



# Grain Refinement of AZ91 Magnesium Alloy: A Review

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Received 5 December 2022

Accepted 7 January 2023

Published 6 April 2023

## Abstract

Grain refinement is an established technique that reduces the grain size of material with the direct intention of improving its finished properties or characteristic. The main objective of grain refinement is to produce a fine, uniform, and equiaxed grain structure. On the other hand, grain refinement of cast magnesium can be achieved by two methods represented by increasing the cooling rate and adding a chemical grain refiner. AZ91 is a cast magnesium alloy used to produce die-cast components. In contrast, the basic microstructure of this alloy consists of a primary  $\alpha$ - phase in which the aluminum-rich  $\beta$ - phase ( $Mg_{17}Al_{12}$ ) is precipitated along grain boundaries in cast magnesium alloy. Cast AZ91 alloy generally exhibits low strength and ductility due to the network-like eutectic  $\beta$ -  $Mg_{17}Al_{12}$  distributed at the grain boundaries. In this review article, the research methods of grain refinement and its effect on the characterization of microstructure and mechanical properties of AZ91 magnesium cast alloy.

**Keywords:** Grain refinement; AZ91 magnesium alloys;  $\beta$ -phase ( $Mg_{17}Al_{12}$ ).

## 1. Mg and Mg-Alloys

Magnesium The Greek word Magnesia, an ancient Greek city now a prefecture in Thessaly, central Greece, gave rise to the name Mg. Sir Humphry Davy performed the first extraction in England in 1808; however, it wasn't until the early 19th century and the development of lightweight aircraft that magnesium began to garner attention [1]. According to the American Society for Testing and Materials ASTM, magnesium alloys are classified [2]. Magnesium alloy is called "green engineering materials"[3].

These alloys have a 1.624 c/a ratio with a hexagonal close-packed (hcp) lattice structure [4]. Due to their low density of 1.74 g/cm<sup>3</sup>, which is 35% lighter than aluminum's 2.7 g/cm<sup>3</sup> and almost five times lighter than steel's 7.9 g/cm<sup>3</sup>, as well as their good castability, thermal conductivity, high electromagnetic shielding characteristics, good die casting, weldability, good mechanical properties, and excellent recyclability they have always been appealing to designers [5-6-7-8-9].

Magnesium alloys have some limitations despite having many positive traits. Low melting point is the main drawback, and insufficient ductility at room temperature and associated poor cold working capabilities are additional drawbacks [10]. In general, die-cast magnesium alloys fall under one of four commercially prevalent categories:

- Mg- Al- Zn-Mn (AZ series),
- Mg- Al-Mn (AM series),
- Mg-Al- Si (AS series), and
- Mg- Al- RE (AE series) [11-12].

The most popular alloys are those in the AZ series [13]. Of all the magnesium-based alloys, the magnesium AZ91 alloy, which contains aluminum and zinc as major alloying elements, has one of the best combinations of castability, mechanical strength, and ductility [14]. This alloy's chemical composition is (Mg -9 Al- 0.7 Zn- 0.2Mn) [15]. There are several

variations of the magnesium alloy AZ91, including AZ91A, AZ91B, AZ91C, AZ91D, and AZ91E [16]. The primary phase is a solid solution of Mg and Al; the  $\gamma$ -phase ( $Mg_{17}Al_{12}$ ), which is a compound made of Mg and Al and precipitated along the grain boundaries and eutectic  $\alpha$ -Mg +  $\beta$ -phase ( $Mg_{17}Al_{12}$ ). Figure 1 represents the Mg-Al phase diagram, and Fig. 2 shows the corresponding microstructure [17-18].

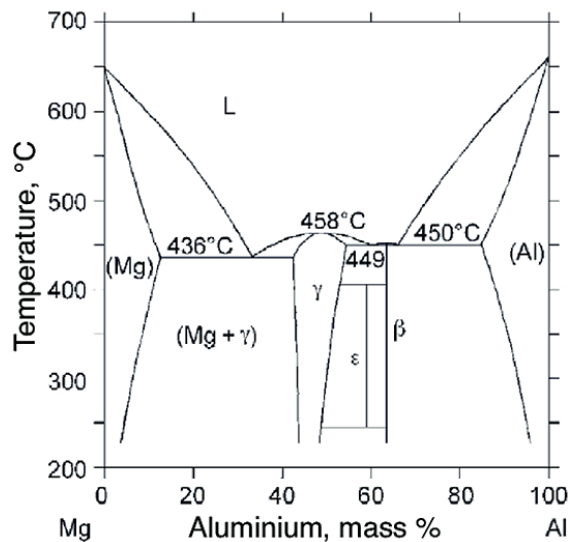


Fig.1 The Mg-Al phase Diagram [17].

