

MILITARY TECHNICAL COLLEGE CAIRO ~ EGYPT

APPLICATION OF THE METHODS OF SELECTION OF

GEAR BOX RATIOS TO PASSENGER CARS

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ABSTRACT

Selection of ratios in mechanical transmission of motor vehicles can be done according to various mathematical progressions such as : arithmatic, harmonic and geometric with constant and increasing roots.

In a paper presented by the same authors, a comparison of the methods of selecting the gear ratios has been made. This was done by calculating the wasted power due to their stepped tractive effort - speed characteristics relative to the ideal one with continuous power transmission. It has been concluded that the gemetric progression would give the least wasted power. This conclusion was based on calculations considering the data of only one Jeep car.

The objective of this paper is to prove the validity of the above mentioned conclusion. In this regard, same method of comparison was applied to 14 small and medium class different passenger cars having engines of swept volume between 0,9 and 1.6 litre.

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INTRODUCTION

Matching of the vehicle engine and transmission is an important job that a vehicle designer has to fulfil. A good matching depends upon both engine and transmission characteristics.

In a mechanical transmission, the choice of the gear ratios represents the most important factor influencing the degree of matching and consequently the vehicle performance.

Selection of the gear ratios is usually done according to certain mathematical progressions such as; arithmatic, harmonic and geometric with constant or increasing roots.

In a paper published by the authors in May 1985 (1) a comparison of the methods of gear ratios spacing has been done. As a measure of comparison, the unobtainable power due to traction-speed characteristics of mechanical transmission relative to the ideal one has been considered. On the traction-speed curve in Fig. 1, the areas representing the unobtainable or wasted power is shown.

The comparison has been made considering the data of a Jeep car and it has been concluded that the geometric progression would give the least wasted power.

To prove the validity of this conclusion, the present study considers a variety of small and medium class passenger cars.

TECHNICAL DATA OF THE PASSENGER CARS CONSIDERED IN THE ANALYSIS.

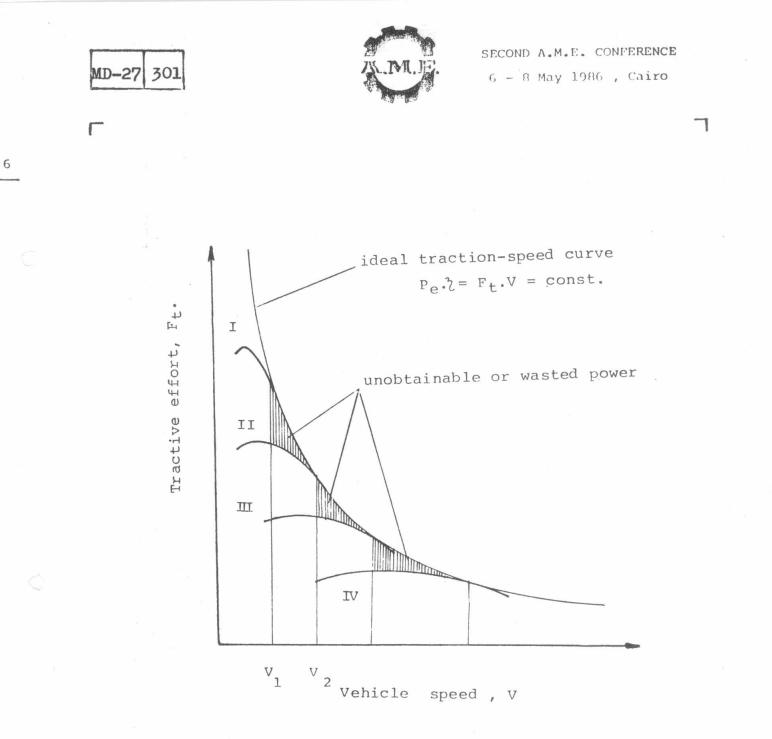
The passenger cars considered in the study belong to the small and medium class cars have swept volume of engine ranging between 0.9 and 1.6 litres. The main technical data of these cars are given in Tables 1a, 1b, and the caharacteristic power and torque curves are shown in Figs. 2,3,4,5.

