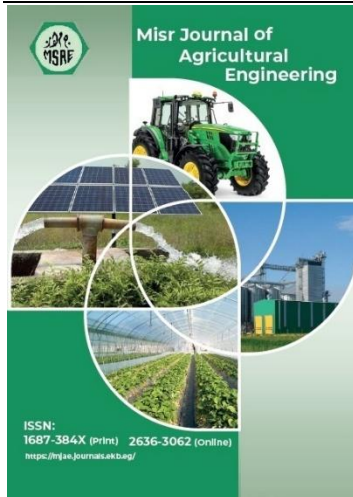


## EXPERIMENTAL MODEL FOR PREDICTING DRAFT AND POWER REQUIREMENTS OF SIMPLE TILLAGE TOOLS

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### Keywords:

Model experimentation,  
draft, power, tillage tools

### ABSTRACT

*The main objective of this study was to perform model experimentation for predicting draft and power requirements of simple tillage tools such as chisel plow. Four tool operating parameters were chosen to be cases for model experimentation. These were tool rake angle (ranged from 15° to 75°), tool depth (ranged from 100 to 300 mm), tool speed (ranged from 0.89 to 1.92 m/s), and tool width (ranged from 100 to 400 mm). Experimentation process was carried out using simulation model modified by Afify et al. (2020) based on Sohne's model, (1956). Validation results of such model showed an acceptable agreement between the test data and the model. The model experimentation was conducted by running a program modified by VB Software using real data as inputs of soil parameters from Afify (1999) and Roza (1997). The soil under these studies was clay soil in terms of soil mechanical analysis. Results of model experimentation showed the model could be predicting draft and power requirements by an accuracy exceeds than 90% for the four examined parameters under this study.*

### 1. INTRODUCTION

Input energy considered one of the important factors affected on the performance efficiency of the tillage tools (Gill and Vanden Berg, 1968). According to the current prices, Egyptian farmers consumed fuel by about 1625 million pounds (108.33 million \$) for tilling 6.5 million hectares (CAPMS, 2019). This estimation based on the average value of fuel need to cultivate one hectare is 35 liters for clay soil by traditional method (Afify et al. 1999). Results of previous studies in terms of power requirements of tillage tools showed that soil cultivating process consumes more than half of the energy needed to grow agricultural products (Abd El Wahed, 2007). This higher energy consumption because of the motion of large amount of soil mass and inefficient methods of energy transfer to the soil (Al-Hamed et al., 2014, and Tong and Moayad, 2006). Modern agriculture practices need a challenge technique to determine energy requirements of tillage tools. Therefore, simulation models are an efficient technique for evaluating the performance of tillage tools. Many researches have been carried out in developing computer-based models and simulation programs for determining energy requirements of tillage tools (Shahgholi et al., 2019; Moenifar et al., 2014; Kheiralla et al., 2004; Al-Hamed et al., 2014; Akbarnia et al., 2014; Abu-Hamdeh et al., 2003; and Abd El Wahed, 2007). On the other hand, few of these studies performed model experimentation

process. The subject of model experimentation is not new and is widespread in fields like natural sciences and economics. Experimentation has also prevailed in literature on strategic role management and transitions management focusing on searching, learning and experimenting for sustainable development (Bocken et al., 2018). Therefore, the main objective of this study was to accomplish model experimentation for predicting draft and energy for tillage tools using four examined tool parameters.

## 2. MATERIALS AND METHODS

### 2.1. Model Development

Under this study, Visual Basic was used as a computer programming language to develop a model based on Sohne's model for simple tillage tools. The effect of soil-tool interaction on predicting draft of tillage tools was investigated. The model is an interactive program where the user is prompted to enter his relevant input data for the model. A set of screens, object buttons, scroll bars, and menus which available at Visual programming were used to design the form. The objects can be positioned on a form, and their behaviors are described through the use of a scripting language associated with each one. The structure of building the model consisted of interrelated screens and tasks arranged in a logical and easily understandable in order to form an integrated and complete unit as showed in Figure (1). A simulation model that has been modified by Afify et al. (2020) was used to perform model experimentation for predicting draft and power requirements. The model was designed for simple tillage tools such as chisel plow as it is the famous plow used under Egyptian conditions.

