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Blade Optimization Approach for a Vertical Wind Turbine

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Abstract: Harvesting electrical power from wind energy is a feasible solution for the issue of abundance energy. Blade is the wind turbines performance key. The research considered the design and optimization issue of blade's structure made from composite material. Genetic algorithm used as an optimization tool for defining different parameters in the blade fibre and matrix materials, fibre orientations, layer thickness, and number of layers for blade crosssection. Building an efficient genetic algorithm requires a good representation to the phenomenon through an appropriate definition of the fitness function. The presented approach aim to optimize the blade deign against different loads such as aerodynamic, inertia, and operating couples. Material model predicate all properties in principal directions. Force model analyze all external force-couple system. Stress and failure model evaluate all stress condition then check their values against material strength. Failure criterion determines whether the proposed model is safe or not. All these parameters embedded into single fitness function to decide whether this model would replace one of the preceding generation or not. New design parameters produced through crossover, mutation, and replacement processes until the algorithm converges. The results form presented approach is a design benchmark for blade material design and selection process.

Keywords: wind turbine blade, composite materials, genetic algorithm.

Introduction

The vertical wind turbines blade is designed to support air and centrifugal loads. Hence, mathematical equations are derived to describe shape parameters, stress analysis, and failure analysis. After that, a representation for the mathematical model in the form of genetic algorithm, while handling the mixed integer parameter issue in the programming. Consequently, the fitness evaluation model overcomes this problem by using index material selection and continues parameters as dimensions and number of layers.

Optimization decision parameters have the behaviour of integer programming. Parameters include index for selected reinforcement material, matrix material, orientation of reinforcement, number of layers, volume fraction, and width of core box. Genetic algorithm generates random values for those parameters, and then they fed into evaluation model for the objective function that includes the mechanical model evaluating failure conditions. The fitness value used in reproducing new offspring, first by selecting fitter designs, then crossover and mutates the selected designs; finally, a new population is then created. Algorithm is repeated until changes in fitness value stall.

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Ladson and Brooks in 1975 started the first step to compute and draw the NACA cross section using computer based program [1]. They introduced a systematic equations to relate the shape with *x* and *y*-axis. In addition to, other shape parameters were related too such as camber location, maximum thickness of airfoil, and there relation to chord length. 2013 Manikandan and Stalin [2].

The issue of blade design and selection related not only to the shape geometry, yet for aerodynamics and force analysis. In 2014, Vulloju, M.Kumar, E. Kumar, and K. Reddy introduced a direct approach for estimating the forces acting the blade induced from the solid to fluid flow interactions. [3]

Before the previous article with one month, another article published by M.R. Saber, M.H. Djavaraeshkian introducing the same concept the impact of blade design on the wind turbine performance. The analysis used genetic algorithm as optimization technique for the blade shape; optimum blade shape was E387 Eppler. A comparison was carried out between optimum shape and NERL phase VI cross section; the result from comparison a slight improvement in the power factor [4].

September 2012 Schubel and Crossley aroused the conflict of increasing performance while maintaining a structure that supports the loads; such comments give reason why we need approaches to select, design and optimize blades from material point of view [5]. 2012 Cai, Zhu, Pan, and Gu presented structural optimization using finite element analysis and Particle Swarm method for HWAT blade [6].

Composite Materials

Thousands years before calendar Pharaohs built tombs and templates using composites bricks; which consists of straw and mud. Another famous monumental used mud bricks is the Djenne mosque built in 1907 in Maali at West Africa [7]. There are many historical examples of composite materials using natural components.

Many researches started to develop before the period of 1950 has to study the behaviour of building using reinforced concrete. The concept of composition sand, cement, minerals rocks, and steel bar inspired many scientists. Stephen W. Tsai one of the most famous contributor to composite material science concerned by what affects composites and how they behave under different condition [8]. Since 1960's and Tsai was very devoted to study the behaviour of composite material, in the end, he could derive equations to formulate the behaviour based on classic elasticity.