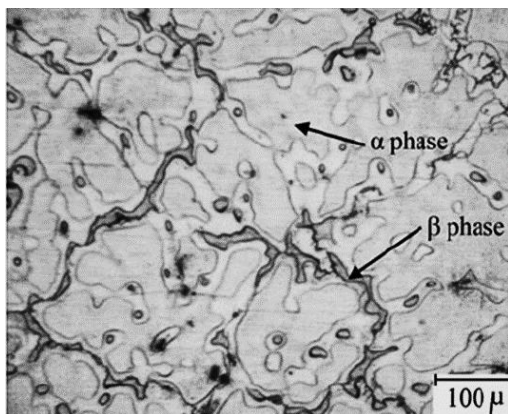


Fig. 2 Microstructure as cast of AZ91Mg alloy [19].

Due to its ideal blend of castability, mechanical strength, low production cost, ductility, and excellent corrosion resistance, AZ 91 is the most sought-after alloy. Its characteristics are listed in table 1 [20–21]. Sand and die castings use a general-purpose alloy [22]. Table 1: Properties of Commercially available die-cast AZ91 Mg alloy:

Property	Value
Density	1.81gm/cc
Melting Point	470-595C <sup>0</sup>
Yield Strength	150Mpa
Tensile Strength	230Mpa
% Elongation	3%
Elastic Modulus	44.8Gpa
Shear Strength	140Mpa
Hardness	75BHN
Thermal Conductivity	72W/mk
Coefficient of Thermal Expansion	25 $\mu$ m/m <sup>0</sup> k
Electric resistivity	14.1 $\mu$ $\Omega$ cm
Fatigue Strength	70Mpa

## 2- Grain Refinement of AZ 91Mg alloys

Since the late 1930s, Mg alloy grain refinement has been crucial to the broader adoption of alloys in various industrial applications [23]. The best way to increase the strength and plasticity of magnesium alloys is through grain refinement. The main objective of grain refinement is to produce a fine, uniform, and equiaxed grain structure, leading to a significantly improved, stable, and predictable set of mechanical properties. The cast surface and the surface that will be machined later have improved surface finish thanks to small interconnected holes with homogenous porosity distribution [24–25]. They also improve machinability, uniform mechanical properties, increasing castability, and more homogenous distribution of second phases. Two main techniques are widely used:

### 2.1 Rapid cooling

Rapid cooling of liquid metal during solidification: Rapid cooling prevents the diffusion of atoms from the liquid phase to the solid phase, which promotes the establishment of constitutional undercooling. For instance, superheating, Mechanical shearing, "ultrasonic wave and electromagnetic fields".

## 2.2 Chemical grain refinement method

This method involves adding elements or compounds to the melt to promote heterogeneous nucleation. For instance, C inoculation and the addition of other solutes such as Silicon Si, Strontium Sr, and Calcium Ca. And Elfinal process [3-26-27].

### 2.1.1 By superheating

According to a 1931 patent, one of the earliest techniques developed to regulate the grain size of Mg-Al-based alloys was superheating. Superheating is the usual term used to describe high-temperature treatment. And the procedure entails quickly cooling to the pouring temperature and a brief holding period at that temperature before casting the melt at a temperature significantly higher than the alloy's liquids, typically in the range of 453k to 573k.

Although many variables can affect how effectively superheating refines grains, there are some fundamental characteristics of this process. To begin with, only Mg-Al alloys with a minimum addition of Mn/Fe content can produce a noticeable grain refinement response. The grain refining effect must then be maximized at a specific temperature above the pouring temperature. The final requirements for producing fine grains include quick cooling from the overheating temperature to the pouring temperature and a short holding time [28–29]. In the previous studies, by Mehmet Unal [30], the hardness of alloys has been increased with cooling rates increase and silicon addition to this alloy. Also, with silicon addition in the 2 wt % to AZ91 that have occurred Mg<sub>2</sub>Si phases. Depending on the change in the cooling rate, the phase of Mg<sub>17</sub>Al<sub>12</sub> has been changed, and thinner grains have been obtained. The distance between the  $\alpha$ -Mg particles is narrowed.

