.
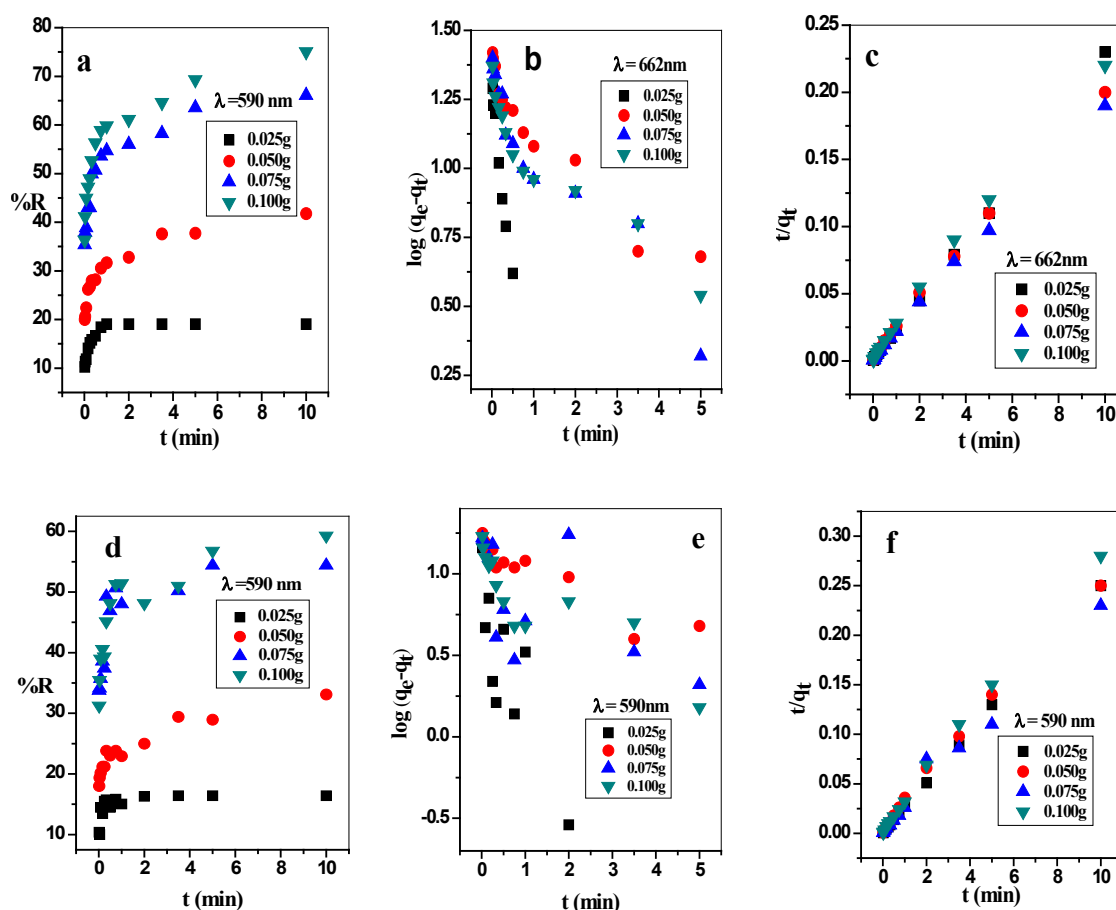

Fig. 4. **Effect of dose concentration (g/20ml) on adsorption process for both dyes MB and CV, (a, d) dye removal percent (%R); (b, e) pseudo-First-order kinetic model; (c, f) pseudo-Second-order kinetic model, respectively (dye concentration = 300 ppm, pH = 7 and T = 25 °C).**

The removal process is highly affected by the amount of the contacting sorbent in the aqueous phase [44]. Figure 4(a, d) illustrates that removal percent of the dyes rapidly increased by increasing the adsorbent dose for both dyes at the first 2 min. After that %R reach steady state and this agreement with another work [45].

