14<sup>th</sup> International Conference on *AEROSPACE SCIENCES & AVIATION TECHNOLOGY*, *ASAT - 14 –* May 24 - 26, 2011, Email: <u>asat@mtc.edu.eg</u> Military Technical College, Kobry Elkobbah, Cairo, Egypt Tel: +(202) 24025292 –24036138, Fax: +(202) 22621908



# A Neural Predictive Control Scheme for Small Turbojet Engines

I.M. Atia<sup>\*</sup> and A.M. Bayoumy  $^{\dagger}$ 

**Abstract:** Artificial Neural Networks (NN) is a well-known tool among artificial intelligence techniques that are able to reproduce arbitrary nonlinear relationships existing between input and output variables. Model based Predictive Control (MPC), or simply predictive control, is a family of control schemes that uses a model from the plant as a predictor of the future plant outputs a nd he nce opt imizes the future c ontrol i nputs for the m inimum future e rrors a nd minimum control energy. Among this family Generalized Predictive control (GPC) is one of the most famous.

In another part of this work [5],, a neural network representation is shown to be suitable for modeling a small gas turbine engine (SR-30). In the present paper, this model is used in a model-based predictive c ontrol s cheme. The r esults of this c ontroller are c ompared with a classical P roportional-Integral-Derivative (PID) c ontroller tune d offline w ith a g enetic optimization technique. Both are tested on the SR-30 turbojet engine model.

PID controller cannot cope with model changes in the whole operating range of the engine and therefore a predictive control scheme is then proposed as a solution to this problem. A neural model is used as a predictor for the calculation of GPC parameters. The nonlinear system free response is obtained by recursive future predictions while the dynamic response matrix is obtained by instantaneous linearization of the input /output relation.

The results illustrate the improvements in control performance that could be achieved with a neural predicative scheme compared to that of a classical PID controller.

**Keywords:** Small tur bojet e ngines, artificial int elligence, neural n etworks, predictive controller, PID, GPC.

## Nomenclature

ARX	AutoRegressive with eXternal input
F	Vector of predicted free response
G	system impulse response matrix
$G_{\mathrm{f}}$	Fuel flow rate (kg/s)
K <sub>d</sub>	derivative gain
K <sub>i</sub> ,	
K <sub>p</sub> ,	proportional gain, integral gain
N	Engine revolution speed,(rpm)
$N_1$	lower value of predicting horizon
N <sub>2</sub>	Higher value of predicting horizon
NN	Neural networks

<sup>\*</sup> Egyptian Armed Forces, Egypt, <u>Hema1080@yahoo.com</u>

<sup>&</sup>lt;sup>†</sup> Egyptian Armed Forces, Egypt, <u>ambayoumy@gmail.com</u>

NNGPC	Neural network generalized predictive controller
Nu	Control horizon
PID	Proportional, integral and derivative controller
Т	Sampling time
t <sub>r</sub>	Rise time
ts	Settling time
$\hat{\mathbf{y}}$	Vector of predicted outputs for prediction horizon
ũ	Vector of future control increments for the control horizon
$\mathbf{W}$	Vector of future references
λ	Weighting factor for control increments

# Introduction

Model B ased P redictive C ontrol (MBPC), or s imply P redictive C ontrol, i s a f amily o f algorithms with common strategy. MBPC appeared in the decade of 1970s and had got a good reputation in the chemical industries and process control [1].

The main strategy of the MBPC is as follows, (**Error! Reference source not found.**): A model of t he c ontrolled s ystem i s us ed t o pr edict i ts be haviour i n t he f uture. A know n required reference trajectory is then given for certain prediction horizon. Then an optimisation algorithm i s us ed t o find the optimum control s equence for certain number of steps in the future that minimise a certain cost function which includes future predicted errors and control increments. A receding horizon technique is then applied where only the first control signal of the optimum future control sequence is applied to the controlled system.

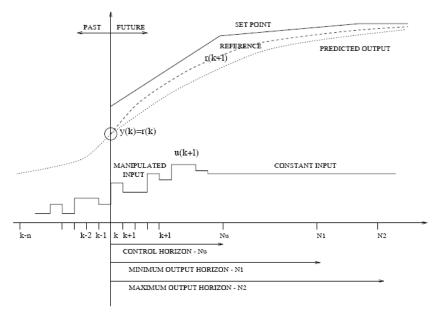


Fig. 1 Prediction strategy

Generalized Predictive Control (GPC) was developed by Clarke et al. in 1987 [2]. The GPC uses ideas from Generalized Minimum Variance (GMV) [3] and is perhaps one of the most popular methods at the moment.