Tsai model based on classic plastic model named after the great scientist Henry Tresca, the founder of plasticity science. Henry Tresca defined new criterion to describe the flow stress in the plastic region. Then it came to Timoshenko who developed failure criteria and introduced it in his publications and handbook Elasticity. In addition, Richard Von Misses developed another new criterion called von misses yield criteria in the early 1940's. [9]

For decades and scientists are concerned with updating elastic models to cope with new design trends. Professor John Reddy was one of the pioneers in introducing new models using finite elements and variation methods. In 2010 Reddy, Arcinieg and Moleiro published an article introducing a finite element analysis technique for composite plates and shells used in the aerospace [10].

Optimization of composite lamina is a rich research field, which related to different application. In 2007, Almeida and Awruch introduced a genetic algorithm optimization technique for composite plates and shells design, in which the decision variables are orientation angle and ply thickness [11]. In 2010, Almeida and Awruch implemented harmony search algorithm for rectangular composite laminate, the decision variable were ply thickness and fibre orientation [12]. Akbulut and Sonmez formulated a simulated annealing algorithm to optimize design procedure of laminated composites; the objective was reduction of thickness [13].

Genetic algorithm

Optimization model is a set of iteration to find optimum value for decision variables without violating the constraint parameter, in addition to maximizing or minimizing the objective function. There are different methods for solving the optimization model; those methods depend on the nature of the model. Thus, model categorized from the aspect of decision into variables nature, objective function behaviour, degree of constraints.

Optimization models are categorized according to the behaviour of the model such as (one dimension, multidimensional, linear, nonlinear, integer, mixed integer, continues, statics, dynamics, deterministic, and stochastic). The model could be a multidimensional, deterministic, and linear with integer decision variables having static behaviour. The identification of model type will facilitate the proper solving method such as graphical solution, exact solution, Dichotomous search, golden section, quadratic interpolation, cubic interpolation, Fibonacci search, Davis and Campeny, Newton, or steepest-descent).

The paper presents another direction for solving optimization model known as evolutionary method; it considered beneath artificial intelligence algorithms category. Genetic algorithm is an iterative search method depends on the fitness of each solution set to find the optimum results from whole problem domain. In early 60's a professor from university of Michigan named *John Holland* studied the development of genes behaviour in living organisms and he started to mimics or imitate such behaviour by a mathematical algorithm. The first publication for Professor *John Holland* was 'adoption in Natural and artificial systems' 1975. [14]

Genetic algorithm represents the problem in the form of chromosome that includes the property for each entity. Properties then translated to real values and evaluated for the aspect of objective function. Evaluated results used as guide to reproduce procedure to breed new generation that is more fit.

Genetic optimization algorithm consists of individual, and population. The solo solution called individual; on the other hand, a set of solution called population. Search technique followed by genetic algorithm starts with generating initial population, then breeding new modified population until satisfying the stopping criteria.

Individual consists of two elements genotype and phenotype. Chromosome is the form of genotype that is a raw representation for the solution variables. The way of expressing the value of solution called phenotype. The Chromosome consists of genotype array each one represent specific phenotype. Model presented herein consists of hundred twenty-three genotype forming one chromosome. There are several methods to represent each phenotype in genotype then join into single chromosome; such as, binary, hexadecimal, and octal encoding.

Breeding is the heart of any genetic algorithm. Breeding is the method to create a new generation from the previous population, imitating the biological behaving during reproduction of genes in living species. Four operators are carried out to accomplish the

proper breeding process and to generate the new offspring. First operator is selection of parents, and then breeds those selected parents to generate offspring. Breeding starts with crossover, then mutation, tables (1 and 2) show the basic concept of crossover and mutation.