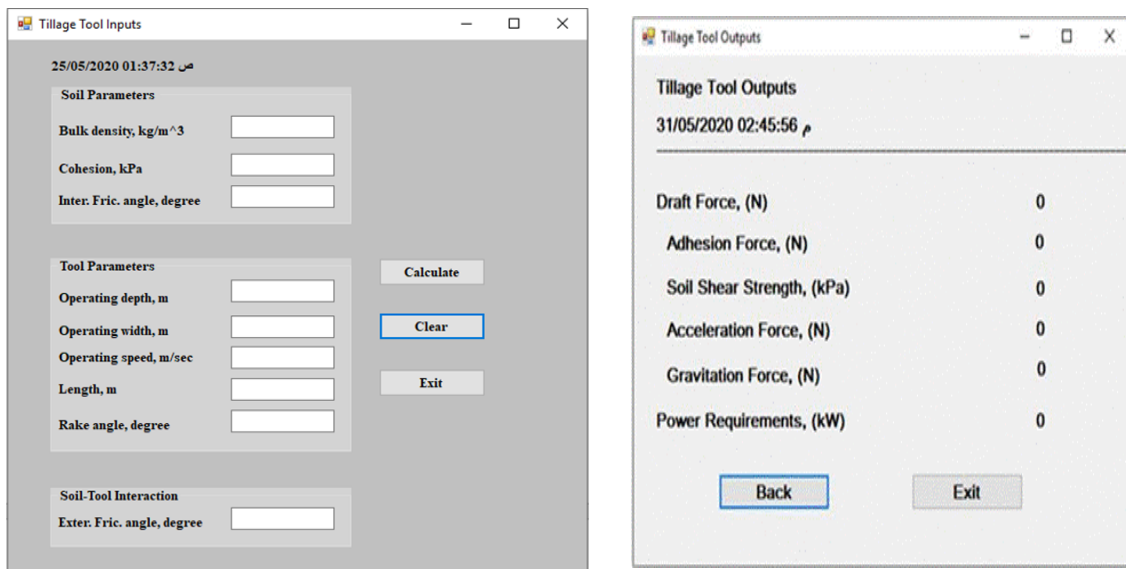


Figure (1): Screenshots for input and output interfaces of the modified program for predicting draft force.

The draft under such model was predicting through calculating the forces resulting from soil-tillage tool interactions based on Sohne's model. All variables were defined using the Visual Basic language to calculate the draft and consequently, power requirements. After creating the procedures and functions, equations from mathematical analysis of Sohne's model were used to calculate the draft. However, the predicting power requirements of tillage tools was estimated based on draft and tool speed using equation of ASAE, (1998). The verifying procedure was carried out using data from previous studies available in literature (Akbarina et al., 2014;

Ibrahmi et al., 2014; Ucgul et al., 2014; Fielke, 1988; Zang et al., 2018; Moeenifar et al., 2014). Results of validation showed an acceptable agreement between the test data and the model.

**2.2. Model Experimentation**

Implementation test of any model involves three basic steps. These were desk-checking, debugging, and running real-experimental data to make sure that the model works. These three steps must be conducted to make sure that is realistic works and it’s free of errors. Model experimentation performed in order to improve the precision of the results and to limit the model constraints for any examined parameters. Therefore, in this study, the model experimentation was conducted by running a program using real data from Afify (1999) and Roza (1997). Table (1) illustrates the data used as inputs of soil parameters for model experimentation through running the program of modified model. The soil under these studies was classified as clay soil. It has 45.35% clay, 30.65% silt, and 24.0% sand.

Table (1): Some physical and mechanical properties of clay soil used as inputs data (Roza, 1997, and Afify, 1999).