Since the last three decades predictive control has shown to be successful in control industry. Generalized P redictive C ontrol (GPC) w as one of t he m ost f amous l inear pr edictive algorithms. T he control l aw of G PC c ontains t wo parameters t hat d escribe t he s ystem dynamics: s ystem free r esponse (f) and system i mpulse r esponse m atrix (G). Often these parameters a re c alculated from the di screte line ar mode l. For nonl inear s ystems, either a

nonlinear system model is instantaneously linearized or a nonlinear optimization is used. The validity of the linear model is the shortcoming of the first one and the possibility of non-uniqueness of local minimum is that for the second. The neural network (NN) model is used as a predictor to calculate these parameters for GPC.

The nonl inear s ystem free r esponse is obtained instantaneously while d ynamic r esponse is linearized every batch of time. This m ethod [4] is tested on a benchmark nonlinear model. Results a re c ompared with t hat of ot her neural pr edictive t echniques f ound i n pr evious literature. Also, this method in[4] is applied and validated on a realistic multivariable aircraft model. The simulation results show that this method has some good advantages over others neural pr edictive t echniques. In one h and, the s ystem d ynamics pa rameters ar e cal culated more accurately directly from the nonlinear NN model. And in the other hand, the used linear GPC has a c ost function with only one global minimum. The method in [4], as a trade-off between nonl inear ne ural pr edictive c ontrol (NPC) a nd i nstantaneous l inearization approximate ne ural l inear pr edictive control (APC), is pr omising for control of nonl inear systems.

A. W atanabe et al [7] w orked on PID and fuzzy logic algorithm in order to control SR-30 turbojet engine. They obtained transfer function of the SR-30 by using frequency response method. They tested and simulated both closed loop controller PID and fuzzy logic controller. They developed their model with MATLAB environment and tested it by NI LabVIEW.

R. Andoga et al [8] discussed digital electronic control of a small turbojet engine. They stated that the main purpose of control of gas turbine was increasing its safety and efficiency. Their engine w as c ontrolled b y PIC 16 F84A m icrocontroller, which manipulating the fuel flow valve.

M.Lichtsinder et al. [9] worked on de velopment of a simple real-time transient performance model f or AMT j et engine. T he fast m odel i s obt ained us ing t he Novel G eneralized Describing Function, proposed for investigation of nonlinear control systems. They presented the Novel G eneralized Describing Function de finition and then discusses the application of this technique for the development a fast turbine engine simulation suitable for c ontrol and real-time applications.

In another part of this work [5], a neural networks representation is shown to be suitable for modeling a small gas turbine engine (SR-30). In the present work, this model is used in a model-based predictive control scheme. This model is linearized at different engine design points, this linearized model is used in design of a classical PID controller. The PID controller is t uned of fline with a genetic opt imization technique. B oth c ontrollers a re t ested on t he SR-30 t urbojet e ngine model a nd c omparison i s m ade be tween t he r esults f rom t hese controllers with the same input.

# **Turbojet Engine Controller Design**

For a gas-turbine engine, particularly for a jet engine, the speed n control is one of the most important a spects (even most important than the engine t emperature control) and it is currently realized by some specific hydro-mechanical or electro-mechanical controllers.

The engine speed is the most important operating parameter, especially for the multi-spool engines, because it represents the parameter which assures the most accurate co-relation with the engine thrust amount, as well as with the engine fuel consumption; meanwhile, the speed

*n* offers an image about the dynamic load of the engine mobile parts (compressor blades and disks, turbine blades and disks, shafts), as well as an indirect image about the thermal charge of the engine hot parts (combustor, turbine(s), exhaust nozzle).

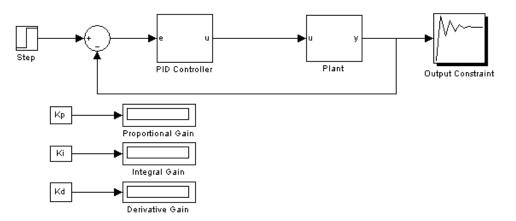
An aircraft engine operates at various flight regimes, that means at various flight speed and flight altitudes, which means that the engine thrust variation must follow the aircraft flight dynamics n ecessities, therefore the engine speed (and thrust) must be strictly controlled, because of its important operating role.

The engine speed is one of the engine operating parameters, which is the easiest to measure, both for steady state regimes and for dynamical regimes. That fact represents an advantage and promotes the engine speed as the most important controlled engine parameter.

In this paper one has studied an engine speed controller with fuel flow rate as a regulating parameter. The controller design was based on engine neural networks model.

