

## WEAR BEHAVIOR OF HYBRID COMPOSITE REINFORCED WITH TITANIUM DIOXIDE NANOPARTICLES

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### ABSTRACT

The aim of the present study is to investigate the influence of polymerization times, normal loads and titanium dioxide nanoparticles content on the wear of hybrid composite resin reinforced with titanium dioxide ( $\text{TiO}_2$ ) nanoparticle. The materials used are hybrid composite resin and titanium dioxide nanoparticles ( $\text{TiO}_2$  nanoparticles). Four groups of composite resin samples are prepared; one as received and three groups reinforced with  $\text{TiO}_2$  nanoparticles in contents of 0.1, 0.2 and 0.3 wt. %. Hybrid composites resin is manually mixed with  $\text{TiO}_2$  nanoparticles. The resulting blend is packed into plastic cylindrical bars. The samples are then cured from both sides for 10, 20, 40, 60 and 80 seconds using a visible light curing unit. To determine the wear, all samples are tested with two-body abrasion, reciprocating sliding apparatus at room temperature. The test conditions are; sliding velocity= 60 strokes/min, load= 6, 8, 10, 12 and 14 N, time= 60 seconds. Results show that the wear decreases with the increase of polymerization time at all normal loads. Results showed also that wear depends on the normal load. The wear initially decreased and reached a minimum at a concentration of 0.1 wt. %  $\text{TiO}_2$  nanoparticles, above 0.1 wt. %  $\text{TiO}_2$  nanoparticles, the aggregation of  $\text{TiO}_2$  nanoparticles led to increase of the wear. The present study suggests that in order to minimize wear, it is important to use relatively higher polymerization time, lower  $\text{TiO}_2$  content and lower force of chewing.

**Keywords:** *Polymerization time, dental nanocomposite, wear, titanium dioxide, nanoparticles, hybrid composite resin, normal load.*

### 1. INTRODUCTION

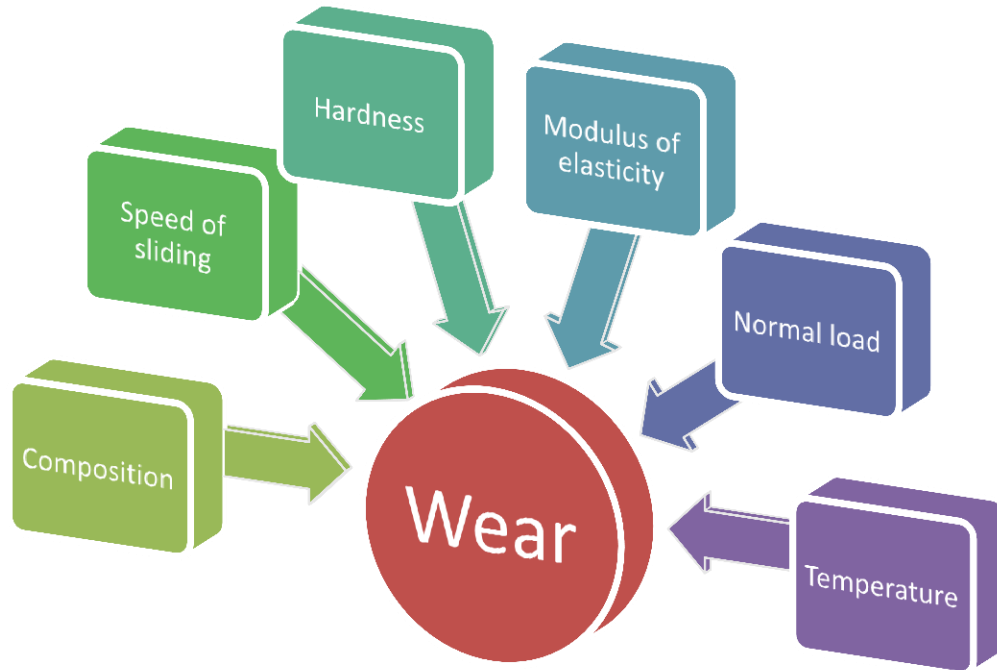
Dental composite restorative materials are made of a highly cross linked dimethacrylate resin strengthened with silanated inorganic filler particles (about 50 vol. %) [1]. Composite resins gain more importance and popularity for the restoration of all cavity classes because of their excellent aesthetic properties. However, clinically, their comparatively poor wear resistance is still considered as a factor that participates to materials' failure [2]. Wear appears as a surface damage or elimination

of material from one or both sides of solid surfaces that are in contact during motion. In most cases, wear happens by surface interactions on the surface non uniformity [3]. Wear resistance is very significant to dental composite resins, specially when being used in heavily loaded regions. Failure rates are higher for larger restorations, and may still be an important mode of failure for patients with bruxism and clenching customs. Therefore, discussing the friction and wear behavior is of pivotal importance to the advance of dental material development [4].

Refinements of mechanical properties of the composite materials have permitted its use in posterior teeth with greater reliability than was the case some years ago. These refinements included; development of smaller particle sizes of filler, better bonding systems, curing improvements and sealing systems [5]. Ayman et al., [6], concluded that the change of wear resistance depends

on the size and volume fraction of the nanofilling materials.