Moisture content (%)	Buck density (Mg/m <sup>3</sup> )	Soil cohesion (kPa)	Internal friction angle (deg.)	Soil-metal friction angle (deg.)
	1.30	14.13	36.2	24
10	1.35	15.82	37.6	24
	1.41	19.96	39.8	23.9
	1.38	10.15	28.1	23.8
15	1.45	12.91	29.8	23.7
	1.52	13.43	31.5	23.7
	1.48	6.81	21.3	23.8
20	1.56	7.71	23.2	23.6
	1.66	9.31	25.3	23.5

**3. RESULTS AND DISCUSSION**

**3.1. Model Experimentation for Draft**

Figures from (2) to (5) present predicting draft under various levels of tool rake angle, tool depth, tool speed, and tool width, respectively. The effect of tool rake angle on predicting draft at different tool depths and at (1.38 m/s tool speed, 300 mm tool width, 15% moisture content, and 12.91 kPa soil cohesion) is shown in Figure 2. Results indicated that the increase in tool rake angle caused increasing in predicting draft for various tool depths. The change in the tool rake angle from 15° to 75° produced increasing in the predicting draft by 93%, 87%, 71%, 58%, and 42% for tool depths of 100, 150, 200, 250, and 300 (mm), respectively. Correlation coefficient for predicting draft with different levels of tool rake angles was 0.85 as polynomial function. These results are similar to the results obtained by Ucgul et al. (2014), and Hamied (2016).

The effect of tool depth on predicting draft at different tool speeds and at (45° tools rake angle, 300 mm tool width, 15% moisture content, and 12.91 kPa soil cohesion) is shown in Figure 3. The highest values of predicting draft were obtained with tool depth of 300 mm. However, the lowest vales were resulted with the tool depth of 100 mm under various tool speeds. The change in the tool depth from 100 to 300 mm resulted in increasing of the predicting draft by 95%, 92%, 64%, 69%, and 76% for

tool speeds of 0.89, 1.11, 1.38, 1.67, and 1.67 m/s, respectively. Correlation coefficient for predicting draft with tool rake angle was 0.90 as polynomial function. These results are in agreement with pervious results obtained by Akbarnia et al., (2014), Ucgul et al., (2014), and Ibrahim et al., (2014). The effect of tool speed on predicting draft under different levels of tool depths and at (rake angle of 45°, tool width of 300 mm, 15% moisture content, and 12.91 kPa soil cohesion) is showed in Figure 4. The change in the tool speed from 0.89 to 1.92 m/s resulted in increasing of the predicting draft by 94%, 78%, 82%, 65%, and 73% for tool depths of 100, 150, 200, 250, and 300 (mm), respectively. Correlation coefficient for predicting draft with tool speed was 0.92 as polynomial function. These results are in agreement with pervious findings by Aboukarima, (2007), Zang et al., (2018), and Moenifar et al., (2014).

The effect of tool width on predicting draft under different levels of tool depths and at (45° of rake angle, tool speed of 1.39 m/s, 15% moisture content, and 12.91 kPa soil cohesion) is shown in Figure 5. The change in the tool width from 100 to 400 mm resulted in increasing of the predicting draft by 86 %, 85%, 83%, 68%, and 55% for tool depths of 100, 150, 200, 250, and 300 mm, respectively. Correlation coefficient for predicting draft with tool with was 0.96 as polynomial function. These results agreed with pervious results obtained by Ucgul et al., (2014), Ibrahim et al., (2014), Aboukarima, (2007), Zang et al., (2018), and Moenifar et al., (2014).

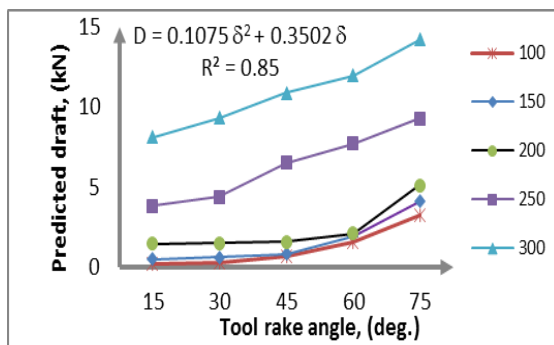


Figure 2. Predicting draft with rake angles under different depths.