Formulating the blade optimization model

In order to choose the optimized criterion, an objective function defined in equation 1. The aim of the objective function is to reduce the weight while maintaining acceptable strength behaviour. Therefore, the objective function depends on the minimization the value of polynomial failure criteria and the ratio of current weight to extreme weight

$$Min Z = Weight$$
 (1)

The variables that affect the objective function's value called decision variables. Blade structure design consists of several design variables such as composite material: reinforcement material used in each layer, matrix material used in each layer, fibre volume fraction for each layer, and shape parameters: number of layers, thickness of each layer, width of core box, , and orientation of reinforcement in each layer. Consequently, the number of decision variables arrays is thirteen variable arrays. Table 3 summarizes the decision variables chosen for the presented model.

Constraints are determined according to the aspects of study. For example, there are limits, if the model selected maximum thickness for all layers and maximum number of layers, then those selections should not violate the geometric limitation, as shown in Table 4.

The chromosome presented in the form of bit string; Table 5 shows the number of bits representing each genotype. Total number of bits called chromosome length equal to 323 bytes. Consequently, solutions number equal to 2^{323} approximately 1.7×10^{97} solutions. The evaluation of a fitness function depends on the mechanical model presented in the subsequent section. Fitness function role is to sort individual in the population according to their objective value.

Reproduction process carried on three steps, as the following, selection, crossover, and mutation. Selection is a process to choose the fitted individuals from the population to generate offspring with higher fitness. There are two types of selection method. The first called proportional selection where selection for individuals carried regarding the fitness value relative to others values. The second method called ordinal-based selection, which selects upon ranks of individuals according to the fitness value. Consequently, selection depends on the value of fitness for each individual in the population according to the design of fitness function in the mathematical modelling and formation.

Crossover is a process of mixing selected individuals to generate new individuals with better fitness. The process carried through selection of a point where the crossing occurs after this point. Different methods used to select this point and redundancy of crossing point. Method selected to carry crossover depends on the nature of chromosome; whether it is haploid (each genotype has a single chromosome) or diploid (each genotype has a multi chromosome). The most common methods constraints depended system; in which the location of crossover point mix the same genotype with each other.

Stopping conditions depend on the desired outcome and computation device capabilities. Consequently, the condition could depend on number of iterations, a maximum number of generations after stalling, change in the tolerance of fitness function, or time of simulation.

Mechanical Model

The presented model evaluates the design parameters generated by genetic algorithm against constant inputs from aerodynamic analysis. Consequently, first part will clarify variables introduced to the model and constant input data. The second part describes geometric relations, reference system, and shape parameters, and Input data from aerodynamic analysis.

Three reference frames defined for the blade such as global, centre, and aerodynamic frames. Global reference frame located at the tip of airfoil notated by O. Centre reference frame located at the centre of shape (GC). Aerodynamic reference frame located at aerodynamic centre (AC). Air loads resolved at the aerodynamic centre in the form of tangent, normal forces and moment couple shown in Fig. 2.

The cross-section geometry characteristics defined using the NACA 4-digit designation (NACA xxxx-xx). The two digits after the hyphen state the chord length. First digit after the letters indicates the maximum camber height as percentage of the chord length. Second digit indicates the location of maximum camber height as tenth digit representation. The two digits before the hyphen represent the maximum thickness ratio of chord length. The following equations describe the shape of airfoil in two dimensions. [1]

$$y = \frac{t}{0.2} \left(a_0 \left(\frac{x}{c} \right)^{0.5} + a_1 \left(\frac{x}{c} \right)^1 + a_2 \left(\frac{x}{c} \right)^2 + a_3 \left(\frac{x}{c} \right)^3 + a_4 \left(\frac{x}{c} \right)^4 \right)$$
 (2)

Where $a_0 = 0.2969$, $a_1 = -0.126$, $a_2 = -0.3516$, $a_3 = 0.2843$, $a_4 = -0.1036$, t =the maximum thickness and c =the chord length.