The acquired R^2 values (correlation coefficients) for the linear plot of t/qt versus t of pseudo-second-order equation for the dyes (Fig. 4 b, e) greater than that belongs to the pseudo-first-order (Fig. 4 c, f). It was found that the adsorption kinetics were better fitted by pseudo-second-order kinetic model. In addition, Table 4 demonstrates that the q_e values (experimental) agree totally with the calculated q_e values. This indicates that the adsorption process –on s-soil- for both dyes follows the second-order kinetics.

Initial pH effect

Figure 5(a,d) introduce the removal percent of both dyes at different pH. The results prove that R% increase quickly within the first 2 min and appears to be constant after this time for all the solution pH values. Dyes adsorption increases at pH values 3.7 and 7 while a decrease in pH values 2 and 8.7. Minor adsorption of CV and MB at an acidic pH may be referred to the existence of excess H^+ ions occupying the adsorbent active sites which preventing adsorption of the dye [46]. In addition, the above behaviour can come from the electric layer polarity change on both the silica and alumina contents of the clay from positive to negative charge. These changes improve cationic dye removal from its aqueous solution by attracting the dye cations. Furthermore, the

hydroxylated oxides acid-base dissociation of the clay followed by ion exchange with the dye cations could be responsible for the maximum removal of the cationic dye from its solution. Above pH 7, the density of negative charge on the surface of the adsorbent decreased, this led to a slow decline in the clay removal ability. Yet, between pH values 3.5 and 7, the removal percent nearly the same indicates that the presence of high concentrations of hydronium ions does not influence the kinetics of adsorption and consequently, the removal is at its maximum.

Figure 5(b,e) and 5(c,f) represent plotting of the pseudo-first-order and pseudo-second-order adsorption kinetic models at various pH values for both CV and MB dyes, respectively. The calculated correlation coefficients and kinetic parameters were obtained are listed in Table 5. The table and figure data demonstrated that pseudo-second-order adsorption kinetic models fitted well with the experimental data depending on calculated R^2 (> 0.990) and q_e values.

(b, e) pseudo-First-order kinetic model; (c, f) pseudo-Second-order kinetic model, respectively

Temperature effect

Figure 6 displays the temperature effect on the MB and CV adsorption on the adsorbents. It can be seen that uptake percent increases rapidly at earlier steps of adsorption and the removal percent reaches to equilibrium overall temperature values.

Figure 6 (b,e) and 6 (c,f) display the linear relation of pseudo-first-order and pseudo-second-order adsorption kinetic models for CV and MB dyes, respectively. Table 6 illustrates the calculated values of q_e and R^2. The obtained R^2 values

TABLE 4. Calculated parameters of the pseudo First-order and pseudo Second-order kinetic models for various s-soil doses.