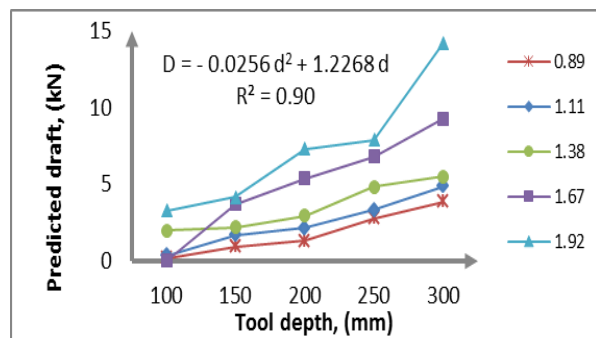


Figure 3. Predicting draft with tool depths under different speeds.

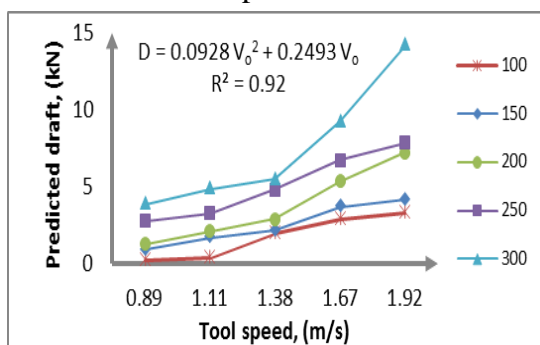


Figure 4. Predicting draft with speeds under different depths.

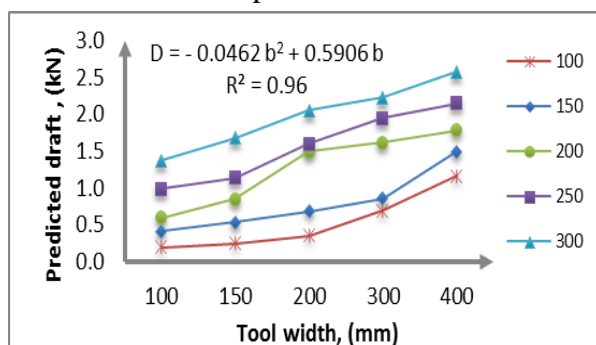


Figure 5. Predicting draft with tool widths under different depths.

Multi-regression analysis was performed for the data in Table (2) to driven a general relation between predicting the draft force with the examined parameters. The derived equation is:

$$D = 1.63 b + 2.13 \delta + 2.8 V_0 + 2.3 d \quad (R^2 = 0.91)$$

Where:

D = draft, (kN), b = tool width, (m),  $\delta$  = tool rake angle, (deg.),  $V_o$  = tool speed, (m), and d = tool depth, (m).

Analysis of variance (Table 3) for predicting draft force with the four examined parameters could be summarized as the following:

- There were highly significant differences of predicting draft with relation to tool rake angle, tool depth, and tool speed. However, it was only significant with tool width.
- LSD test indicated that there were significant in the mean differences of predicting draft with the different levels of tool rake angles and tool depths. However, there was none significant with tool speeds and tool widths as shown in Table (4).

Table (2): Predicting draft with different levels of tool rake angles, tool depths, tool speeds, and tool widths at (15% moisture content and 12.91 kPa soil cohesion).