The following two equations represent the camber effect.

$$b_1 = \frac{b_7(2b_6x - x^2)}{b_6^2}, if \ x < b_6, b_2 = \frac{b_7((1 - 2b_6) + 2b_6x - x^2)}{(1 - b_6)^2}, if \ x \ge b_6$$
(3)

Where b_6 is the camber location and b_7 is the camber percentage of chord length. Then equations describing the upper and lower profile of the airfoil are as the following:

$$(y_{u,l})_{head} = b_1 \pm y \text{ and } (y_{u,l})_{tail} = b_2 \pm y \text{ for all } x \text{ domain}$$
 (4)

Centrifugal force acts at the centre of gravity; hence, the following two equations estimate the coordinates of this centre in reference to airfoil global frame.

$$x_{gc} = c \left(\left(\frac{a_0}{2.5} + \frac{a_1}{3} + \frac{a_2}{4} + \frac{a_3}{5} + \frac{a_4}{6} \right) / \left(\frac{a_0}{1.5} + \frac{a_1}{2} + \frac{a_2}{3} + \frac{a_3}{4} + \frac{a_4}{5} \right) \right),$$

$$y_{gc} = \frac{2}{A} (y_1 + y_2 - y_3), z_{gc} = \frac{lenght}{2}$$
(5)

Where the y_1 , y_2 and y_3 are the expression for surface integration for airfoil gradient equation.

Lift and drag forces act at centre of pressure. Distribution of pressure changes that cause the pressure centre to be variable. On the other hand, force analysis needs a fixed point for aerodynamic forces. Consequently, lift and drag forces are resolved into force and moment acting at fixed point called aerodynamic centre. Subsonic blade has aerodynamic centre located at 29 % of chord length on symmetric axis. y coordinate is determined by similarity between centre of shape coordinate and x coordinate for aerodynamic centre; due to the inclination of symmetric line. [15]

$$x_{ac} = 0.29 * c, y_{ac} = \frac{(y_{gc} * x_{gc})}{x_{ac}}$$
 (6)

Blade weight depends on the total area of the cross section and density of material. Total area composite of shell and core cross section area. Shell area (A_s) estimated by calculating difference between the integration of outer and inner profiles. The core area derived with the same method.

$$A_{s} = \int_{0}^{b_{6}} (y_{u})_{h} dx + \int_{b_{6}}^{b_{0}} (y_{u})_{t} dx + \int_{b_{0}}^{c} (y_{u})_{t} dx - \int_{0}^{b_{6}} (y_{l})_{h} dx - \int_{b_{6}}^{c} (y_{l})_{t} dx$$
 (7)

$$A_s = A_1 + A_2 - A_3 - A_4 = \frac{2t}{0.2} \left(\frac{a_0}{1.5\sqrt{c}} c^{1.5} + \frac{a_1}{2c} c^2 + \frac{a_2}{3c^2} c^3 + \frac{a_3}{4c^3} c^4 + \frac{a_4}{5c^4} c^5 \right)$$
(8)

For an ideal case, the composite volume is the summation of matrix and fibre volumes. Hence, the percentage of fibre volume to composite volume considered a key parameter to the design of composite laminate. The rule of mixtures predicts density, strength, and elastic modules as discussed in [16].

The rule of mixtures used to predict the engineering constants too. Although there are limitations on predicting the transverse constants, it shows acceptable results for predicting axial modulus of elasticity and rigidity only. Consequently, the prediction of transverse properties is completely deviated from the experimental data. There are different approaches and methods formulate relation for transverse properties. Halphin Semi-empirical formula for predicting the transverse properties of composite lamina that found in [17]. Another method called Tsai Hahn that is used in the analysis and found in [18] [19]. Prediction of material strength values carried out using the same technique used for material properties.

$$\frac{1}{E_2} = \frac{1}{v_f + \eta_2 v_m} \left[\frac{v_f}{E_f} + \frac{\eta_2 v_m}{E_m} \right]$$
 where $\eta_2 = 1$ (9)

$$\frac{1}{G_{12}} = \frac{1}{v_f + \eta_2 v_m} \left[\frac{v_f}{G_f} + \frac{\eta_2 v_m}{G_m} \right] \text{ where } \eta_2 = 0.5$$
 (10)

Force analysis

Blade loading condition include aerodynamic loads (Moment couple, tangent and normal force) and inertia load (centrifugal and weight). The air load is model inputs. They are resolved on the aerodynamic centre. Inertia loads acts at the mass centre in 3D study or centre of shape in 2D section study.