The main parameters affecting the wear are shown in Fig. 1. The contact temperature has an important effect on the wear resistance [7]. Abrasive wear would rise as the temperature increases, because the hardness and yield strength decrease [8].



**Fig. 1.** Main factors affecting the wear behavior.

The normal load affects strongly the wear rate. Wear rate increases with the increase in normal load for glass fiber, PTFE and nylon. The shear force and frictional thrust also increase with the increase in applied load and these increments accelerate the wear rate [9]. The rate of abrasive wear was found to increase slightly with the rise in sliding speed in the range from 0 to 2.5 m/s (0 to 8.2 ft/s). This rise in wear may be attributed to frictional heating [8]. It was found that the mechanical wear of teeth increased with increasing the velocity of brushing due to the accelerated motion of abrasive particles [10, 11]. Modulus of elasticity describes

stiffness, a measure of the resistance to deformation under load of the material, with a high number indicating greater stiffness [12]. Also the composition of the materials has an important influence on the wear behavior. Aljosa et al., [13], illustrated that the inorganic filler type and concentration have the major effect on the mechanical behavior of the composites. Filler particles dimensions have been changed and decreased over the years, down to the nano-dimension, in order to develop better material properties. Nanoparticles have high surface area and unparalleled physicochemical characteristics, and they

can influence the overall bulk material lineaments. Further, high inorganic filler content reduces the volume of the organic matrix that causes unfavorable material characteristics, such as: low wear resistance, low mechanical strength, polymerization contraction, high coefficient of thermal expansion, etc.

Several studies have examined the influence of normal load and titanium dioxide nanoparticles weight percent on wear resistance. Manhart et al., [14], found that the wear resistance of composite resins significantly improved with increased filler loading and with decreased average filler particle size. Higher wear rates are related to the larger filler particles in the composite materials. Agarwal et al., [15], revealed that wear rate increases with the increase in the value of normal load of SiC filled chopped glass fiber reinforced epoxy composite. Ramadan et al., [16], showed that wear of acrylic tooth slightly increased with increasing the normal load. At a normal load of 3 N the mechanical wear reached 16.6

mg. This value increased to 22 mg at normal load of 5 N. Chang et al. [17] studied the influence of TiO<sub>2</sub> nanoparticles on short fiber reinforced epoxy under various loading conditions. They found that the addition of 5 vol. % of titanium dioxide nanoparticles could significantly decrease the wear rate of epoxy composites than padding only by conventional fillers.

The goal of the present work is to study the effect of polymerization times, normal loads, and reinforcement weight percent on the wear behavior of dental hybrid composite resin filled with titanium dioxide nanoparticles.

## 2. MATERIALS

The materials used are hybrid composite resin of shade A1 and TiO<sub>2</sub> nanoparticles of 25 nm diameter. Detailed information about the materials used in the present work is shown in Tables 1 and 2.

**Table 1:** Specifics of composite resin

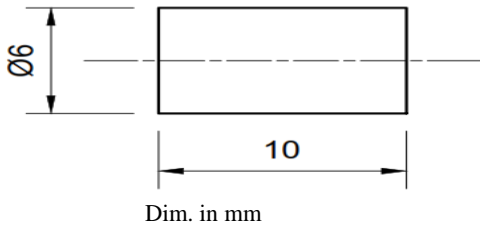
Description	Classification	Manufacturer	Shade	Curing	Lot no.
Visible light cure, Resin-based dental restorative material	Hybrid composite	Prime-Dent, U.S.A.	A1	Light cure	YL08Q

**Table 2:** Specifics of TiO<sub>2</sub> nanoparticles

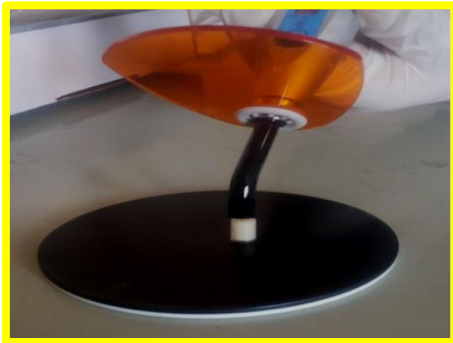
Diameter	Density	Surface area
21 nm	4 g cm <sup>-3</sup>	50 m <sup>2</sup> g <sup>-1</sup>

### 3. EXPERIMENTAL METHODS

In this study there are four experimental groups consisting of three hybrid composites resin containing TiO<sub>2</sub> nanoparticles in different contents of 0.1, 0.2 and 0.3 wt% and one as received group, contained no TiO<sub>2</sub> nanoparticles. The method of preparation of samples is illustrated in Ref. [18]. The samples have cylindrical form with 6 mm diameter and 10 mm height as illustrated in Figs.2.



Dim. in mm  
**Fig.2** Dimensions of specimen.



**Fig.3** Polymerization of the samples by light emitting diode source (LED).

### 4. POLYMERIZATION OF SAMPLES

The light source used in this research to polymerize samples is blue light emitting diode (LED). Figure 3 shows the polymerization of the samples by light emitting diode source. Specifications of the LED are shown in the Table 3. The light polymerization modes used in this research were as follows: gradually strong, flashing and strong mode.