In another work for fast cooling by Haonan Li [31], results reveal that grain coarsening occurs in cast AZ91 alloys when the cooling rate exceeds 90 k/s while it can be effectively inhibited upon adding NPs. The marked inhibition effect may originate from the formation of TiCN or  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> Np- can also promote further nucleation events and lead to significant grain refinement. An analytical model has been established to quantitatively account for the restriction effect of NPs on grain growth. It work may shed new light on the grain coarsening of cast alloys during fast cooling and provide an effective approach to circumvent it.

### 2.1.2 By vibrations

The vibration processes of mechanical, ultrasonic, and electromagnetic waves have all been documented [32]. Solid pieces of the solidified alloy make up the best grain refiner for an alloy. Growing dendrites are broken up by vibration, which promotes heterogeneous nucleation. Low-frequency vibrations cause the entire melt to oscillate in phase, with no mixing occurring in most liquid. However, surface waves are produced, and shearing occurs at the melt's free surface. Surface waves may be to blame for the observed grain refinement in these circumstances, with nuclei forming at or near the free surface and mixing by convection during filling. If the nuclei are not remelted in the flowing metal, this mechanism works as intended [33].

Many ways to produce vibrations in molten metals and alloys, including low-frequency vibration of the mold and direct generation of vibrations within the melt using electromagnetic fields and ultrasonic probes [34]. The influence of varying amplitudes at a constant frequency on the grain size and mechanical properties of AZ91Mg ally was investigated by Katja Pranke [35], As a result, there achieved a reduction in grain size as well as an increase in tensile strength, hardness, and elongation.

### 2.2.1 By carbon inoculation

Nearly 75 years have passed since the discovery of the grain refinement of Mg-Al-based alloys, but the grain refinement mechanism with carbon addition is still not fully understood [27–36]. The introduction of carbon into the molten magnesium at 700–800 C<sup>0</sup> is the crucial step in this process [1-31]. Hexachlorobenzene (C<sub>6</sub>Cl<sub>6</sub>), hexachloroethane (C<sub>2</sub>Cl<sub>6</sub>), silicon carbides SiC, aluminum carbides Al<sub>4</sub>C<sub>3</sub>, calcium carbides CaC<sub>2</sub>, and master alloys such as Al<sub>4</sub>C<sub>3</sub> - SiC / Al and Al- 1.5 C [26-31] are just a few examples of the many carbon-containing materials that can be added to molten magnesium. This process investigated by M. Suresh [37], the addition of charcoal particles effectively refines the grains in AZ91 Mg alloy. Maximum grain refinement is achieved with 0.4 wt% charcoal addition, which is found to be optimum. Both the Al<sub>4</sub>C<sub>3</sub> and Al<sub>2</sub>MgC<sub>2</sub> particles act as effective nucleates for magnesium grains. As a result of the fine-grained structure and the presence of hard particles, charcoal-treated alloys show better hardness and tensile properties. Also, investigated by HuiHan [38], Al<sub>4</sub>C<sub>3</sub> particles have been fabricated successfully by powder in situ synthesis process under argon atmosphere, In-situ Al<sub>4</sub>C<sub>3</sub> shows perfect grain refining effect for AZ

91D alloy. With the addition of 0.6%  $Al_4C_3$ , the sharp decrease of grain size and finer dendrite are readily obtained. And the grain refinement mechanism is attributed to  $Al_4C_3$  can act as the efficiently heterogeneous nuclei of primary  $\alpha$ -Mg and decrease the degree of undercooling the primary  $\alpha$ -Mg phase. And another study by TiJun Chen [39], indicates that  $MgCO_3$  can decrease its grain size from 311 to 53  $\mu m$ . Correspondingly, the tensile properties are improved.