Depth (mm)		100	150	200	250	300
		Draft (kN)				
Width (mm)	100	0.19	0.41	0.59	0.98	1.37
	150	0.24	0.53	0.84	1.13	1.67
	200	0.35	0.68	1.49	1.59	2.05
	300	0.69	0.85	1.61	1.94	2.22
	400	1.16	1.49	1.78	2.14	2.57
Rake angle (deg.)	15	0.20	0.52	1.48	3.85	8.14
	30	0.30	0.66	1.51	4.41	9.32
	45	0.68	0.85	1.61	6.54	10.87
	60	1.57	1.97	2.14	7.73	11.96
	75	3.25	4.14	5.11	9.28	14.21
Speed (m/s)	0.89	0.18	0.90	1.28	2.77	3.85
	1.11	0.35	1.68	2.13	3.30	4.86
	1.38	1.96	2.17	2.91	4.82	5.48
	1.67	2.86	3.68	5.35	6.76	9.23
	1.92	3.28	4.15	7.26	7.87	14.2

Table (3): Analysis of variance for predicting draft force with respect to tool rake angles and tool depths.

Source	Sum of Squares	D.F	Mean Square	F	Sig.
Corrected model	632.443	16	39.528	12.465	0.00
Intercept	64.342	1	64.342	20.290	0.00
Rake	80.880	4	20.220	6.376	0.00
Depth	320.601	4	80.150	25.275	0.00
Speed	117.043	4	29.261	9.227	0.00
Width	33.027	4	8.257	2.604	.045
Error	183.925	58	3.171		
Total	1624.167	75			
Corrected Total	816.368	74			

Table (4): LSD test for predicting draft with tool rake angles and tool depths.

(I) rake	(J) rake	Mean Difference (I-J)	(I) Depth	(J) depth	Mean Difference (I-J)
30	45	-528.9524*	100	200	-430.1111*
	60	-526.6667*		300	-904.3333*
45	30	528.9524*	200	100	430.1111*
	60	2.2857		300	-474.2222*
60	30	526.6667	300	100	904.3333*
	45	-2.2857		200	474.2222*

\*The mean difference is significant at the .05 level.

### 3.2. Model Experimentation for Power Requirements

Figures from (6) to (9) show predicting power requirements under various levels of tool rake angles, tool depths, tool speeds, and tool widths, respectively. The effect of tool rake angle on predicting power requirements at different tool depths and at (1.38 m/s tool speed, 300 mm tool width, 15% moisture content, and 12.91 kPa soil cohesion) is shown in Figure 6. The highest values of predicting power requirements were obtained at the tool rake angle of 75° under various tool depths.

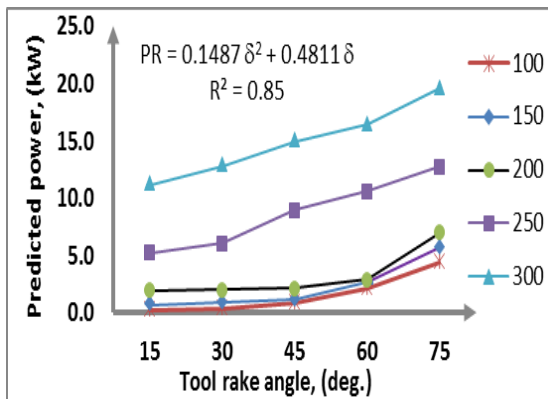


Figure 6. Predicting power with rake angles under different depths.

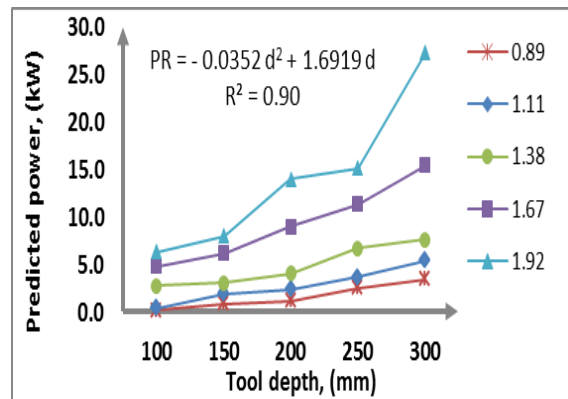


Figure 7. Predicting power with tool depths under different speeds.