**Table 3:** Specifications of the Light Emitting Diode (LED)

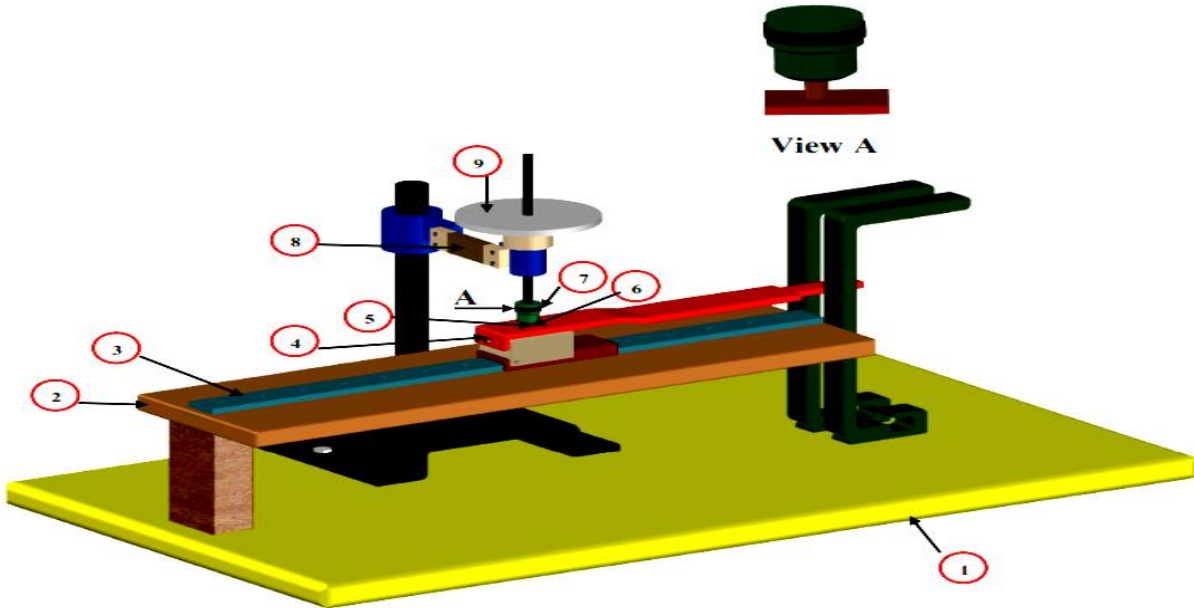
Intensity (mW/cm <sup>2</sup> )	Spectral emission (nm)	Solidify time and depth
1200-2000	420-480	5s/3mm

### 5. WEAR TEST

To study the wear of the composite, cylindrical samples (6 mm in diameter and 10 mm in length) of each condition were made in bars with 6 mm diameter and 10 mm height. Each sample is held stationary in a jig under different normal loads (6, 8, 10, 12 and 14 N) against emery paper (1000 grit

size) counter face using two-body abrasion test. The emery paper is attached to the table of linear bearing. The table moves reciprocating motion at a velocity of 60 strokes/min. Each sample is scraped for a distance of 6 m on a fresh emery surface. To find out the accurate weight loss, the specimens are weighted before and after wear test, then wear is determined by the weight loss using digital balance of±

0.0001g accuracy. Figure 4 shows two-body abrasion, reciprocating sliding apparatus.



**Fig. 4** Two-body abrasion, reciprocating sliding apparatus (1) Base plate (2) Plate (3) Linear bearing (4) Table (5) Emery paper (6) Test sample (7) Sample jig (8) Load cell (9) Normal load

## 6. RESULTS AND DISCUSSION

In order to investigate the influence of polymerization time, normal load and titanium dioxide nanoparticles content on the wear of tested samples, a series of experiments were carried out at various curing times, normal loads and titanium dioxide nanoparticles weight content. Wear versus polymerization time of the gradually strong mode, flashing mode and strong mode are shown in Figs. 5, 6 and 7, respectively, for as received samples. Figs. 5, 6 and 7, revealed that wear decreases with increasing polymerization time at all normal loads used. The reason for the decrease in wear is attributed to increase the hardness [18]. As it is evident in Figs. 5, 6 and 7 the hybrid composite cured at 80 s exhibited the lowest wear followed by the hybrid composite cured at 60 s, then the

hybrid composite cured at 40 s, then the hybrid composite cured at 20 s and lastly the hybrid composite cured at 10 s. the hybrid composite cured at 80 s and the hybrid composite cured at 60 s are significantly better than the hybrid composite cured at 20 s and the hybrid composite cured at 10 s.

The wear appears to depend on the normal load; as the normal load increases, the wear first increases, and then falls. The decrease in the wear at high normal loads may be due to the decrease in the sliding speed of the apparatus at the high normal loads, as the sliding speed decreases, the wear decreases. Fig. 5 shows that when the normal load is above 6 N, the wear increases up to 8 N. Above this load and up to about 14 N, the wear decreases with increasing the normal load. As indicated in Fig. 5, the higher wear is produced by the normal load 8 N, while

the low wear is produced by the normal load 14 N.