### 2.2.2 Elfinal process or $FeCl_3$ process

At the end of World War I, in Germany, the process was first discovered [36]. Fe- Mn- Al compound nucleation. The process involves adding 0.4–1% of a hydrous ferric chloride  $FeCl_3$  powder to a molten magnesium alloy at temperatures between 740 and 780  $C^0$  [28]. The Prives Study by Xiaoying,[40]. The effect of  $MnCO_3$  addition on the grain refinement efficiency of AZ91Mg alloy has excellent grain refining efficiency for AZ91balloy, which is mainly attributed to the  $Al_4C_3$  Particles formed in the melt, Mn is indispensable to grain refinement in Al-bearing magnesium alloys. There is an optimal addition amount of 0.6% at 740  $C^0$  and the grain size is reduced from 245 to 91 $\mu m$ . At the same time, the corrosion resistance performance  $MnCO_3$ -added AZ91 alloy is improved.

### 2.5 Solute additions

An increase in undercooling at the solid/liquid interface can result from adding solute elements. With more particles acting as nucleants due to the higher undercooling, the grain size will be finer. Reported that Ca,Sr and Si [36]. This finding agreed with the work done by Hai Hao, [41]. Indicated that the addition of 1.5 wt% Sm with or without 0.8Si/Ca led to a decrease in the volume fraction of the  $\beta$ - $Mg_{17}Al_{12}$  Phase and the formation of the intermetallic compounds of Al-Sm,  $Mg_2Si$ ,  $MgAlCa$  and  $Al_2Ca$ . The microstructure of AZ91 alloy was significantly refined, and distribution became discrete with the addition of Sm and Ca; the average grain size of the  $\alpha$ -Mg matrix was reduced from  $239.7 \pm 16.9 \mu m$  to  $66.43 \pm 5.10 \mu m$ . The AZ91- Sm-Ca alloy exhibited a good combination of yield strength at 135 Mpa, ultimate tensile strength at 199 Mpa, and elongation at 4.32%, ascribed to grain refinement strengthening. Furthermore, the T6-treated AZ91-Sm-Ca alloy possessed yield strength of 154Mpa and elongation of 7.1%, which was due to grain refinement strengthening and reduction in discontinuous precipitates.

### 3. Advantages and Disadvantages of Grain refinement methods

Regarding the capable, technical, economic, environmental, and safety aspects, a new and superior grain refinement process is required [26]. Superheating and C inoculation, for instance, can significantly refine grains while the Elfinal process only slightly refines them. In contrast, solute addition can significantly reduce grain size even without the addition of a nucleant. While it was that some grain refinement has been achieved, added Sic works fairly well. However, when Fe and Mn are both present, poisoning happens. Despite the fact that these methods have some issues from the perspectives of technical, economic, and environmental issues, Superheating is challenging to control, and C inoculation is the only commercially available method at this time.

### 4. Future Considerations

Considerations for specific grain refinement techniques can be summed up as follows:

- C inoculation and Sic; A successful commercial strategy has not yet been developed, and grain refinement's effectiveness is only marginally better than average.
- The Elfinal procedure: While there is circumstantial evidence that this occurred, it is challenging to find concrete proof. Additionally, it is challenging to use this method to account for all observations due to the wide variety of effects. However, it is worthwhile to make further efforts to find a powerful grain refiner for these alloys given the commercial significance of Mg-Al-based alloys.
- Solvent additions; a lack of physical data that would allow the developed predictive equations to reliably predict grain size [26].

### 5. Conclusion

Some techniques used for years have a mechanism for refining grains. However, consequently, more research is required to comprehend the mechanisms of current methods and to uncover some fresh approaches to improving the microstructure of magnesium alloys. Grain refinement, which entails the formation of small, equiaxed grains in the presence of dendrites and is connected to forming intermetallic phases as a coating on the nuclei, can enhance an alloy's mechanical properties. There are several ways to refine the grains of the AZ91 magnesium alloy, including superheating,

C inoculation, vibration, the Elfinal process, and the addition of solutes. Their mechanisms involve both physical and chemical processes. In general, from the earlier research about various methods. Generally speaking, results from earlier studies on various methods of grain refinement for AZ91Mg alloy lead to an improvement in the material's mechanical properties and grain size of the microstructure