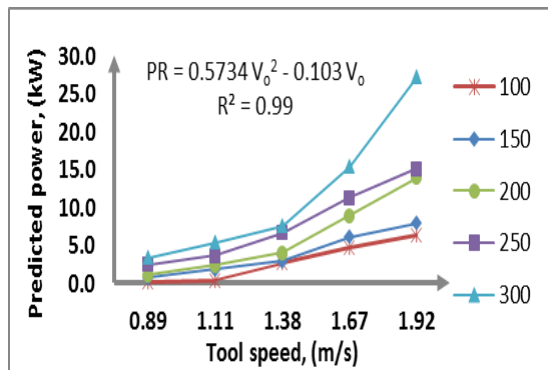


Figure 8. Predicting power with speeds under different depths.

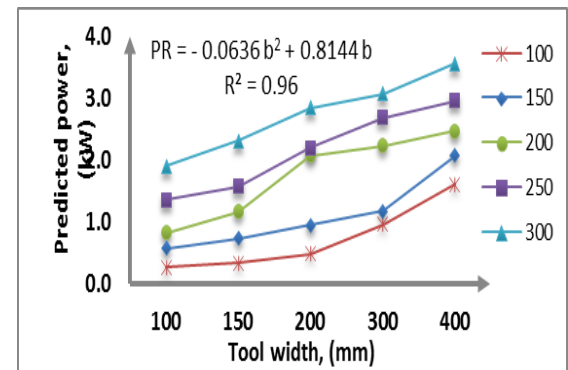


Figure 9. Predicting power with tool widths under different depths.

However, the lowest values were obtained with the tool angle of 15°. At tool rake angle of 45°, the power requirements increased by 20%, 47%, 76%, and 40% as the tool depths changed from 100 to 150 mm, 150 to 200 mm, 200 to 250 mm, and 250 to 300 mm, respectively. Correlation coefficient for predicting power requirements with tool rake angle was 85% as polynomial function. These results are in agreement with previous findings by Moeenifar et al., (2014), Akbarnia et al., (2014), Aboukarima, (2007), and Zang et al., (2018).

The effect of tool depth on predicting power requirements at different tool speeds and at (45° tools rake angle, 300 mm tool width, 15% moisture content, and 12.91 kPa soil cohesion) is shown in Figure 7. It indicated that the increase in tool depth from 100 mm to 300 mm resulted in increasing of predicting power requirements by about 96%, 93%, 65%, 69%, and 77% for tool speeds of 0.89, 1.11, 1.38, 1.67, and 1.92 m/s, respectively. At high level of tool depth, the predicting power requirements increased by 27%, 29%, 51%, and 44% when the tool speed changed from 0.89 to 1.92 m/s.

Correlation coefficient for predicting power requirements with tool depth was 90% as polynomial function. These results are in agreement with pervious findings by Akbarnia et al. (2014), Aboukarima, (2007), Zang et al., (2018), and Moeenifar et al., (2014).

The effect of tool speed on predicting power requirements under different levels of tool depths and at (rake angle of 45°, tool width of 300 mm, 15% moisture content, and 12.91 kPa soil cohesion) is showed in Figure 8. Results showed similar trends as with tool depths. The increase in tool speed from 0.89 to 1.93 m/s resulted in increasing in the power requirements by 97%, 90%, 92%, 84%, and 88% for tool depths of 100, 150, 200, 250, and 300 mm, respectively. Correlation coefficient for predicting power requirements with tool speed was 99% as polynomial function. These results are in agreement with pervious findings by Akbarnia et al. (2014), Aboukarima, (2007), Zang et al., (2018), and Moeenifar et al., (2014).