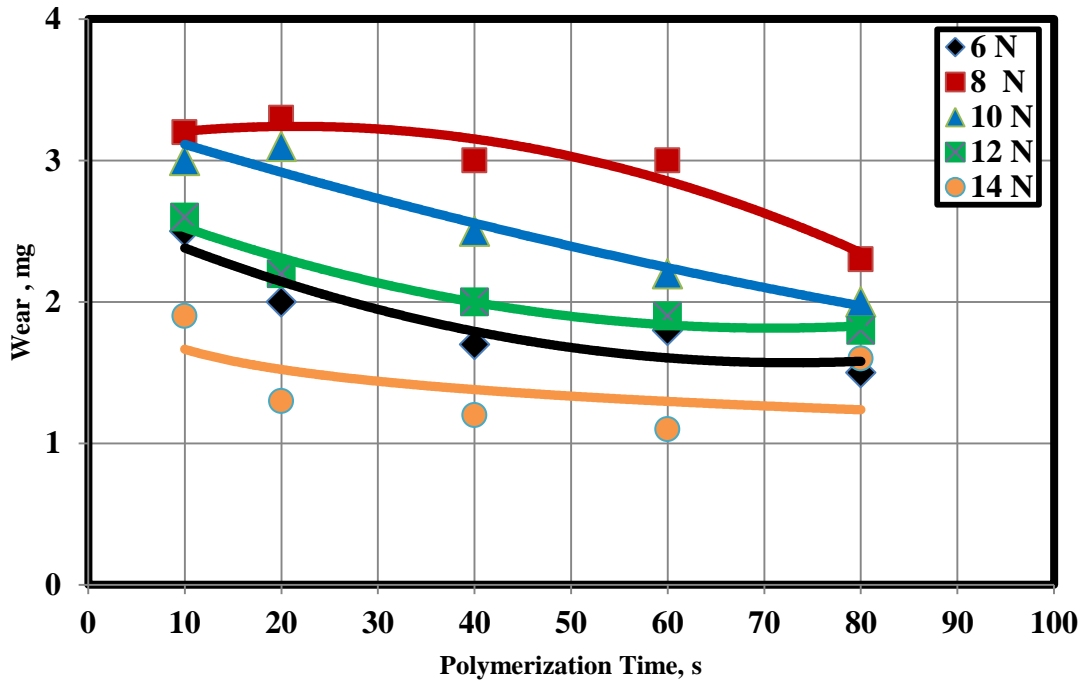


Fig. 5. Effect of polymerization time on wear for as received samples in gradually strong mode.

Also Figs. 6 and 7 show that when the normal load is above 6 N, the wear increases with increasing the normal load up to 12 N. Above this load up to about 14 N, the wear decreases with increasing the normal load. The reason for the increase in the wear up to 12 N may be attributed to the increase in the contact area when the normal load is increased. As illustrated in Fig. 6, the higher wear is produced by the normal load 12 N, while the low wear is produced by the normal load 14 N. Fig. 7 revealed that the

highest value of the wear is observed in the normal load 12 N, while the lowest value of the wear is observed in the normal load 6 N. It observes from the results that the hybrid composite resin cured at 80 s gives the lowest value of the wear. For the gradually strong and flashing modes specimens, the normal load 14 N gives the lowest value of the wear, while for the strong mode specimens the normal load 6 N gives the lowest value of the wear.

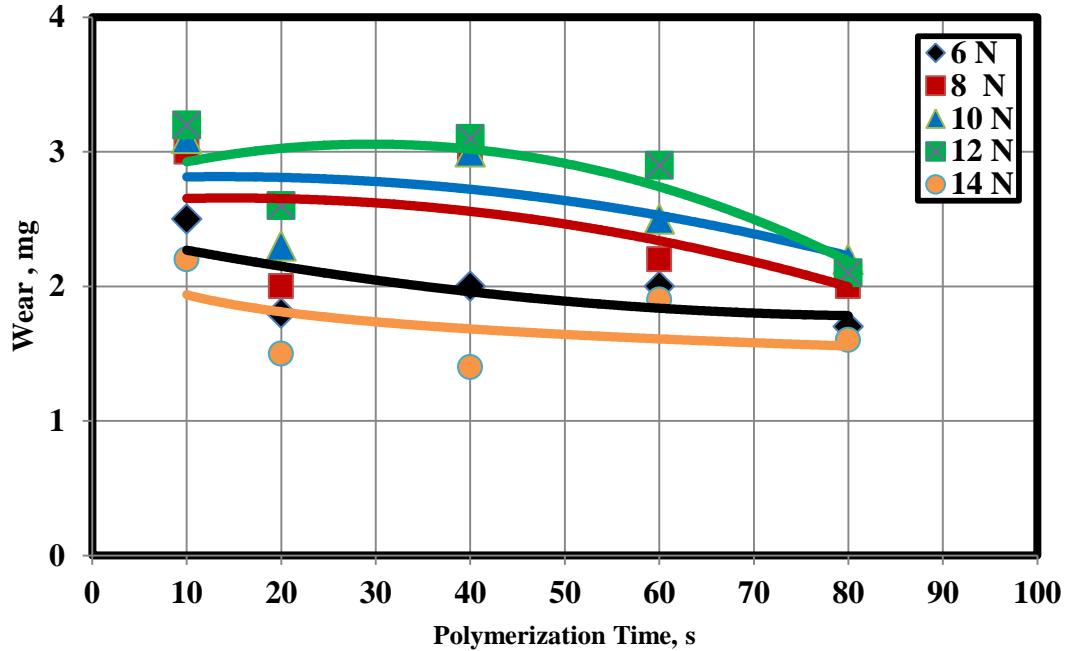


Fig. 6 Effect of polymerization time on wear for as received samples in flashing mode.