## References

- [1] S. Tzamtzis, Solidification behavior and mechanical properties of cast Mg-alloys and Al-based particulate metal matrix composites under intensive shearing, Thesis, Brunel university, (2011).
- [2] C. Moosbrugger, editor, "Engineering properties of Magnesium Alloys" ASM, (2017).
- [3] Wang Chang, Yanping Shen, editor, Grain Refinement of AZ91Magnesium alloy Induced by Al- V-B Master Alloy", Metals, 9 (2019) 1333.
- [4] A. SIAHSARANI, Ghader FARAJI. processing and characterization of AZ91magnesium alloys via a novel severe plastic deformation method: Hydrostatic extrusion compression (HCEC), Trans. Non-ferrous Met.Soc.China, 31, (2021) 11155.
- [5] Z. Yu, Jia, Fu-Sheng pan and Zhengyuan Gao, Effect of the high content of manganese on microstructure, texture and mechanical properties of magnesium alloy, 136 (2018) 310.
- [6] A.H. Feng and Z.Y. Ma, Enhanced mechanical properties of Mg-Al-Zn cast alloy via friction stir processing, Scripta Materialia, 56 (2007) 397.
- [7] M. Szymanek, B. Augustyn, D. Kapinos, S. Boczkal, J. Nowak, production Ultrafine Grain Structure in AZ91 Magnesium alloy cast by Rapid Solidification", Archive of Metallurgy and Materials, 59 (2014) 317.
- [8] M. Asmussen, David Shoemsmith, The influence of Microstructure on the Corrosion of Magnesium Alloy, Corrosion, 71 (2015) 242.
- [9] H.A. Goren, M. Unal and E. Koc, A comparative study on Microstructure properties of AZ91 Magnesium Alloy with Silicon Addition Using Ceramic Mold, Acta Physica Polonica, 135 (2019) 884.
- [10] T. Vavra, Superplastic deformation of ultrafine-grained magnesium alloys containing rare earth metals and zinc, A thesis, Charles University, (2019).
- [11] A. Z. Hanzaki, S.M. Fatemi, Microstructure and mechanical properties of an AZ91 Magnesium Alloy processed through Backward Extrusion, Arch. Metall. Mater. 63 (2018)149.
- [12] R. Zeng, Precipitation hardening in AZ91 magnesium alloy, Met.Mat. Trans.A, 43 (2013) 3891.
- [13] R. Sampathkumar, Magnesium and its Alloys for Automotive- A Review, Int J Adv Manuf Technol 39 (2008) 851.
- [14] V. Sklenička, M. Pahutová, K. Kuchařová, M. Svoboda, T. G. Langdon, Creep processes in magnesium alloys and their composites, Metallurgical and Materials Transactions A, 33 (2002) 883.
- [15] H. Shastri, Correlation of Microstructure with tensile, creep and corrosion behavior of AZ91Mg alloy fabricated by three different casting techniques, A Thesis, National Inst. Tech. Odisha, (2015).
- [16] P. Agarwal, Microstructure and properties of AZ91 magnesium alloy, China Foundry, 16 (2015) 319.
- [17] H. Dini, AS- cast AZ91 D Magnesium Alloy properties: Effect of Microstructure and Temperature, A Thesis, Jönköping University, (2017).
- [18] S. Chowdary, R. Dumpala, A. Kumar, K. Ratna Sunil, Influence of heat treatment on the machinability and corrosion behavior of AZ91 Mg alloy, J. Magnesium Alloys, 6 (2018) 52.
- [19] P. Asadi, N. Parvin, A.A. Araei, M.T. Hargh, ON the role of cooling and tool rotational direction on microstructure and mechanical properties of friction stir processed AZ91, Int J Adv Manuf Technol, 63 (2012) 990.
- [20] A.B. Asha, N. Akram, S. Roy, K.M. Shorowordi. Aging Behavior of AZ91 and Boron added AZ91Magnesium cast alloy, 1st ICEMME (2016) Dhaka, Bangladesh,2.
- [21] CW Chung, RG Ding, YL Chiu, M.A. Hodgson, W Go, Microstructure and mechanical properties of an as- cast AZ91 magnesium alloy processed by equal channel angular pressing, IOP Conf. Ser.: Mater. Sci. Eng., 4 (2009) 012012.
- [22] D. Minal Sanjay, To study corrosion and mechanical Behavior of Friction Stir Processed AZ91 Mg alloy, Materials Today Proceedings, 44 (2020) 1980.
- [23] D.H. St JOHN, M. QIAN, M.A. Easton, Peng CAO, and ZOE HILDEBRAND, Grain Refinement of Magnesium Alloys, Met.Mat.Trans. 36A (2005)1670.
- [24] C. ZhiYuan, The preparation of nano AZ91magnesium alloy powders with Hydrogenation Disproportionation Desorption Recombination, J. Alloys Compounds, 819 (2020) 153253.
- [25] E. Yaliniz, Development of high-temperature creep resistant aluminum-based sand cast magnesium alloys, Thesis, Graduate School of Natural and Applied Sciences (2018).