Blade mass (M_T) calculated by summation mass of each lamina in shell and core. Centrifugal force (F_c) depends on blade mass, rotation speed, and radius of wind turbine arms.

$$F_c = M_T R \omega^2, M_T = \sum_{i=1}^{no \ of \ shell \ layers} V_{si} * \rho_{si} + \sum_{j=1}^{no \ of \ core \ layers} V_{cj} * \rho_{cj}$$

$$\tag{11}$$

Where R is the arm radius, ω is the angular speed, M_T is the segment total mass, $V_{s\,i/c\,j}$ is the single shell/core lamina volume, $\rho_{s\,i/c\,j}$ is the density of single shell/core lamina.

The components of resultant force acting at the centre of gravity shown in equation

$$F_x = F_{tangent}, \ F_y = F_c + F_{normal}, \ F_z = M_T * g \tag{12}$$

Where F_x is the x-axis component, F_y is the y-axis component, F_z is the z-axis component, $F_{tangent}$ is the aerodynamic tangent component, F_{normal} is the aerodynamic force normal component, and g is the gravity acceleration. The units of all the forces are Newton.

The moment force around the three axes is shown in equation

$$M_z = M_{blade} - F_{tangent} \| y_c - y_{ac} \| - F_{normal} \| x_c - x_{ac} \| + M_{bending} F_{x \& Fy} + M_{shear}$$
 (13)

First term (M_{blade}) indicates the torque applied on the blade due to air loads. The second and third terms are the moment applied due to equivalence of air load from aerodynamic centre to shape centre. Fourth term is the value of bending moment due to F_x in the plane x-z and F_y in the plane y-z. Last term is the moment due to shear force acting at the centre of shear.

Stress and failure analysis

Starting step is blade idealization into two sections. The first section is the core, which carries all direct and torsion loads. Second section is the shell, which carries all shear loads. After that, all loads analyzed into forces per unit length for each section. Stress analysis carried using Classical Laminate theory presented in [1], where each section stiffness matrices consists of extensional stiffness, bending, and coupling coefficients. The material failure analysis is checked using Tsai Hill Failure criteria presented in [2]. The fitness function always equal design weight until failure occur in any lamina, then the model stop and fitness value is altered with maximum weight according to upper boundary.

Case study solving

Aerodynamic loads are a result of extensive fluid structure simulation. Hence, the data imported to the model verified by computational fluid dynamics simulation done by (*Blue Power Consultation Company*). Load data contains reading for tangent, normal and moment at each rotation degree shown in Table 6. Model parameters are blade length, rotation speed, and arm radius shown in Table 7. The following tables show the input data.

Test data implementation carried out on MATLAB genetic optimization GUI tool. Population type was double vector. Size of population depends on chromosome length where it equal tenth time variables number. The reason behind population dependence of chromosome length is the presence of enough individuals for proper selection. Fitness scaling is Rank sorting. Selection method follows stochastic uniform distribution technique. Reproduction used multi point crossover with fraction of 0.8, while mutation was constraints dependent. The mutation flips random number according to genotype number location. Genetic algorithm used simple technique without any parallel or migration algorithms. Stopping conditions varied between maximum number of generation and fitness function tolerances.

Conclusion

The presented approach evaluated different layup composite material to aid designer in selecting proper material structure for vertical wind turbine. Data in Table 8 shows no constraints violation. Fitness values is less than maximum weight, which means no failure occurred in any lamina. Presented results give blade designer a role model to start with. Numbers of lamina needed for shell and core estimated clearly. In addition to, thickness of each lamina and core width indicated to brief the internal structure's geometry. Moreover, selection of material, orientation, and mixing conditions indicated. This design schema improves the blade design process because sometime designer scope directed toward expensive solution.