The effect of concentration of  $\text{TiO}_2$  nanoparticles on the wear of the hybrid composite resin cured with gradually strong, flashing and strong modes at various normal loads are displayed in Figs. 8, 9 and 10, respectively at 80 second polymerization time. It is evident that the wear first decrease when  $\text{TiO}_2$  NPs increased from 0 wt. % to 0.1 wt. % and then increase when  $\text{TiO}_2$  increased from 0.1 wt. % to 0.3 wt. % for the three modes at all values of normal loads. The decrease in the wear up to 0.1 wt. % of  $\text{TiO}_2$  NPs may be attributable to higher contact surface of nano fillers with the organic matrix, which leads to improve the material strength [19]. Therefore, the wear will decrease. The reason for the increase in wear after 0.1 wt. % of  $\text{TiO}_2$  may be attributed to an increment the concentration of  $\text{TiO}_2$  nanoparticles. The interface between nanoparticles and a polymer matrix can transfer stress, which is beneficial for the

enhancement of the tensile strength of composite films. However, with increasing the concentration of nanoparticles, aggregation occurs, which leads to a decrease in the interaction between particles and polymer resulting in defects in the composites [20]. So the wear will increase. Fig. 8 revealed that the hybrid composite containing 0.1 wt. %  $\text{TiO}_2$  nanoparticles exhibited the lowest wear value followed by the hybrid composite containing 0.2 wt. %  $\text{TiO}_2$  nanoparticles, then the hybrid composite containing 0 wt. %  $\text{TiO}_2$  nanoparticles and lastly the hybrid composite containing 0.3 wt. %  $\text{TiO}_2$  nanoparticles. In other words, the hybrid composite containing 0.1 wt. %  $\text{TiO}_2$  nanoparticles has a higher resistance to wear than the hybrid composite resin containing 0, 0.2 and 0.3 wt. %  $\text{TiO}_2$  nanoparticles.



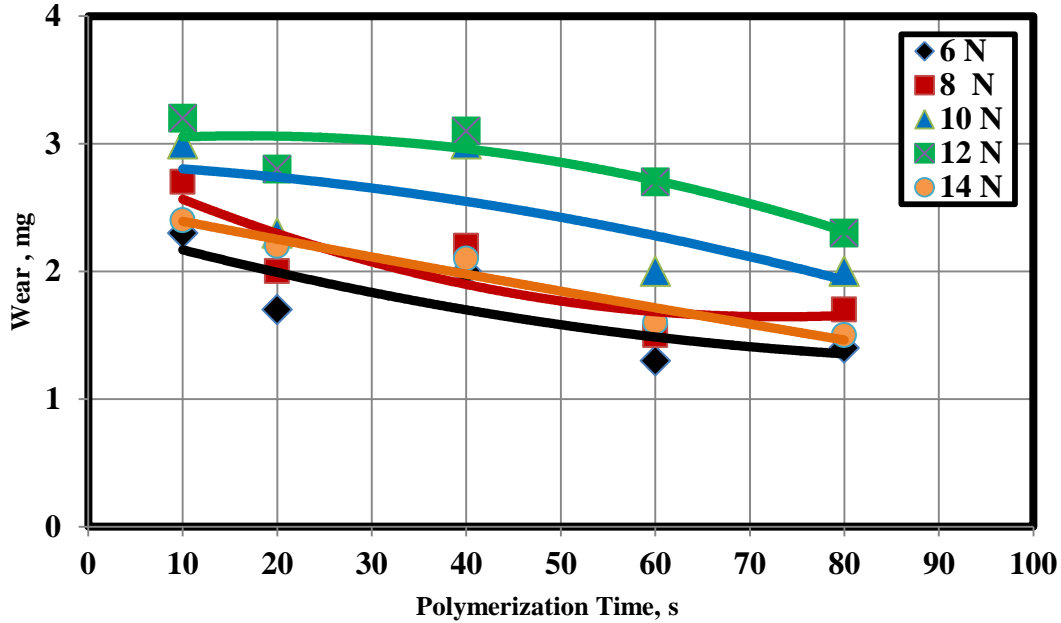


Fig. 7 Effect of polymerization time on wear for as received samples in strong mode.