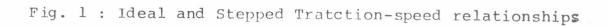
The engine power curve can be predicted by an equation of the following form :

$$P_{e} = P_{e} \max \left[A \left(\frac{n_{e}}{n_{N}} \right) + B \left(\frac{n_{e}}{n_{N}} \right)^{2} + C \left(\frac{n_{e}}{n_{N}} \right)^{3} + D \left(\frac{n_{e}}{n_{N}} \right)^{4} \right]$$
(1)

Where :

Pe = engine power, HP Pe max = engine maximum power, HP ne = engine revolutions, r.p.m. n = engine revolutions at max. power, r.p.m. A,B,C,D = constants.



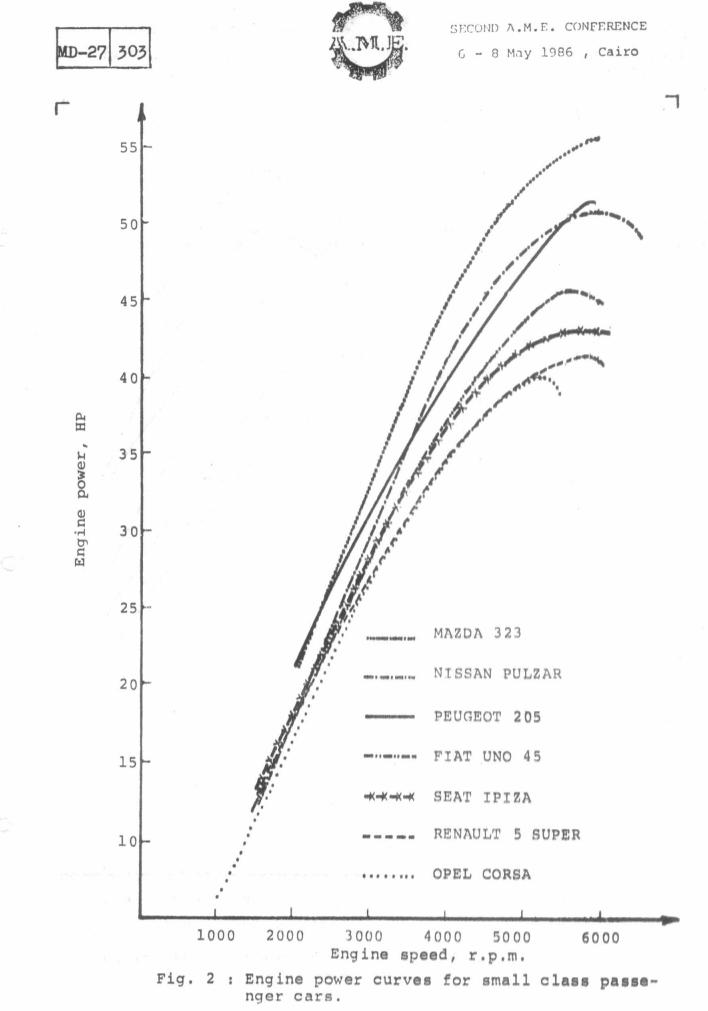


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							,	final		0	hov ratio	50	
Time Of	Power	r (HP)	Torque	ue	max.	Swept volume	d yn. radius	drive		dear	-		
Vehicle	N e max	4	Me max	at at	r.p.m.		rd(m)	ratio i	il	i2	ч С	i4 .	ц Г
		IL D III		1									2
a) Small Class													
MAZDA 323	55	6000	ß	4000	6000	1.071	0.275	4.39	3.42	1.84	1.29	0.92	1
NTSSAN PULZAR	50	6000	7.58	4000	6 500	0.988	0.279	4.47	3.33	1.96	1.29	0.9	-
TOFOT	50.34	5800	7.58	3000	6000	1.188	0.274	4.79	3.88	2.07	1.38	0.94	1
		200	a v	30.05	6000	0.903	0.265	4.07	3.91	2.06	1,34	0.96	
			•		C	0.903	0.274	4.79		1.95	1.32	0.97	1
SEAT IPIZA	4 6 . 3	7000	•	2							1	1	
RENAULT 5	40.8	5750	6.3	000	6000	0.956	0.274	3.875	3.73	2.05	1.32	0.0	I
OPEL CORSA	4 0	5200	6.32	3000	5400	0.993	0.274	4.18	3.55	1.96	1.3	0.89	1
b) Medium Class			Ŷ				1		, co	ч г г	811	0.85	0.71
HONDA CIVIC	81.83	6000		20	20	4 4 8	10	VV	. 4	. 0	. 2	6.	1
V.W. JETTA	74.8	5000	12.74	2506	6000	. ت ط	. 42	0.0	.		1	0.89	1
OPEL ASCONA	70.72	5400	12.03	3000	6000	1.598	0.291		י יד י		1 1	σ	1
NISSAN SUNNY	7.0	5200	11.7	3200	5500	l.488	0.279		٤.٤.٢	. 0	4	•	0 83
FIAT REGATA	74	5500	11.35	3500	6 0 0 0	1.498	0.279	3.59	•	~	3ª 1	0 0	F
SEAT MALAGE	82.5	5800	11.5	3500	6000	1.461	0.279	3.74	S.	5	n. 1	10.0	σ
RENAULT 9	58.48	5250 .	10.194	3000	5500	1.397	0.279	4.08	3.73	2.05	1.32		