Results show that reduction of weight is promising while maintaining no failure. However, the model needs integration with cost analysis model to be capable of comparing different type of material such as carbon and Kevlar. Further works could include modification in optimization model to be multi objective model. Indeed this modification will need reconsider

mixed integer model into full binary model. Another issue is the integrations of vibration analysis. This integration requires more definition of laminate as finite element analysis. Eventually, the experimentation of different optimization results to verify the approach results.

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Figures

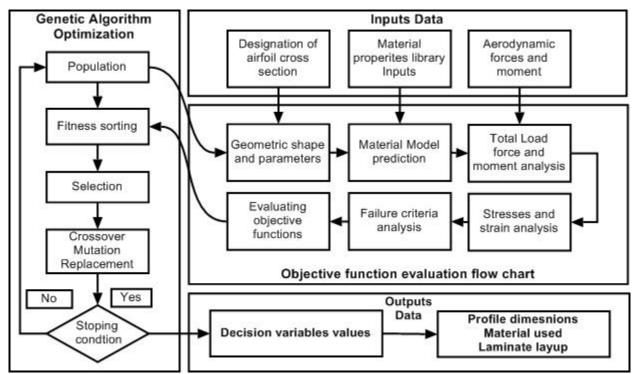


Fig. 1 Flow Diagram showing different steps for the Design and optimization approach

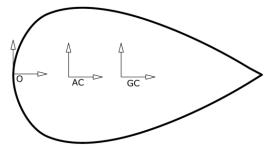


Fig. 2 shows the origin, aerodynamic center and centroid

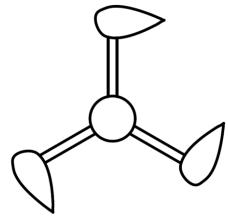


Fig. 3 Three blades vertical wind turbine (top view)

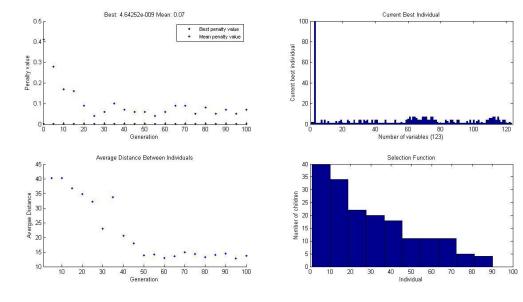


Fig. 4 Final Results of Genetic Algorithm showing all the random trends

Tables

Table 1 Crossover Explanation Example

Individual	Before	After	Different Crossover mode
C	11001011	1100 0101	Single point after 4 digits from the start the
		·	crossover between C and B
В	10110101	10 00 01 11	Double point after 2 digits sequence the
			crossover between C and B
D	00011100	Rejected	
A	01100010	Rejected	

Table 2 Mutation Explanation Example

Individual	Before	After	Different Mutation mode
C	110 <mark>0</mark> 1011	110 <mark>1</mark> 1011	Single point flip the 4 th digit from the
			start
В	10 <mark>1</mark> 10 <mark>1</mark> 01	10010001	Double points flip 3 rd digit and 6 th digit
C'	11000101	10010000	Multi points 2 nd , 4 th , 6 th , and 8 th
B '	1 <mark>0</mark> 000 <mark>1</mark> 11	1 1 000 0 11	With ratio 20%, and 75%

Table 3 Decision Variables notation

No	Description	Notation	Nature
1	Number of Shell Lamina	X(1)	Discreet
2	Number of core Lamina	X(2)	Discreet
3	Width of core box	X(3)	Continues
4	Thickness of each shell lamina	X(4) - X(19)	Continues
5	Thickness of each core lamina	X(20) - X(27)	Continues
6	Fiber Material Index for each shell lamina	X(28) - X(43)	Integer
7	Matrix Material Index for each shell lamina	X(44) - X(59)	Integer
8	Fiber Volume Fraction for each shell lamina	X(60) - X(75)	Continues
9	Fiber orientation Index for each shell lamina	X(76) - X(91)	Integer
10	Fiber Material Index for each core lamina	X(92) - X(99)	Integer
11	Matrix Material Index for each core lamina	X(100) - X(107)	Integer
12	Fiber Volume Fraction for each core lamina	X(108) - X(115)	Continues
13	Fiber orientation Index for each core lamina	X(116) –X(123)	Integer
·	Total Number of independent variables	123	Mixed
		X(1) - X(123)	Integer