The effect of tool width on predicting power requirements under different levels of tool depths and at (45° of rake angle, tool speed of 1.39 m/s, 15% moisture content, and 12.91 kPa soil cohesion) is shown in Figure 9. The increase in tool width caused an increase in the predicting power requirements under different tool depths. The percentage changes in the predicting power requirements with different tool widths were 86%, 85%, 83%, 69%, and 45% as the tool depths increased from 100 to 300 mm. Correlation coefficient for predicting power requirements with tool width was 96% as polynomial function. These results are in agreement with pervious findings by Akbarnia et al. (2014), Aboukarima, (2007), Zang et al., (2018), and Moeenifar et al., (2014).

Multi-regression analysis was performed for the data in Table (5) to driven a general relation between predicting power requirements with respect to examined parameters. The derived equation is:

$$PR = 3.1 b + 2.82 \delta + 4.7 V_o + 4.12 d \quad (R^2 = 0.90)$$

Where:

PR = power requirements, (kW), b = tool width, (m),  $\delta$  = tool rake angle, (deg.),  
 $V_o$  = tool speed, (m), and d = tool depth, (m).

Analysis of variance (Table 6) for predicting power requirements with respect to tool rake angles, tool depths, tool speeds, and tool widths could be summarized as the following:



- There were highly significant differences of predicting power requirements with relation to tool rake angle, tool depth, and tool speed. However, it was none significant with tool width.
- LSD test indicated that there were significant in the mean differences of predicting power requirements with the different levels of tool rake angles, tool speeds, and tool widths. However, there was none significant with tool depths as shown in Table (7).

Table (5): Predicting power requirements from running the program of modified model with different levels of tool rake angles, tool depths, tool speeds, and tool widths at (15% moisture content and 12.91 kPa soil cohesion).

Depth (mm)	100	150	200	250	300	
	Power requirements (kW)					
Width (mm)	100	0.26	0.57	0.81	1.35	1.89
	150	0.33	0.73	1.16	1.56	2.30
	200	0.48	0.94	2.06	2.19	2.83
	300	0.95	1.17	2.22	2.68	3.06
	400	1.60	2.06	2.46	2.95	3.55
Rake angle (deg.)	15	0.28	0.72	2.04	5.31	11.23
	30	0.41	0.91	2.08	6.09	12.86
	45	0.94	1.17	2.22	9.03	15.00
	60	2.17	2.72	2.95	10.67	16.50
	75	4.49	5.71	7.05	12.81	19.61
Speed (m/s)	0.89	0.16	0.80	1.14	2.47	3.43
	1.11	0.39	1.86	2.36	3.66	5.39
	1.38	2.70	2.99	4.02	6.65	7.56
	1.67	4.78	6.15	8.93	11.29	15.41
	1.92	6.30	7.97	13.94	15.11	27.26

Table (6): Analysis of variance of predicting power requirements with respect to rake angles, depths, speeds, and widths.

Source	Sum of Squares	D.F	Mean Square	F	Sig.
Corrected model	1643.916	16	102.745	13.547	0.000
Intercept	163.051	1	163.051	21.499	0.000
Rake	154.117	4	38.529	5.080	0.001
Depth	657.632	4	164.408	21.678	0.000
Speed	583.092	4	145.773	19.221	0.000
Width	62.884	4	15.721	2.073	0.096
Error	439.878	58	7.584		
Total	3810.355	75			
Corrected Total	2083.794	74			



Table (7): LSD test for predicting power requirements with tool rake angles and tool speeds.

(I) rake	(J) rake	Mean Difference (I-J)	(I) speed	(J) speed	Mean Difference (I-J)
30	45	-528.9524*	1.10	1.39	-.6022
	45	-.6667		1.67	-1.7067*
45	60	-1.8222*	1.39	1.10	.6022
	30	.6667		1.67	-1.1044*
60	60	-1.1556*	1.67	1.10	1.7067*
	30	1.8222*		1.39	1.1044*

\*The mean difference is significant at the .05 level.