Table 1 a,b: Technical data of small and medium class vehicles

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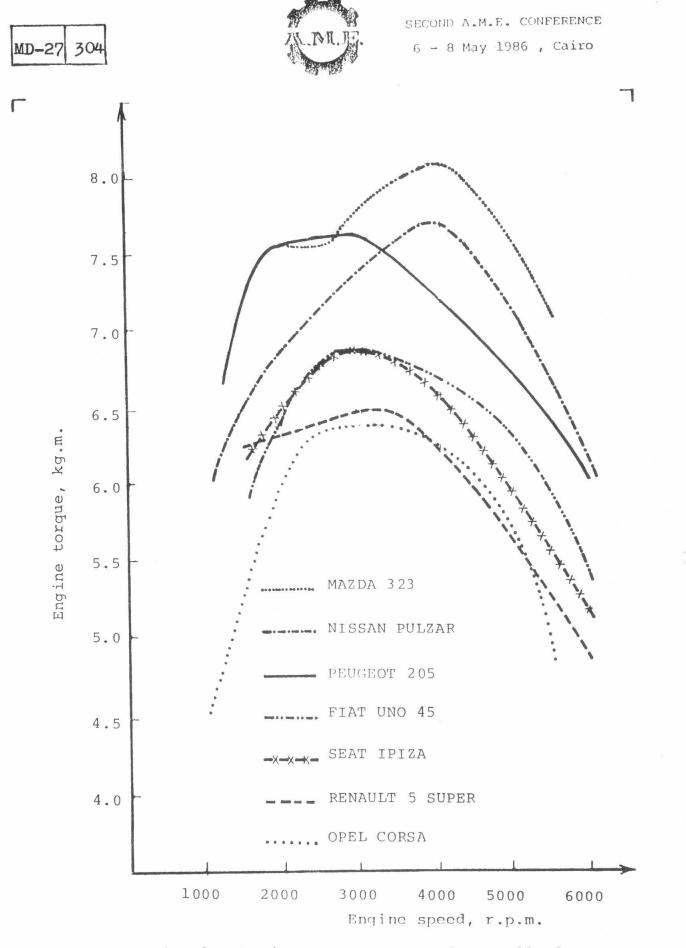
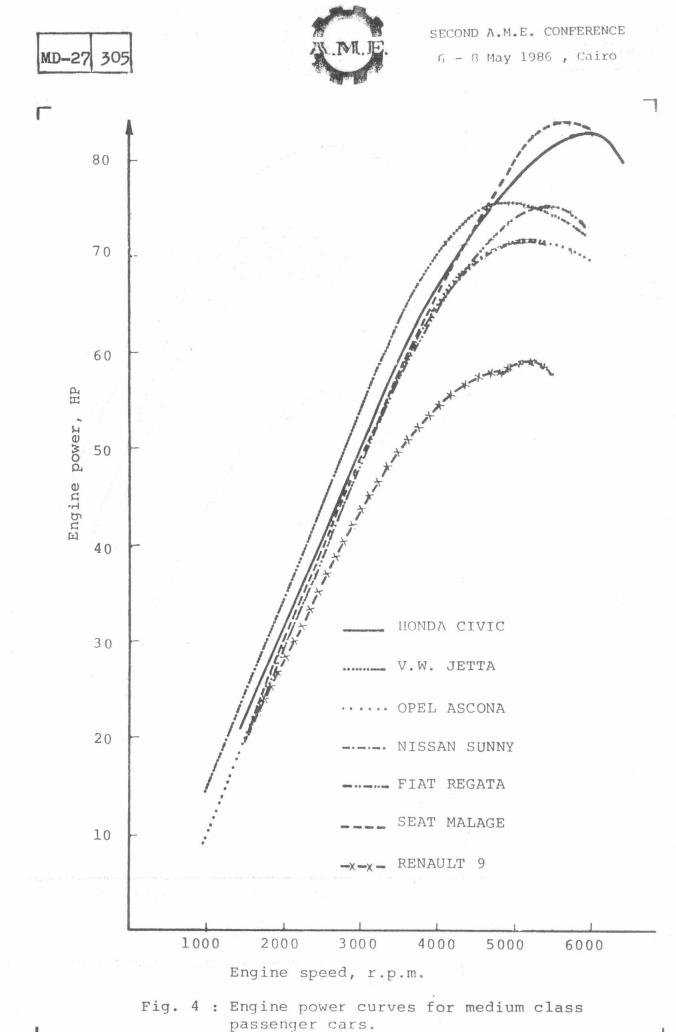