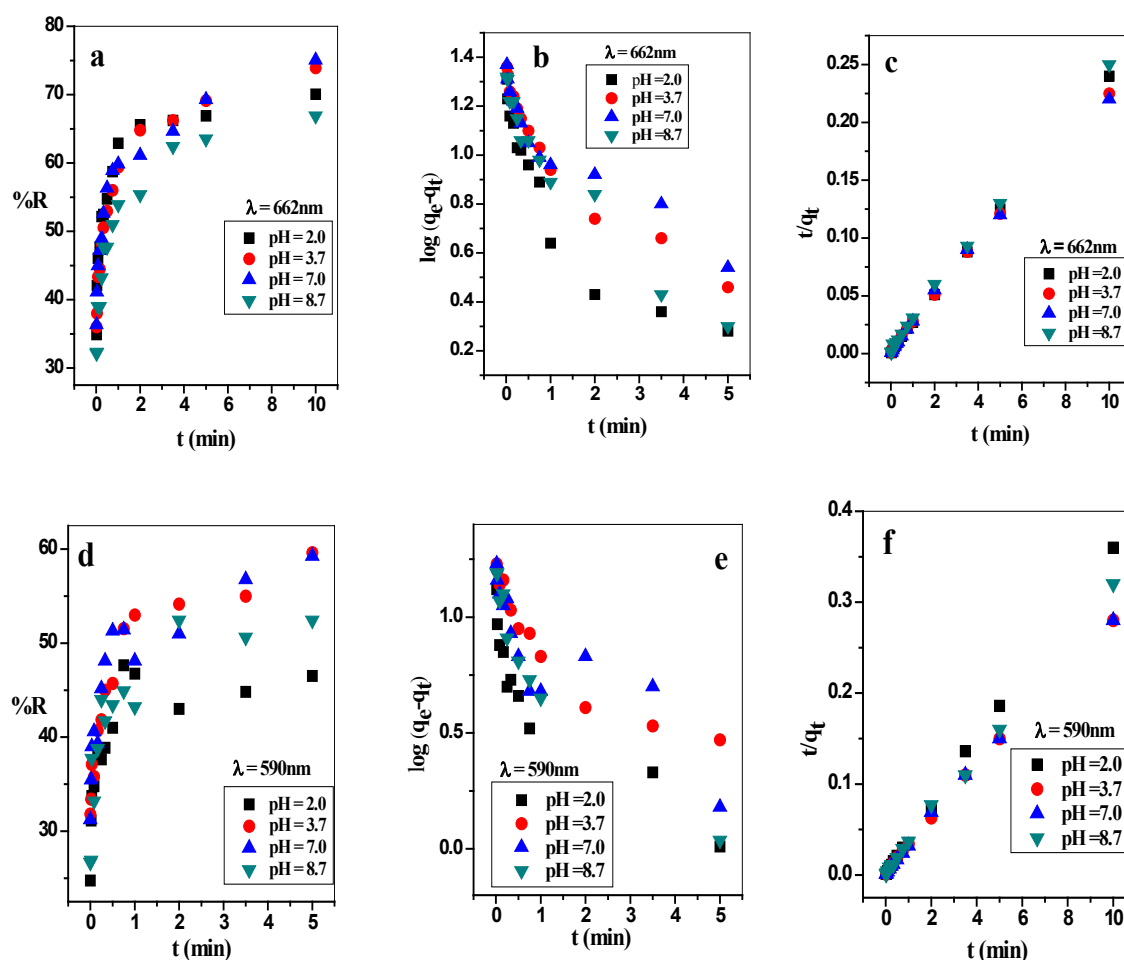| Dye	Adsorbent dose (g)	$q_{e\,exp}$ (mg g^{-1})	First-order kinetic parameter			Second-order kinetic parameter		
			K_{ads} (min^{-1})	$q_{e\,cal}$ (mg g^{-1})	R^2	K_{ads} (g mg^{-1} min^{-1})	$q_{e\,cal}$ (mg g^{-1})	R^2
MB	0.025	44.16	-3.25	19.00	0.978	1.24	43.50	0.999
	0.050	50.11	-0.35	20.40	0.897	0.10	50.00	0.996
	0.075	53.52	-0.41	19.00	0.875	0.15	52.60	0.998
	0.100	45.02	-0.32	16.60	0.852	0.12	45.45	0.995
CV	0.025	39.41	-0.28	14.80	0.856	0.11	40.00	0.994
	0.050	39.60	-0.32	10.72	0.333	0.15	43.50	0.984
	0.075	43.96	-0.37	11.22	0.709	0.19	35.71	0.997
	0.100	35.70	-1.61	7.60	0.658	0.11	40.00	0.999

Fig. 5. Effect of the pH on adsorption process for both dyes MB and CV, (a, d) dye removal percent (%R); (b, e) pseudo-First-order kinetic model; (c, f) pseudo-Second-order kinetic model, respectively (dye concentration = 300 ppm, s-soil dose= 0.1g/20 mL and T = 25 °C).

TABLE 5. Calculated parameters of the pseudo First-order and pseudo Second-order kinetic models for different pH values.