- [26] Amit Azad, Grain refinement of magnesium alloy AZ91E. *Metas*, 9 (2012)1333.
- [27] D.H.St. John, P.b. Cao, M.b. Qian, M.A. Easton, A Brief History of the development of grain refinement technology for cast magnesium alloys. *Magnesium Technology*, (2013) 3.
- [28] P.Cao, M. Qian, H. Davi, Mechanism for grain refinement of magnesium alloys by superheating, *Scripta Materialia*, 56 (2007) 634.
- [29] Bo Jiang, Solidification Behaviour of Magnesium Alloy., Springer, Tesis, Brunel University, (2013).
- [30] H.A. Mehmrtunal, E. Goren, K. Yunus T. Hayrettin, Effect of Cooling Rate and 2wt% Silicon Addition on Microstructure and Mechanical Properties of AZ91Mg alloys. *Journal of Materials Science*, 5 (2017), 5.
- [31] H. Li, K. Wang, G. Xu, H. Jiang, Q. Wang, Y. Wang, Effective inhibition of anomalous grain coarsening in cast AZ91 alloys during fast cooling via nanoparticle addition, *Journal of Magnesium and Alloys*, (2021) 2.
- [32] V. Chaturvedi, A. Sharma, U. Pandel, Effect of Mechanical Vibrations on Grain Refinement of AZ91Mg alloy, *J.Mater.Eng.Perform.*, 30 (2012) 3187.
- [33] A. Maitais, M. Fiset, and D. Dube, Grain refinement of magnesium alloy AZ91D cast in permanent Mold using Mechanical Vibration, *Materials science forum*, 426-4321 (2003) 527.
- [34] V. Chaturvedi, U. Pandel and A Sharma, Effect of mechanical vibrations on the wear behavior of AZ91 Mg alloy, *IOP Conf. Ser.: Mater. Sci. Eng.*, 314 (2018) 012030.
- [35] K. Pranke, K. Eigenfeld, About ultrasonic melt treatment during solidification and its influence on grain size and mechanical properties of magnesium alloy AZ91. *Materials Science Forum*, 649 (2010) 295.
- [36] E. Karakulak, A review: Past, Present, and Future of grain refining of magnesium castings, *J. Magnesium Alloys*, 7 (2019) 355.
- [37] M. Suresh, A. Srinivasan, U.T.S. Pillai, B.C. Pai, Mechanism of grain Refinement and Mechanical properties of AZ91Mg alloy by Carbon Inoculation, *Procedia Engineering*, 55 (2013) 93.
- [38] H. Han, H. Miao, S. Liu, and Y. Chen, Grain Refinement of AZ91D Magnesium Alloy by In-situ  $Al_4C_3$  Particles. *Materials Science Forum*, 306-307 (2011) 429.
- [39] T.J. Chen, X.D. Jiang, Y.M. Rui, Q. Wang, Y. Hao, Grain refinement of AZ91D Magnesium Alloy by  $MgCO_3$ , *Mat. Res.*, 14 (2011)1.
- [40] X. Liu, H. Geng, M. Zuo and P. Ji. Influence of  $MnCO_3$  addition on the grain refinement of AZ91Mg alloy. **Applied Mechanics and Materials**, 703, (2014) 56.
- [41] H. Hao, Microstructure and mechanical properties of AZ91 magnesium alloy with minor additions of Sm, Si and Ca elements, *China Foundry*, 16 (2019) 319.