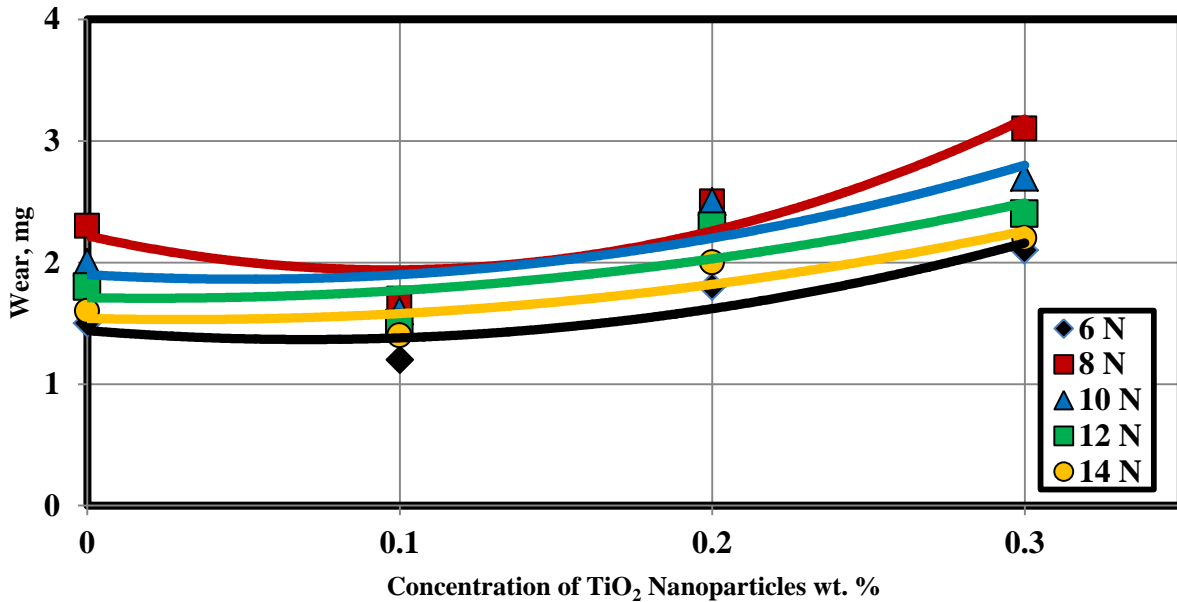


Fig. 8 Effect of concentration of TiO<sub>2</sub> nanoparticles on wear of gradually strong mode samples at 80 second.

Regarding to the normal load, it is clear that the wear first increase then decreases with increasing normal load from 6 to 14 N. the reason for this behavior was discussed in Fig. 5 page 7. Figs. 8 shows that when the normal load is above 6 N, the wear increases with increasing the normal load

up to 8 N. Above this load up to about 14 N, the wear decreases with increasing the normal load. The wear is higher for the normal load 8 N followed by the normal load 10 N, then the normal load 12 N, then the normal load 14 N and lastly the normal load 6 N. So the normal load 6 N has the



highest resistance for wear. As shown in Figs. 9 and 10, the wear first increases when the normal load increased from 6 N to 10 N and then decrease when the normal load increased from 10 N to 14 N. From Figs. 9 and 10, it is clear that the normal load 6 N gives minimum wear, while the normal load 10 N gives maximum wear. These results

demonstrate that wear resistance of the hybrid composite resin is improved remarkably by adding a small content of TiO<sub>2</sub> and by using low normal load. This study suggests that in order to optimize wear, it is important to use high polymerization time, low content of TiO<sub>2</sub> nanoparticles and low masticatory forces.

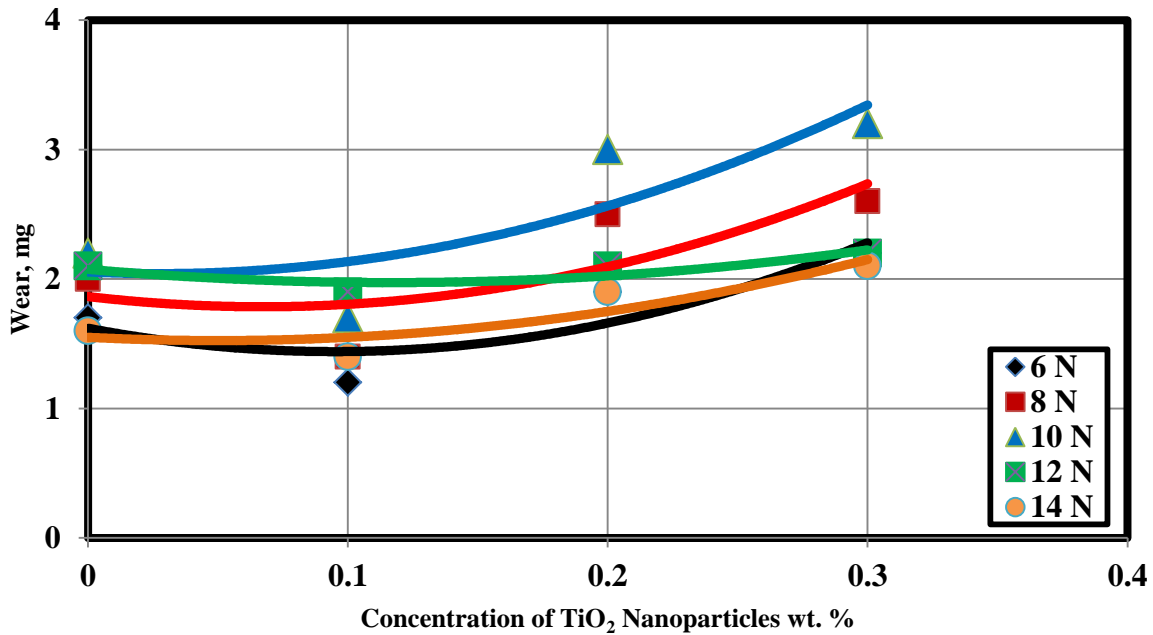


Fig. 9 Effect of concentration of TiO<sub>2</sub>nanoparticles on the wear of flashing mode samples at 80 second.