Fig. 3 : Engine torque curves for small class passenger cars.

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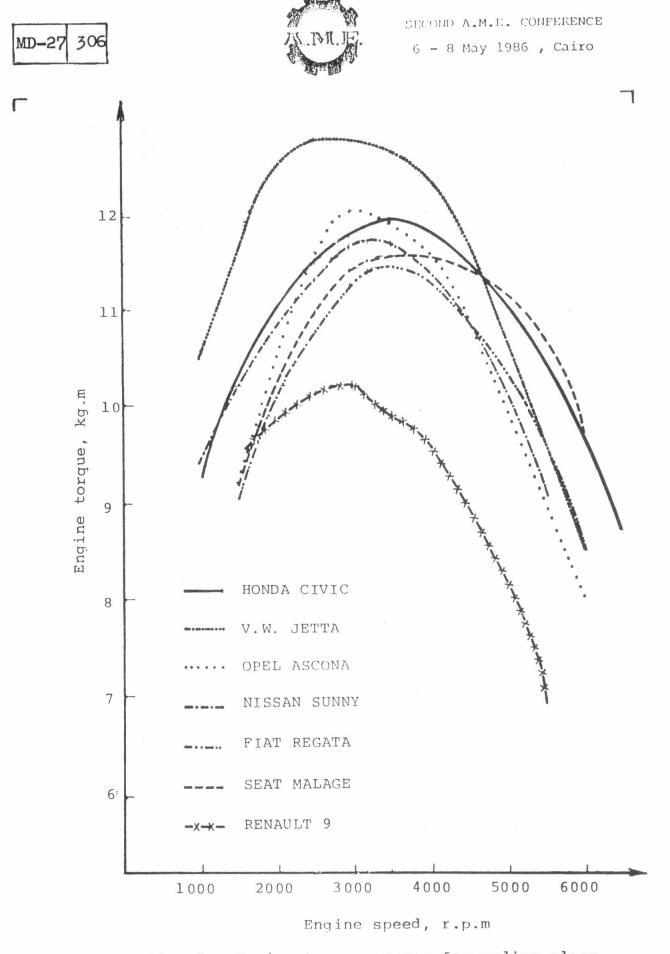


Fig. 5 : Engine torque curves for medium class passenger cars.

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The constants A,B,C,D in equation (1) could be determined by taking the values of engine power and the corresponding engine speed at four points widely spaced on the power curve between the engine speed values corresponding to max power and torque.

A special BASIC computer program (Appendix 1) has been written to calculate the constants A,B,C,D for each of the fourteen power curves.

CALCULATION OF THE GEAR RATIOS ACCORDING TO DIFFERENT METHODS.

The following methods were used to calculate the intermediate ratios while the maximum and minimum are given as vehicle data.

A special BASIC computer program (Appendix 2) has been written to calculate the gear ratios according to arithmatic, harmonic, geometric with constant root and geometric with increasing roots.

The relationships for calculating the individual ratios according to the mentioned progressions are as follows : Arithmatic :

 $i_1 - i_2 = i_2 - i_3 = \dots = i_{n-1} - i_n = const$

Harmonic :

 $1/i_2 - 1/i_1 = 1/i_3 - 1/i_2 = \dots = 1/i_{n-1} - 1/i_n = constant$

Geometric with constant root :

$$i_1/i_2 = i_2/i_3 = \dots = i_{n-1}/i_n = \text{constant}$$

Geometric with increasing root :

 $\frac{i_1}{i_2} = q_1$, $\frac{i_2}{i_3} = q_2$, ..., $\frac{i_{n-1}}{i_n} = q_{n-1}$

and

.

$$q_1/q_2 = q_2/q_3 = \dots = q_{n-2}/q_{n-1} = q = constant$$

COMPUTATION OF THE WASTED POWER.