## **Discrete PID Based on Engine NN Model**

The discrete PID controller was used with the NN model of the SR-30 turbo jet engine. Now, the tuning of the PID is achieved by using genetic algorithm. The GA is carried out using a MATLAB built-in r outine s o c alled S imulink R esponse O ptimization (SRO) T oolbox a s shown in Fig. 2. The SRO, automatically, formulates an optimization problem and calls a genetic algorithm and direct search toolbox, as an optimization routine to solve the problem.





A classical discrete PID control system can be described as shown. The input-output relation of the PID controller is expressed mathematically by equation (1)[13].

$$u(t) = K_{p} \cdot e(t) + TK_{i} \sum_{t=0}^{N} e(t) + K_{d} \frac{e(t) - e(t-1)}{T}$$
(1)

where, u(t) is the c ontrol s ignal, e(t) is the error s ignal, and  $K_p$ ,  $K_i$ , and  $K_d$  denotes the proportional gain, integral gain and derivative gain respectively, T is the sampling time and N is the number of samples,  $u_1(t)$  represents the output of the controller at the sampling point (t).

If the sampling period is short enough, the approximate calculation by equation (1) can get an accurate result and the discrete control process is close to the continuous control process.

The digital PID Controller transfer function as a function of z has the following form [13]

$$C(z) = K_p + K_i T\left(\frac{z}{z-1}\right) + \frac{K_d}{T}\left(\frac{z-1}{z}\right)$$
(2)

where:  $K_p$ ,  $K_i$  and  $K_d$  are the proportional, integral and derivative parameters of the controller respectively and 'T' the s ampling time. The r equired step response characteristics of t he engine are rise time ( $t_r$ ) = 0.872 s, settling time ( $t_s$ ) = 4 s and maximum overshoot ( $M_p$ ) = 2%.

PID controller is tuned, based on t he linearized ne ural model at different operating points, with s tep c hange f rom 41050 t o 82000 r pm. The opt imal P ID p arameters a re s hown i n Table (1) and t he r esulted s tep r esponse s hown i n **Error! Reference source not found.** represents the engine response at step input from n=41050rpm to n=82000 rpm. This input covers a wide range of engine speeds.

In contrast, if the same controller is used with an input of smaller amplitudes as shown in **Error! Reference source not found.** and **Error! Reference source not found.**, the response of the engine with the full range PID controller has a high over shoot response compared with the s cheduled P ID c ontroller. T his is due t ot he f act t hat the P ID controller is a 1 inear controller. It is thus not capable of de aling optimally with a nonlinear constrained system across its whole operating range.

Gain-scheduling P ID controllers are proposed and their parameters are recalculated and shown in Table (1) using small-amplitude step inputs, to cover the engine operating ranges in which the data used for the estimation and validation are available.

Model	Step changes (rpm)	k <sub>p</sub>	k <sub>i</sub>	k <sub>d</sub>	MSE
Linearized neural models at certain design points	41050-46050	22.3465	11.7934	2.6964	0.002554
	46050-51060	9.5792	8.7627	0.99334	0.00336
	51060-56050	6.1426	8.6645	1.2238	0.00371
	56050-61050	6.3598	9.2752	1.1889	0.003231
	61050-66060	8.3136	12.1784	0.99342	0.002649
	66060-71060	5.1877	8.9899	1.6088	0.003409
	71060-76100	7.479	13.4361	1.3721	0.00245
	76100-82000	4.6472	10.6291	0.70902	0.002762
Linearized model at n <sub>o</sub> =61050 rpm	41050-82000	7.4465	11.5974	1.2223	0.02024

Table (1) PID parameters at different step changes based on	
linearized neural network models and ARX model	

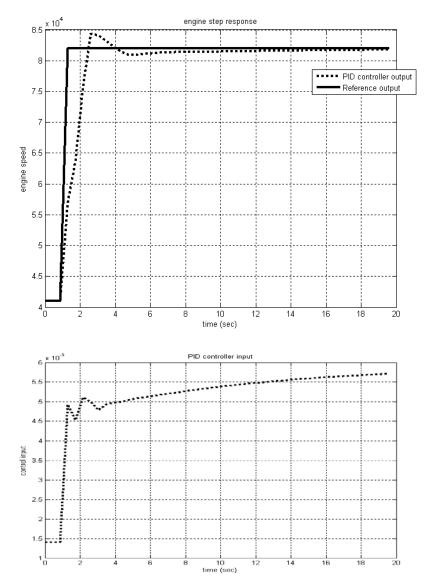


Fig. 3 Engine response with step change from n=41050 to n=82000 rpm. (a) Engine step response, (b) PID controller input