## 7. MICROSCOPIC EXAMINATION

The surface of the hybrid composites was observed by optical microscope to study the effect of polymerization time on the surface morphology of the composite samples. Fig. 11 (a-e) shows the morphology of surfaces of strong mode light cured samples for as

received condition at 10, 20, 40, 60 and 80 seconds polymerization time. From Fig. 11 (a-d), it is clear that the surface of samples contains white bubbles, while Fig. 11 (e) shows that the surface of sample has brown bubbles. Fig.11 (d) demonstrates presence of small particles of debris on the surface of sample.

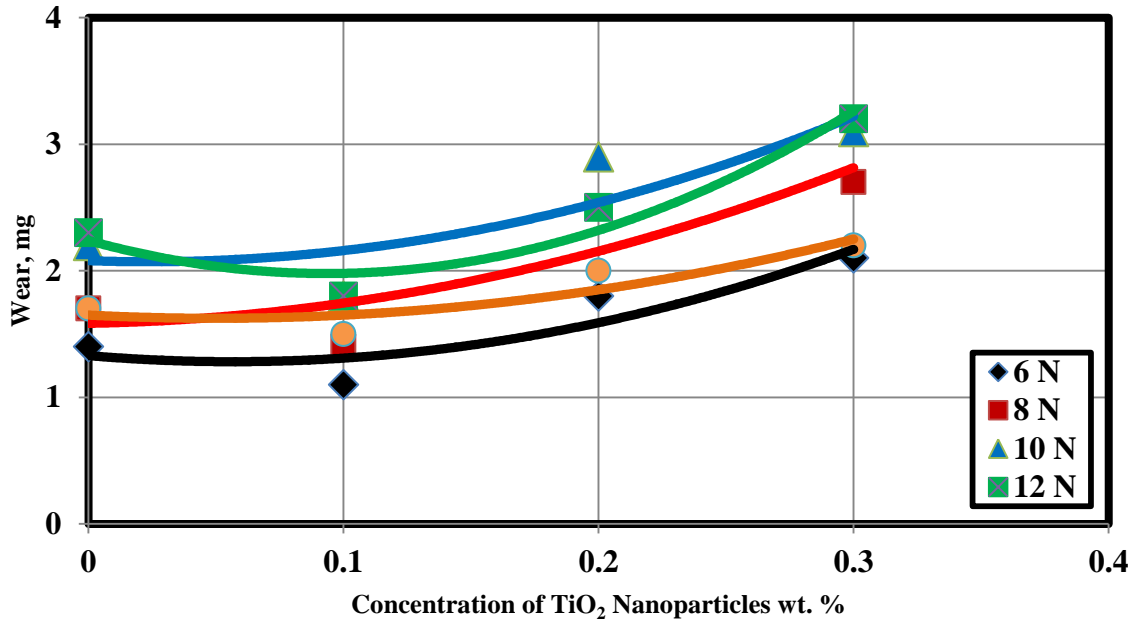


Fig. 10 Effect of concentration of TiO<sub>2</sub> nanoparticles on the wear of strong mode samples at 80 second.