The wasted power represented by the hatched areas in Fig.l can be computed using the following mathematical integration:



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ere :	HD HD
∆ Pe	= the total wasted power, HP
v_1, \breve{v}_2	= vehicle speeds as in Fig. 1
Ft	= tractive effort given by the ideal traction
Ξt	characteristics,
	$\eta \cdot 2700/V$, Newtons
F+	- Tractive effort given by the individual clace
rt	ion curves of the mechanical transmission.
	$F_{t} = P_{e} \cdot 2 \cdot 2700/V$
	Pe : given by the equation (1)
	$V = \frac{0.577 \text{ Me} \cdot 10}{100}$
	V : given by the equation : V - it
	rd : wheel dynamic radius.
	it : total transmission ratio.
	η : total mechanical efficiency.

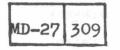
To facilitate the computation of the wasted power, a special BASIC computer program (Appendix 3) has been written.

RESULTS

The actual power delivered at wheels (areas under the stepped curves in Fig. 1), the power at wheels in case of ideal transmission (area under the hyperbolic curve in Fig. 1) were calculated in five cases for each car. In the first case the actual gear ratios of the car were considered and in the other four cases the gear ratios spaced according to the previously mentioned mathematical progressionshave been taken into account. The results of computations are shown in Table 2.

CONCLUSIONS.

- 1- Based on the calculated unobtainable power due to mechanical transmission characteristics relative to the ideal one, the geometric with constant root stands as the best progression for gear ratios spacing.
- 2- The geometric progression with increasing root gave slightly higher wasted power than in case of constant root.
- 3- The arithmatic and harmonic progressions gave approximately 30% higher wasted power relative to the geometric progression.



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Table 2 : Unobtainable power for used vehicles with different progressions.

PROGRAM TO CALCULATE THE LOSSES -----

FROGRESSION DIFFERENCE

16655.7

16780.68

FIAT UND

ARITHMATIC PROGRESSION:	19619.99
HARMONIC FROGRESSION:	19636.72
GEOMETRIC FROGRESSION:	16252.81
GEOMET.WITH INCR.ROOT:	16943.54
REAL GEAR RATIOS:	18105.14
OPEL CORSA	
ARITHMATIC PROGRESSION:	19128,95
HARMONIC PROGRESSION:	17827.43
GEOMETRIC FROGRESSION:	15993.47

MAZDA 323

GEOMET.WITH INCR.ROOT:

REAL GEAR RATIOS:

ARITHMATIC FROGRESSION:	39909.41
HARMONIC PROGRESSION:	39916.97
GEOMETRIC FROGRESSION:	23459.03
GEOMET.WITH INCR.ROOT:	27500.1
REAL GEAR RATIOS:	35542.79

NISSAN PULZAR

ARITHMATIC FROGRESSION: 15401.21 HARMONIC PROGRESSION: 15403.79 GEDMETRIC PROGRESSION: 12276.3 GEOMET.WITH INCR.ROOT: 13059.95 REAL GEAR RATIOS: 12917.37

SEAT IFIZA

ARITHMATIC PROGRESSION: 11034.9 HARMONIC PROGRESSION: 11039.1 GEOMETRIC PROGRESSION: 8740.774 GEOMET.WITH INCR.ROOT: 9387.649 REAL GEAR RATIOS: 10188.74

NISSAN SUNNY

ARITHMATIC PROGRESSION: 20988.31 HARMONIC FROGRESSION: 20772.17 GEOMETRIC PROGRESSION: 16465.96 GEOMET.WITH INCR.ROOT: 17661:31 REAL GEAR RATIOS: 17446.63

V.W.JETTA

ARITHMATIC PROGRESSION: 27963.39 HARMONIC PROGRESSION: 27966.99 GEDMETRIC PROGRESSION: 22752.44 GEOMET.WITH INCR. ROOT: 74144 97

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Table 2 continued.