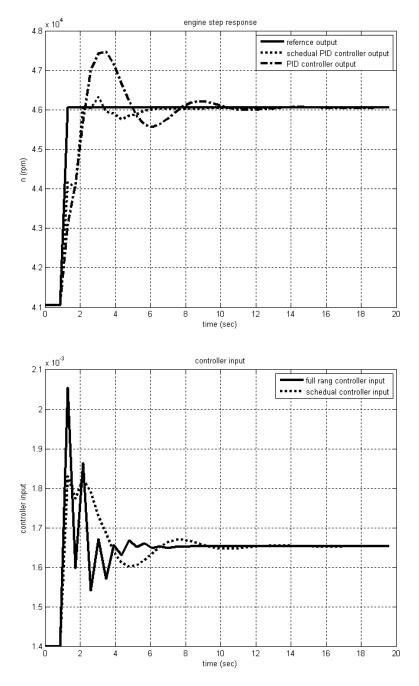


Fig. 4 Engine response with step change from n=41050 to n=46050 (a) Engine step response, (b) PID controller input

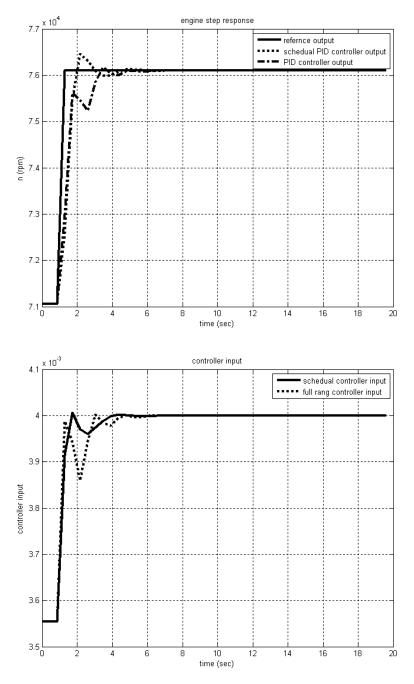


Fig. 5 Engine response with step change for n=71060 to n=76100 (a) Engine step response (b) PID controller input

**Error! Reference source not found.** represents the output from a neural model controlled with PID controller tuned at n=61050 rpm, the curve shows that the engine response became better as engine speed became near to the  $n_0$ = 61050 rpm and the error increased as the point became far away from the design point  $n_0$ .

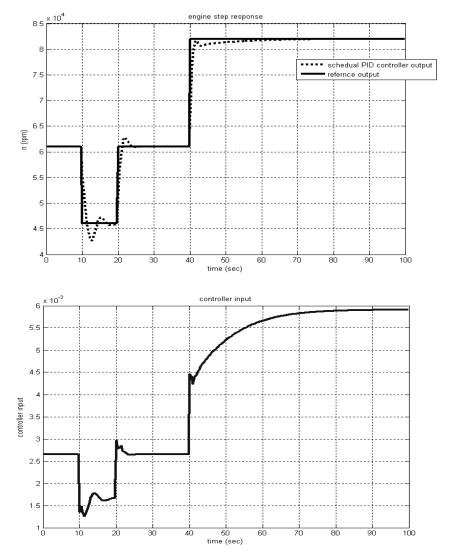


Fig. 6 Engine response with different steps change from n=61050 to n=82000 (a) Engine step response (b) PID controller input

The system nonlinearity is well illustrated if an increasing amplitude square pulse signal is given to the system. **Error! Reference source not found.** shows the response of the engine in case of square pulse signal input with the PID controller. There is an over shoot in the engine response.

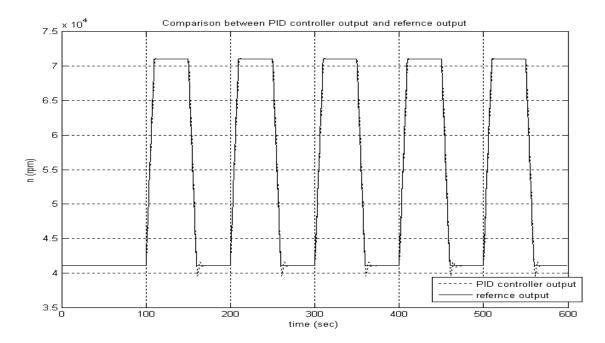


Fig. 7 The response of the engine in case of square pulse signal input with the PID controller

#### Predictive controller design

In order to implement the predictive controller strategy, the basic structure shown in **Error! Reference source not found.** is used. A model is used to predict the future plant outputs, based on pa st and current values and on the proposed optimal future control actions. These actions are calculated by the optimizer taking into account the cost function (where the future tracking error is considered) as well as the constraints.