#### 4. CONCLUSION

Model experimentation for predicting draft and power requirements of simple tillage tools was carried out based on Sohne's model. Four tool operating parameters were chosen to be cases for model experimentation. Experimentation process was carried out using simulation model modified by Afify et al. (2020). It was also performed through running the modified program using real data as inputs of soil parameters. Results of model experimentation may be summarized as the following:

- The model could be predicting draft and power requirements by accuracy of more than 90% for the four examined parameters.
- Correlation coefficient of both predicting draft and power requirements with respect to examined parameters were 85%, 90%, 99%, and 96% for rake angle, tool depth, tool speed, and tool width, respectively.
- There were highly significant differences of predicting draft and power requirements with respect to all examined parameters.
- There were significant in the mean differences of predicting draft and power requirements with the different levels of the examined parameters using LDS test.
- General equations were derived between predicting draft and power requirements with the different examined parameter.

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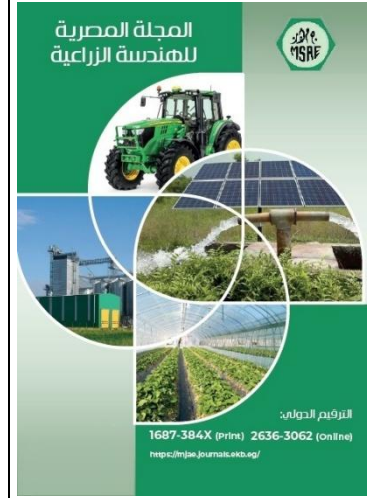
## نموذج تجريبي للتنبؤ بقوة الشد ومتطلبات القدرة لمعدات الحراثة البسيطة

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<sup>1</sup>مدرس بقسم هندسة النظم الزراعية والحيوية - كلية الزراعة - جامعة بنها - مصر.

### الملخص العربي

إن الهدف الرئيسي من هذه الدراسة هو إجراء نمذجة تجريبية للتنبؤ بقوة الشد والقدرة المطلوبة لأسلحة الحراثة البسيطة مثل اسلحة المحراث الحفار الأكثر استخداما في الزراعة المصرية. وقد تم إختيار أربعة عوامل للتشغيل لتكون حالات دراسية للنمذجة التجريبية (زاوية الميل لسلاح معدة الحراثة Rake angel - عمق التشغيل لمعدة الحراثة Tool depth - سرعة التشغيل لمعدة الحراثة Tool speed - عرض التشغيل لمعدة الحراثة Tool width). كما تم إجراء النمذجة التجريبية باستخدام نموذج محاكاة معدل بواسطة (Afify et al., 2020) باستخدام برنامج VB ومستندا إلى نموذج (Sohne, 1956) Sohne's model. كما تم تنفيذ النمذجة التجريبية من خلال تشغيل البرنامج لنموذج المحاكاة الذي تم تطويره باستخدام بيانات حقيقية من نتائج تجارب سابقة كمدخلات للعوامل تحت الدراسة. وكانت أهم النتائج التي تم التوصل إليها أنه يمكن للنموذج التنبؤ بقوة الشد Daft Force ومتطلبات القدرة Power Requirements بدقة وصلت إلى أكثر من ٩٠% للعوامل الأربعة التي تم استخدامها تحت الدراسة كما كان معامل الارتباط Correlation Coefficient لكل من قوة الشد ومتطلبات القدرة بالنسبة للعوامل تحت الدراسة كانت قيمته ٨٥٪، ٩٠٪، ٩٩٪، و ٩٦٪ لكلا من زاوية الميل لسلاح معدة الحراثة، عمق التشغيل لمعدة الحراثة، سرعة التشغيل لمعدة الحراثة، عرض التشغيل لمعدة الحراثة على الترتيب. كما تم استنباط معادلات تجريبية باستخدام برنامج SPSS Software يمكن استخدامها عند تصميم معدات الحراثة لتقدير كلا من قوة الشد والقدرة المطلوبة لأسلحة معدات الحراثة البسيطة مثل المحراث الحفار.



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### الكلمات المفتاحية:

نموذج تجريبي، قوة الشد، متطلبات القدرة، معدات الحراثة