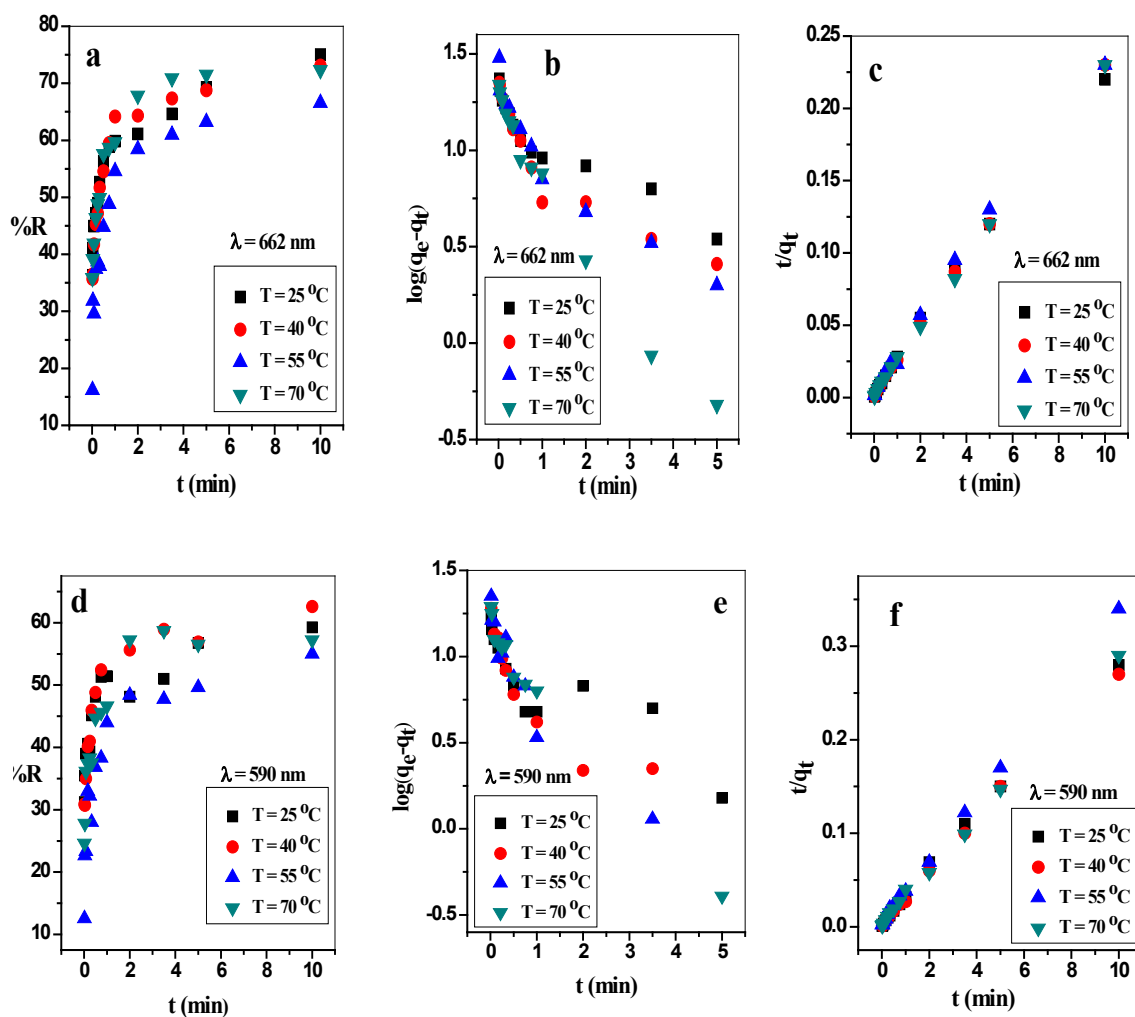| Dye	PH	$q_{e\,exp}$ (mg g^{-1})	First-order kinetic parameter			Second-order kinetic parameter		
			K_{ads} (min^{-1})	$q_{e\,cal}$ (mg g^{-1})	R^2	K_{ads} (g mg^{-1}min^{-1})	$q_{e\,cal}$ (mg g^{-1})	R^2
MB	2	42.05	-0.46	12.60	0.798	0.25	41.70	0.999
	3.7	44.35	-0.39	17.00	0.896	0.14	43.50	0.998
	7	45.02	0. 32	17.00	0.852	0.12	45.45	0.995
	8.7	40.13	-0.46	16.22	0.932	0.14	40.00	0.998
CV	2	27.91	-0.39	7.24	0.803	0.17	35.71	0.998
	3.7	35.92	-0.35	12.60	0.837	0.20	35.71	0.997
	7	35.70	-0.37	11.22	0.709	0.33	31.25	0.998
	8.7	31.47	-0.47	11.00	0.851	0.65	27.78	0.999

Fig. 6. Effect of temperature on adsorption process for both dyes MB and CV, (a, d) dye removal percent (%R); (b, e) pseudo-First-order kinetic model; (c, f) pseudo-Second-order kinetic model, respectively (dye concentration = 300ppm, s-soil dose= 0.1g/20 mL and pH= 7).