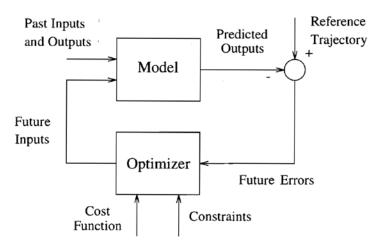


Fig. 8. Basic structure of MPC

The basic idea of GPC is to calculate a sequence of future control signals in such a way that it minimizes a multistage cost function defined over a prediction horizon. The index to be optimized is the expectation of a quadratic function measuring the distance be tween the predicted s ystem out put and s ome predicted r efference s equence over the horizon plus a quadratic function measuring the control effort. GPC provides an explicit s olution (in the absence of c onstraints), it c and eal with unstable and no m inimum phase pl ants a nd incorporates the c oncept of c ontrol horizon a s well a s the consideration of weighting of

control increments in the cost function. The general set of choices available for GPC leads to a greater variety of control objectives compared to other approaches, some of which can be considered as subsets or limiting cases of GPC.

The GPC algorithm consists of applying a control sequence that minimizes a multistage cost function J:

$$J = \sum_{j=N_1}^{N_2} \left[ \hat{y} \left( k+j \right) - w \left( k+j \right) \right]^2 + \lambda \sum_{j=1}^{N_u} \Delta u \left( k+j-1 \right)^2$$
(3)

Subject to:  $\Delta u (k + j - 1) = 0$  for  $N_u < j < N_2$ , where N<sub>1</sub> denotes the minimum prediction horizon, N<sub>2</sub> the maximum prediction horizon and N<sub>u</sub> the control horizon,  $\lambda$  is a weight factor penalizing changes in the control input to obtain smooth control input signals and d is the system time delay.

Then the predictor equation becomes in matrix form

$$\hat{\mathbf{y}} = \mathbf{G} \cdot \tilde{\mathbf{u}} + \mathbf{f} \tag{4}$$

where:

$$\begin{split} \hat{\mathbf{y}} &= \begin{bmatrix} \hat{y} \left( k + N_1 \right) \quad \hat{y} \left( k + N_1 + 1 \right) & \cdots & \hat{y} \left( k + N_2 \right) \end{bmatrix}^T \\ \mathbf{G} &= \begin{bmatrix} g_{N_1} & g_{N_1-1} & \cdots & g_1 & 0 & \cdots & 0 \\ g_{N_1+1} & \ddots & \ddots & \ddots & \ddots & \vdots \\ \vdots & \ddots & & g_1 & 0 \\ \vdots & & \ddots & & g_1 \\ g_{N_2} & g_{N_2-1} & & \ddots & g_1 \\ g_{N_2} - g_{N_2-N_u+1} \end{bmatrix} \\ \tilde{\mathbf{u}} &= \begin{bmatrix} \Delta u \left( k \right) \quad \Delta u \left( k + 1 \right) & \cdots & \Delta u \left( k + N_u - 1 \right) \end{bmatrix}^T \\ \mathbf{f} &= \begin{bmatrix} f \left( k + N_1 \right) & \cdots & f \left( k + N_2 \right) \end{bmatrix}^T \end{split}$$

Then J could be written in matrix form as:

$$J = \left(\hat{\mathbf{y}} - \mathbf{w}\right)^T \cdot \left(\hat{\mathbf{y}} - \mathbf{w}\right) + \lambda \tilde{\mathbf{u}}^T \cdot \tilde{\mathbf{u}}$$
(5)

where:

$$\mathbf{w} = \begin{bmatrix} w \left( k + N_1 \right) & \cdots & w \left( k + N_2 \right) \end{bmatrix}^2$$

Minimize J to get optimum  $\tilde{\mathbf{u}}$  we get:

$$\tilde{\mathbf{u}}^* = \left(\mathbf{G}^T \cdot \mathbf{G} + \lambda \mathbf{I}\right)^{-1} \cdot \mathbf{G}^T \cdot \left(\mathbf{w} - \mathbf{f}\right)$$
(6)

Taking the first element of the control sequence (as the receding horizon principle)

$$\Delta u^*(k) = \mathbf{H} \cdot (\mathbf{w} - \mathbf{f}) \tag{7}$$

where:

$$\mathbf{H} = \begin{bmatrix} 1 & 0 & 0 & \cdots & 0 \end{bmatrix}^T \left( \mathbf{G}^T \cdot \mathbf{G} + \lambda \mathbf{I} \right)^{-1} \cdot \mathbf{G}^T$$

For a linear time-invariant system the parameter  $\mathbf{H}$  is unchanged over the time. But the free response  $\mathbf{f}$  should be calculated every time step.

The incremental controller ensures zero offsets even with non-zero constant disturbance. The choices of p arameters ( $N_1, N_2, N_u$  and  $\lambda$ ) determine the stability and performance of the GPC controller. Some guidelines for selecting them exist in [6-10].