Table 4 Constraints and decision variables

No	variable	Nature	Constraints	Units
1	X(1)	Discreet	$2 \le X(1) \le 18$	Index
2	X(2)	Discreet	$2 \le X(2) \le 10$	Index
3	X(3)	Continues	$20 \le X(3) \le 320$	Mm
4	X(4) - X(19)	Continues	$1 \le X(4) - X(19) \le 3.20$	Mm
5	X(20) - X(27)	Continues	$1 \le X(20) - X(27) \le 3.20$	Mm
6	X(28) - X(43)	Integer	$1 \le X(28) - X(43) \le 4$	Index
7	X(44) - X(59)	Integer	$1 \le X(44) - X(91) \le 4$	Index
8	X(60) - X(75)	Integer	$1 \le X(60) - X(75) \le 9$	Ratio
9	X(76) - X(91)	Integer	$1 \le X(76) - X(91) \le 4$	Index
10	X(92) - X(99)	Integer	$1 \le X(92) - X(99) \le 4$	Index
11	X(100) -	Integer	$1 \le X(100) - X(107) \le 4$	Index
	X(107)			
12	X(108) -	Continues	$1 \le X(108) - X(115) \le 9$	Ratio
	X(115)			
13	X(116) –	Integer	$1 \le X(116) - X(123) \le 4$	Index
	X(123)			

Table 5 Example on representation used in blade model

		- <u>r</u>													
genotype	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
Bit size	4	3	4	4	4	4	4	4	4	4	4	4	4	4	4
genotype	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Bit size	4	4	4	4	4	4	4	4	4	4	4	4	2	2	2
genotype	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45
Bit size	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
genotype	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60
Bit size	2	2	2	2	2	2	2	2	2	2	2	2	2	2	3
genotype	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75
Bit size	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
genotype	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90
Bit size	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
genotype	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105
Bit size	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
genotype	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120
Bit size	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
genotype	121	122	123												
Bit size	2	2	2												

Table 6 Sample of Force input data

Degree	Moment Couple	Normal Force	Tangent Force		
0	14.92344	122.8725	378.1605		
2.4	-14.8822	130.0449	384.2296		
4.8	-35.7909	144.6563	390.4343		
7.2	-45.6371	159.0719	394.1597		
9.6	-58.7571	173.7291	396.7187		
12	-65.1742	186.647	395.0094		
14.4	-62.2403	198.7465	391.186		
16.8	-60.2535	210.8567	386.9634		
19.2	-54.6376	220.2604	378.7905		
21.6	-46.511	228.5552	369.6851		

Table 7 Blade operating parameters

Parameters	Value
Rotation Speed	100 RPM
Blade length	18 m
Segment Length	6 m
Method of fixation	Built in both end
Arm Radius	6 m
Airfoil Designation	NACA 4971
Chord length	0.750 m

Table 8 Optimization Run 1 final value

No	Description	Value
1	Number of Shell Lamina	2
2	Number of core Lamina	2
3	Width of core box	100 mm
4	Thickness of each shell lamina	[1 4]
5	Thickness of each core lamina	[4 1]
6	Fiber Material Index for each shell lamina	[4 2]
7	Matrix Material Index for each shell lamina	[3 2]
8	Fiber Volume Fraction for each shell lamina	[6 7]
9	Fiber orientation Index for each shell lamina	[2 2]
10	Fiber Material Index for each core lamina	[3 3]
11	Matrix Material Index for each core lamina	[3 3]
12	Fiber Volume Fraction for each core lamina	[5 7]
13	Fiber orientation Index for each core lamina	[2 3]