TABLE 6. Calculated parameters of the pseudo First-order and pseudo Second-order kinetic models at different temperatures.

Dye	T (°C)	qe_{exp} (mg g^{-1})	First-order kinetic parameter			Second-order kinetic parameter		
			K_{ads} (min^{-1})	$q_{e\,cal}$ (mg g^{-1})	R^2	K_{ads} (g mg^{-1}min^{-1})	$q_{e\,cal}$ (mg g^{-1})	R^2
MB	25	45.02	-0.32	17.00	0.852	0.12	45.45	0.993
	40	43.87	-0.40	13.00	0.811	0.10	43.50	0.999
	55	40.20	-0.47	17.78	0.881	0.13	43.00	0.995
	70	43.39	-0.78	17.00	0.970	0.17	43.50	0.999
CV	25	35.70	-0.37	11.22	0.709	0.20	35.71	0.997
	40	37.56	-0.60	11.23	0.750	0.24	37.00	0.997
	55	29.77	-0.78	13.80	0.851	0.29	29.41	0.999
	70	34.34	-0.71	14.00	0.970	0.23	34.83	0.998

from pseudo-first-order and pseudo-second-order adsorption model are ≤ 0.990 and ≥ 0.990, respectively. Moreover, the calculated values of q_e match highly effective with the experimental data. This suggests that the kinetic modeling of the temperature effect on the adsorption process is more likely fits to the models of the pseudo-second-order adsorption.

Conclusion

In the present study, the settling technique appears to be effective in the fractionation of local soil clay. The crystal violet and methylene blue dyes (in a binary system) successfully removed from aqueous medium over a soil sample (s-soil) fractioned from a local soil sample (pr-soil). The reaction between the dye species and the soil particles show fast adsorption kinetics. Referring to the q_e and R^2 values the pseudo-second-order model more fitted the adsorption kinetics process. According to Langmuir isotherm, the obtained soil can adsorb 47.82 and 35.71 mg g^{-1} for MB and CV. Those results give a promising solution for crystal violet and methylene blue dye removal from wastewater.

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إزالة صبغتى المثيلين الزرقاء و الكريستال البنفسجى (كنظام الثنائى) من المحاليل المائية بإستخدام الطمى المستخلص من التربة المحلية: دراسة حركية و توازنية

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هذه الورقة تعرض إزالة الصبغة الزرقاء و البنفسجية من النظام الثنائي المائي عن طريق الامتزاز على طين التربة المحلية باعتبارها ماده منخفضة التكلفة ومتاحة بكثرة. تم دراسة تأثير مختلف الظروف التجريبية على عمليه الأمتزاز مثل تركيزات الأصباغ، وزن الممتز، درجة الحموضة ودرجة الحرارة. ولتحديد أداء إدمصاص جزيئات الصبغات على طين التربة ، تم تحليل حركية الإمتزاز باستخدام نماذج متعددة مثل نموذج معدل من الدرجة الأولى والثانية. يبين هذا النوع من الدراسة أن الحد الأقصى للامتزاز الذي تم التوصل إليه كان خلال دقيقتين ويستخدم حركية الطلب الزائفة الثانية. وقد تم دراسة متساوي الاضمحلال في نطاق الأس الهيدروجيني من 2 ، 3.7 ، 7 ، و 8.7 عند 25 درجة مئوية وتحليلها مع نموذجين مختلفين هما Langmuir و.Freundlich تم دراسة تفاعل جزيئات الصبغ مع طين التربة بواسطة SEM و EDS و FTIR وXRD. كان الحد الأقصى لازاله الصبغة الزرقاء و البنفسجية هو 47.82 و 35.71 ملغم / غرام ، على التوالي عن طريق امتصاص الصبغات على التربة الطينية. تقدم هذة الطريقة حلاً واعدًا لإزالة الصبغات الزرقاء و البنفسجية من مياه الصرف الصحي.