#### Free System Response (f)

To get the free system response the prescribed NN is given a zero increment vector  $\hat{\mathbf{u}}$  then the output predicted vector  $\hat{\mathbf{Y}}$  will be the system free response f.

#### Impulse system response (G)

The impulse response of the system is calculated using trained NN model with a linearization around the current operating point. To get the first column of the G matrix a small value for  $\Delta \hat{u}_{k+1}$  is as sumed as small value  $\varepsilon$ , where  $\varepsilon \ll 1$  and the corresponding output prediction is obtained.

$$\hat{\tilde{\mathbf{u}}} = \begin{bmatrix} \varepsilon & 0 & 0 & 0 \end{bmatrix}$$
(8)

Then the first column will be

$$\mathbf{G}_{(1)} = \frac{1}{\varepsilon} \cdot (\hat{\mathbf{Y}} - \mathbf{f}) \tag{9}$$

It will be easy after that to form the special shape of G matrix then calculate H vector.

#### **Predictive controller scheme**

The proposed control scheme **Error! Reference source not found.** consists of a nonlinear neural n etwork m odel in the form of NN m odel and a linear GPC controller. The n eural model is trained of f-line within the complete r ange of system input. After performing the training, the n etwork is then us ed by the GPC controller to calculate the free r esponse of nonlinear system e very time s tep. Every batch of time the impul se response ma trix is calculated through linearization.

The control law **Error! Reference source not found.** is computed every time-step to get the next control increment.

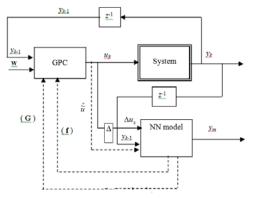


Fig. 9 Proposed Neural Network GPC Control Scheme

#### Application to the SR-30 NN model

The predictive controller parameters are  $N_1 = 1$ ,  $N_2 = 4$ ,  $N_u = 1$ ,  $\lambda = 0.05$ 

The system nonlinearity is well illustrated if an increasing amplitude square pulse signal is given to the system. The Simulations results and Comparison with the PID controller with the same input will be illustrated below.

**Error! Reference source not found.** shows the response of the engine in case of enhancing the full-step response from 41050 t o 82000 r pm. It is clear that the oscillation around final position eliminated and the rise and settling time are reduced

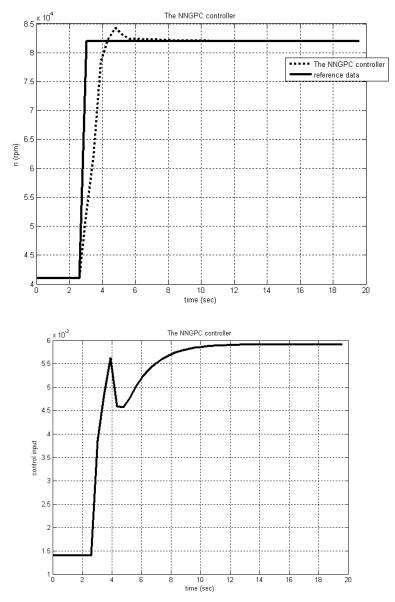


Fig. 10 Engine response with step change from 41050 to 82000 rpm (a) engine step response, (b) predictive controller input

**Error! Reference source not found.** shows the engine step response with random step input from 61050 to 46050 finally to 82000 rpm. It is clear that the engine response with predictive controller is improved where the oscillations are reduced and the settling time is reduced.

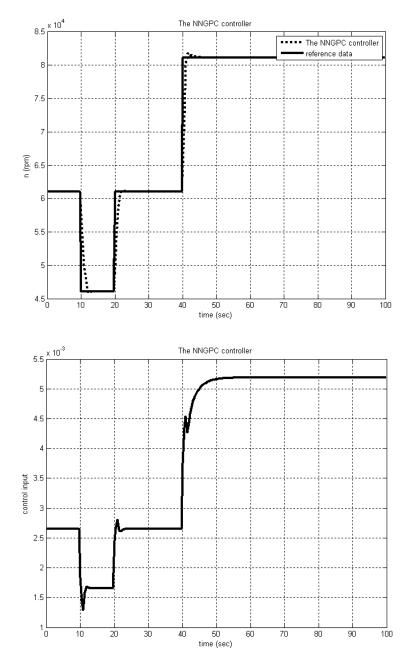


Fig. 11 Engine response with different steps change from n=61050 to n=82000 (a) engine step response, (b) predictive controller input

The system nonlinearly is well illustrated if an increasing amplitude square pulse signal is given to the system. **Error! Reference source not found.** the response of the engine in case of square pulse signal input with the predictive controller. It is clear that there is no over shoot in the engine response.