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OPEL ASCONA ARITHMATIC FROGRESSION: 21287.42 HARMONIC PROGRESSION: 21296.46 GEDMETRIC PROGRESSION: 16439.63 GEOMET.WITH INCR.ROOT: 17565.11 REAL GEAR RATIOS: 17656.23 FEUGEOT 205 ARITHMATIC PROGRESSION: 27682.99 HARMONIC PROGRESSION: 27686.68 GEOMETRIC PROGRESSION: 24421.4 GEOMET.WITH INCR.ROOT: 25055.17 REAL GEAR RATIOS: 25682.6 RENAULT 5 ARITHMATIC PROGRESSION: 15689.05 HARMONIC PROGRESSION: 15690.5 GEDMETRIC PROGRESSION: 12650.9 GEOMET.WITH INCR.ROOT: 13233.69 REAL GEAR RATIOS: 13449.47 FIAT REGATA ARITHMATIC PROGRESSION: 29711.87 HARMONIC PROGRESSION: 29702.62 GEOMETRIC PROGRESSION: 22108.2 GEOMET.WITH INCR.ROOT: 24962.24 REAL GEAR RATIOS: 26965.1 HONDA CIVIC ARITHMATIC PROGRESSION: 25587,15 HARMONIC PROGRESSION: 25577.15 GEDMETRIC PROGRESSION: 20545.52 GEOMET.WITH INCR.ROOT: 23330.9 REAL GEAR RATIOS: 23925:69 SEAT MALAGA ARITHMATIC PROGRESSION: 34575.92 HARMONIC PROGRESSION: 34571.35 GEOMETRIC PROGRESSION: 27793.74 GEOMET.WITH INCR.ROOT: 31054.83 REAL GEAR RATIOS: 32506,97 RENAULT 9 ARITHMATIC PROGRESSION: 18127.82 HARMONIC PROGRESSION: 18131.22 GEDMETRIC PROGRESSION: 12927.15 GEOMET.WITH INCR. ROOT: 14932.5 REAL GEAR RATIOS: 16881.03

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Appendix 1 : Program to calculate constants of power curves.

5 REM PROGRAM TO CALCULATE CONSTANTS OF POWER CURVES 10 REM USING PROGRAM TO SOLVE SYSTEM OF LINEAR EQUATIONS 11 LPRINT"VALUES OF CONSTANTS OF POWER CURVES" 12 LPRINT"------" 13 LPRINT 20 N=4 SO DIM A(N, N+1), B(N), X(N)35 READ T\$ ' TYPE OF VEHICLE (="END" TO FINISH) 36 IF T#="END" THEN 340 37 READ RMAX, FMAX 'rpm at max power , max power 40 FOR I=1 TO N 45 READ REV, POWER 'one point on the curve 50 FOR J=1 TO N 60 A(I,J)=(REV/RMAX)^J 70 NEXT J 80 B(I)=POWER/PMAX 90 NEXT I 100 FOR I=1 TO N 110 A(I, N+1) = B(I)120 NEXT I 130 FOR K=1 TO N 140 = T = 1/A(K,K)150 FOR J=K TO N+1 160 A(K,J) = A(K,J) * T170 NEXT J 180 FOR J=1 TO N 190 IF K=J THEN 240 200 T=A(J,K) 210 FOR I=K TO N+1 220 A(J,I) = A(J,I) - T * A(H,I)230 NEXT I 240 NEXT J 250 NEXT K 260 FOR I=1 TO N $270 \times (I) = A(I, N+1)$ 280 NEXT I 285 LPRINT"TYPE OF VEHICLE:", T\$ 286 LPRINT"VALUES OF CONSTANTS =" 290 FOR I=1 TO N 300 LPRINT X(I), 310 NEXT I 320 LPRINT : LPRINT 330 6010 35 340 END

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Appendix 2 : Program to calculate speed ratios according to different progressions.