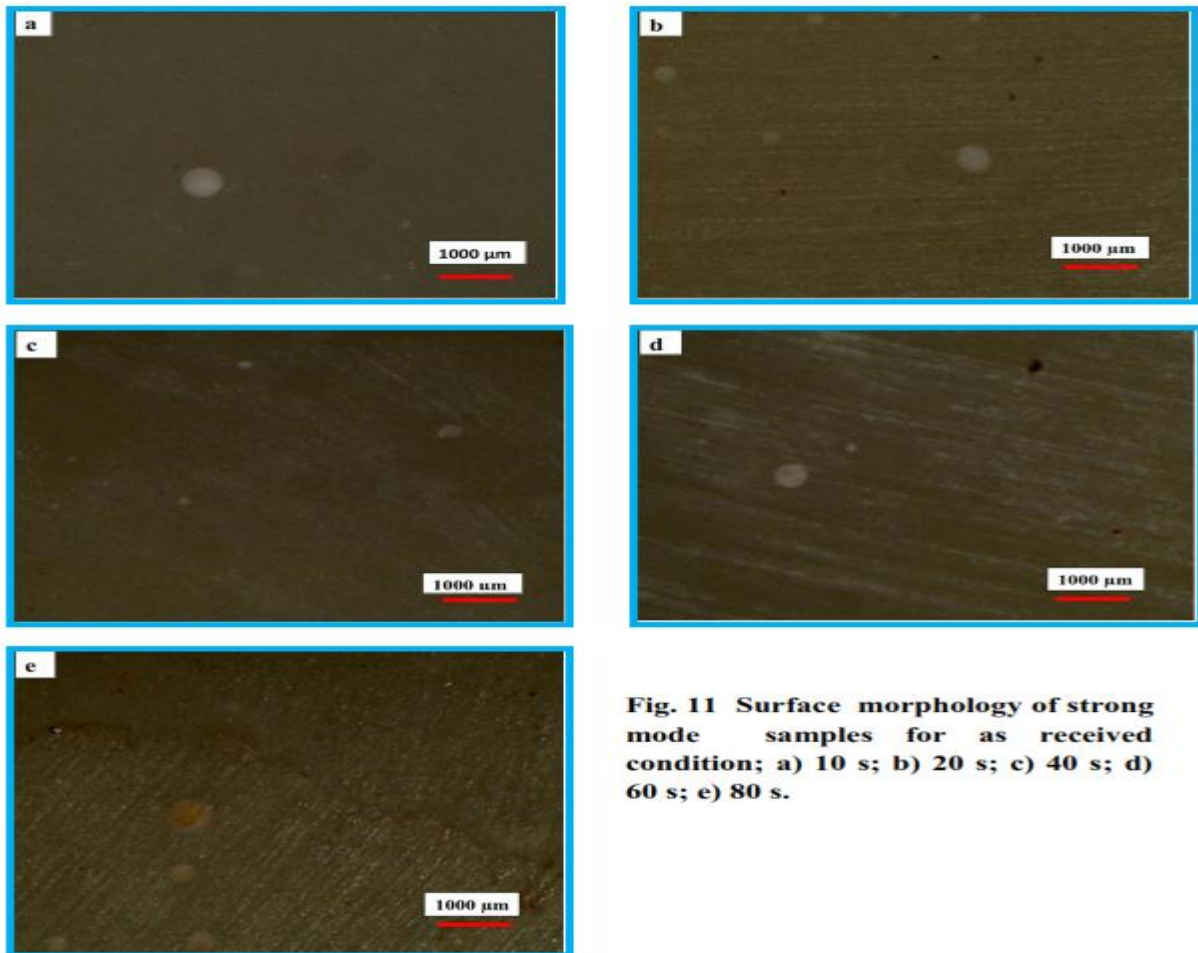


Fig. 11 Surface morphology of strong mode samples for as received condition; a) 10 s; b) 20 s; c) 40 s; d) 60 s; e) 80 s.

## 8. CONCLUSIONS

From the present study on the hybrid composite resin and nanocomposite resin, the following conclusions can be drawn:

1. Wear decreases with increasing polymerization time at all normal loads used for as received group.
2. Wear first increases and then decreases with increasing the normal load for all tested samples.
3. The hybrid composite containing 0.1 wt. % TiO<sub>2</sub> nanoparticles appears to exhibit significantly higher wear resistance compared to the hybrid composite containing 0.2 and 0.3 wt. % TiO<sub>2</sub> nanoparticles as well as unfilled composites with no TiO<sub>2</sub> nanoparticles.
4. Polymerization time, normal load and TiO<sub>2</sub> nanoparticles content have significant influence on the wear results of the tested composite resin.

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## سلوك التآكل لحشوة الراتنج المركب المدعمة بحبيبات ثاني اكسيد التيتانيوم النانوية

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### الملخص:

يهدف هذا البحث الي دراسة تاثير زمن التجفيف والاحمال العمودية و نسبة حبيبات ثاني اكسيد التيتانيوم النانوية علي سلوك التآكل لحشوة الراتنج المركب المملوءة بحبيبات ثاني اكسيد التيتانيوم النانوية. تم استخدام حشوة الراتنج المركب و حبيبات ثاني اكسيد التيتانيوم النانوية لتحقيق هذا الهدف. تم تجهيز أربعة مجموعات من العينات واحدة بدون حبيبات ثاني اكسيد التيتانيوم النانوية والثلاثة مجموعات الاخرى تحتوي علي نسب مختلفة من حبيبات ثاني اكسيد التيتانيوم النانوية 0.1 و 0.2 و 0.3 % بالوزن. عملية الخلط تمت يدويا ثم تم وضع الخليط في أسطبة من البلاستيك ثم تم تجفيف العينات باستخدام جهاز التجفيف الضوئي من الطرفين لمدة 10 و 20 و 40 و 60 و 80 ثانية. وتم تحديد التآكل الحادث في العينات باستخدام اختبارالتآكل القطعي ثنائي الأجسام عند الطرف التالية: سرعة الانزلاق= 60 مشوارلكل دقيقة ، الحمل =6,8,10,12,14 نيوتن، زمن الاختبار = 60 ثانية. وجد أن التآكل يقل مع زيادة زمن التجفيف عند كل الاحمال المستخدمة .كما وجد أن التآكل يعتمد على الاحمال العمودية المستخدمة. كما تبين ان اضافته نسب كبيره من حبيبات ثاني اكسيد التيتانيوم النانوية فوق ( 0.1 % بالوزن) الي حشوة الراتنج المركب تؤدي الي زيادة التآكل ، بينما اضافة نسب صغيرة من حبيبات ثاني اكسيد التيتانيوم النانوية اقل من ( 0.1 % بالوزن) الي حشوة الراتنج المركب تحسن من مقاومة التآكل. تقترح الدراسة الحالية إلى أنه من أجل تقليل التآكل من المهم استخدام زمن التجفيف العالي نسبياً و نسب صغيرة من حبيبات ثاني اكسيد التيتانيوم النانوية وقوة مضغ منخفضة .