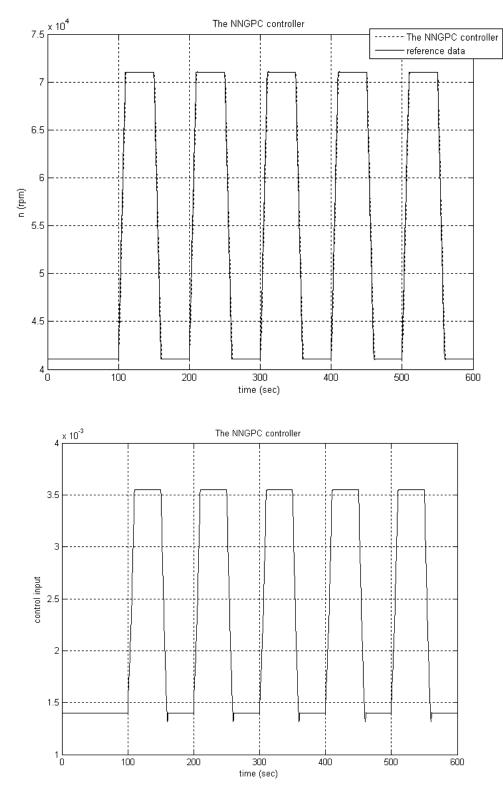


Fig. 12 Engine response in case of square pulse signal input (a) engine step response, (b) predictive controller input

## Results of comparison between PID controller and predictive controller

In t his s ection, a comparison i s m ade b etween t he P ID c ontrollers with t he pr edictive controller with respect to the same input signal as shown in **Error! Reference source not** found., 14 and 15.

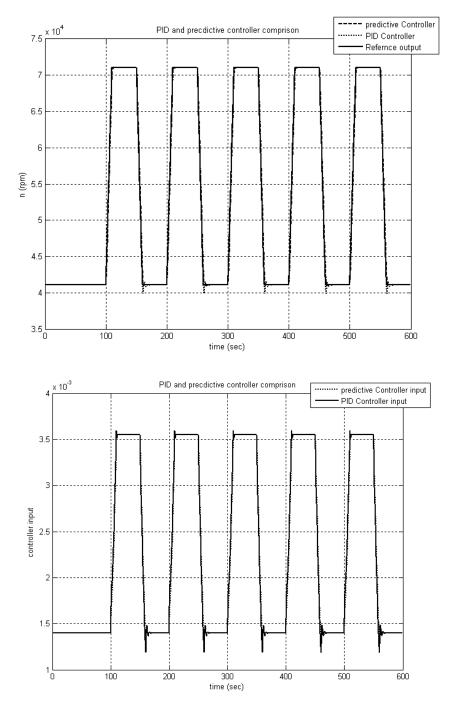


Fig. 13 Comparison between PID and predictive controllers in case of in case of square pulse signal input (a) engine step response, (b) controller input

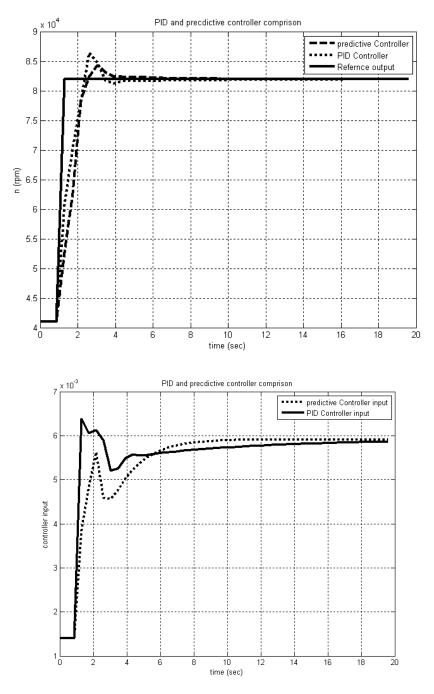


Fig. 14 Comparison between PID and predictive controllers in case of step input from 41050 to 82000 rpm (a) engine step response, (b) controller input