CALCULATION OF SPEED RATIOS ACCORDING TO " 30 LFRINT" DIFFERENT FROGRESSIONS 1.1 40 LFRINT" 50 LPRINT" 55 LPRINT 56 LPRINT"FIRST", "SECOND", "THIRD", "FOURTH", "FIFTH" 57 LPRINT"SPEED", "SPEED", "SPEED", "SPEED", "SPEED" 75 READ T\$, FI, LA, N 76 IF T#="END" THEN 540 80 LFRINT 100 LPRINT 110 LFRINT"VEHICLE TYPE: "; T\$ 120 LFRINT"ARITHMATIC FROGRESSION" 130 I(1)=FI 140 I(N)=LA $150 \ Q = (I(1) - I(N)) / (N-1)$ 160 LPRINT I(1), 170 FOR K=2 TO N-1 180 I(K)=I(1)-(K-1)*Q 190 LFRINT I(K), 200 NEXT K 210 LFRINT I(N) 230 LPRINT"HARMONIC PROGRESSION" 240 LFRINT I(1), 250 Q=(1/I(N)-1/I(1))/(N-1) 260 FOR K=2 TO N-1 270 I(K)=1/I(1)+(K-1)*0 280 I(K)=1/I(K) 290 LFRINT I(K), 300 NEXT K 310 LERINT I(N) 330 LPRINT"GEOMETRIC PROGRESSION" 340 LPRINT I(1), 350 $Q = (I(1) / I(N)) \cap (1 / (N-1))$ 360 FOR K=2 TO N-1 370 $I(K) = I(1) / (O^{-}(K-1))$ 380 LPRINT I(K), 390 NEXT K 400 LFRINT I(N) 420 LPRINT "GEOMETRIC WITH INCREASING ROOTS" 430 0=1.1 440 IF N=5 THEN 470 450 Q1=(I(1)/(I(N)*Q^3))^(1/3) 460 GOTO 480 470 D1=(I(1)/(I(N)*D 6)) (1/4) 490 LPRINT I(1), 490 FOR K=2 TO N-1 500 I(K)=I(K-1)/(Q1*Q^(N-K)) 510 LPRINT I(K), 520 NEXT K 530 LFRINT I(N) 535 GOTO 75

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Appendix 3 : Program to calculate the unobtainable power.

10 REM PROGRAM TO CALCULATE THE LOSSES PROGRAM TO CALCULATE THE LOSSES" 20 LPRINT 30 LPRINT " 'type of vehicle 40 READ T事 50 IF T#="END" THEN 480 60 LPRINT:LPRINT"TYPE OF VEHICLE:",T≸ 70 REM INPUT MAX POWER, REV. AT MAX POWER, DYN. RAD., 80 REM FINAL DRIVE GEAR RATID, NO OF SPEEDS 90 READ PMAX, NN, RD, IO, N 95 REM INFUT FIRST AND LAST SPEED RATIOS 96 READ G(1), G(N) 130 READ A, B, C, D (constants of power curves 140 LPRINT"GREAT AREA", "SMALL AREA", "DIFFERENCE" 150 FOR J=1 TO 5 // different progressions 160 ON J GOTO 170,190,210,230,235 170 LERINT"ARITHMATIC PROGRESSION: " 180 GOTO 240 190 LPRINT"HARMONIC PROGRESSION:" 200 GOTO 240 210 LFRINT"GEOMETRIC FROGRESSION: " 220 GOTO 240 230 LPRINT"GEOMETRIC WITH INCREASING ROOT:" 234 GOTO 240 235 LPRINT"REAL GEAR RATIOS:" 240 FOR I= 2 TO N-1 250 READ G(I) gear ratios 260 NEXT I 270 SUMDIF = 0280 SUMF1=0 270 SUMF2=0 291 FOR I=1 TO N 292 V(I)= .377*NN*RD/(ID*G(I)) 293 NEXT I 300 K1= 2700*PMAX*.9 310 FOR I=2 TO N 'different gears 320 F1 = K1*(LOG(V(I)) - LOG(V(I-1)))330 K2 = IO*G(I)/(.377*RD*NN) 340 A1=(PMAX*,9*2700)*(A*K2*V(I)+B*K2^2*(V(I))^22/2 +C*K2^3*(V(I))^3/3+D*K2^4*(V(I))^4/4) 345 A2=(PMAX*.9*2700)*(A*K2*V(I-1)+B*K2^2*(V(I-1))^2/2+ C*R2^3*(V(I-1))^3/3+D*R2^4*(V(I-1))^4/4) 350 F2 = A1 - A2360 SUMF1=SUMF1+F1 370 SUMF2=SUMF2+F2 380 DIF=F1-F2 390 SUMDIF=SUMDIF+DIF 400 LFRINT F1,F2,DIF 410 NEXT I 420 LERINT"SUMMATION:" 430 LERINT SUMF1, SUMF2, SUMDIE 440 LFRINT 450 NEXT J 460 LFRINT: LFRINT