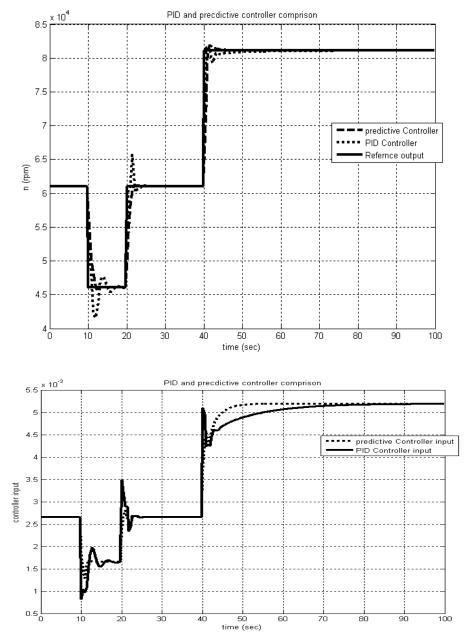


Fig. 15 Comparison between PID and predictive controllers in case of different steps input from 61050 to 82000 rpm (a) engine step response, (b) controller input

The Simulations results of the predictive controller and Comparison with the PID controller with the same input are illustrated above which show that the engine performance is improved with the predictive controller, the r esponse os cillation and ove rshoot is smaller with the predictive controller rather than the PID controller, the engine rise time is also smaller. It can be therefore concluded that the parameters in the gain-scheduling PID controller need to be changed with the operating range, but using predictive controller enables a global controller to be i mplemented and pr ovides the opt imal c ontrol performance across the ope rating r ange. Predictive c ontroller provides the best c ontrol performance against disturbances and m odel uncertainties.

# Conclusion

A representative neural network SR-30 engine model was used to develop a PID controller and pr edictive controller. R esults from the t wo controllers were compared and p redictive controller found to be accurate for engine control during the full operating rang.

The following results are derived from our analysis:

- 1. PID controller was built based on the neural networks model of the SR-30 engine.
- 2. Tuning of the P ID c ontroller w as performed with of fline with a genetic opt imization technique.
- 3. PID c ontroller c annot c ope w ith m odel c hanges i n t he w hole ope rating r ange of t he engine.
- 4. A ne ural m odel w as us ed as a pr edictor f or t he cal culation of G PC pa rameters. The nonlinear s ystem f ree r esponse w as obtained by r ecursive f uture pr edictions w hile t he dynamic response matrix was obtained by instantaneous linearization of the input /output relation.

As a conclusion, the results illustrate clearly the improvements in system performance that could be achieved with a neural predicative controller compared to that of a classical PID controller.

## References

- [1] Garcia C.E., P rett D.M., a nd M. Morari, "*Model predictive control: theory and practice- a survey*," Automatica, 25(3): 335-348, (1989).
- [2] D.W. Clarke, C Mohtadi, and P.S. Tuffs. "Generalized Predictive Control. Part I. The Basic Algorithm. Automatica" 23(2):137-148, 1987.
- [3] D.W. C larke and P.J. G awthrop. "Self-tuning Control. Proceedings" IEEE, 123: 633-640,1979.
- [4] A. M. Bayoumy, J. Bordeneuve-Guibé, "A Neural Predictive Control Scheme For Nonlinear Plants", D epartment of A vionics a nd S ystems, E NSICA, T oulouse, FRANCE, AIAA 2002-1541.
- [5] I. M. Atia and A. M. Bayoumy "*Testing and Model Identification of a Turbojet Engine Using Neural Networks*". ASAT-14, 2011
- [6] Clarke D.W., C. Mohtadi a nd P.S. Tuffs," *Generalized Predictive Control. Part2: Extensions and interpretations*," Automatica, vol.23, N°2, pp. 149-160, (1987)
- [7] Watanabe, A., Imen, S. M., Leland, R., Whitaker, K. W., and Trevino, L. C., 2004, *"Soft Computing Applications on SR-30 Turbojet Engine"* AIAA Paper No. 2004–6444.
- [8] Andoga, Rudolf, Ladislav Madarasz, and Ladislav Fozo. "Digital Electronic Control of a Small Turbojet Engine - MPM 2." 12. International Conference on Intelligent Engineering Systems. Miami, Florida. 37-40, 2008.
- [9] Michael Lichtsinder, Yeshayahou Levy "*Jet Engine Model for Control and Real-Time Simulations*" Journal of Engineering for G as T urbines and P ower, 200 6 b y ASME, OCTOBER 2006, Vol. 128 / 745.
- [10] Clarke D .W. a nd C . M ohtadi ," Properties of generalized predictive control" Proceedings of the 10th triennial world congress of IFAC, Munich, FRG, pp. 65 -76, (1987).
- [11] Clarke D.W. and R. Scattolini," *Constrained receding-horizon predictive control*" IEEE proceedings-D, vol.138, Nº4, pp.347-354, (1991)
- [12] Rawlings J. B. a nd Muske K. R., " *The stability of constrained receding horizon control*" IEEE Trans. Automatic control, 38(10):1512 1516, (1993)
- [13] Charles L Phillips, "Digital control system analysis and design".