EXPERIMENTAL AND MATHEMATICAL MODELING STUDY FOR SOLAR DRYING OF MINT

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ABSTRACT

Mint plant was dried using greenhouse solar dryer. Two of the forced convection operating modes (continuous and intervals) were used and compared with the open sun drying method. The drying kinetics of mint (Mentha spicata L.) in terms of moisture content, moisture ratio, drying time and drying rate was investigated. The continuous forced convection mode gives the highest drying rate for mint than the interval mode and open sun drying. The drying data of solar and open sun drying of mint were fitted to ten thin layer drying models and the Modified Henderson and Pabis model satisfactorily described the drying behavior of mint with highest R^2 (0.99) and lowest P and RMSE values than other models. The results of the study are very useful for commercial scale drying of mint to optimize the drying process and to achieve a superior quality dried product.

INTRODUCTION

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Product quality and consequently earnings are significantly influenced by the drying regime. Hot air drying has some common problems such as poor rehydration characteristics and loss of nutrients (Kocabiyik et al., 2014). Generally, increasing the temperature and velocity shortens the drying time. However, for heat-sensitive products, such as food and pharmaceutical products high temperature decreases product quality (Kumar et al., 2015). Essential mint oils are retained to a greater extent when plants are dried under ambient conditions, compared to sun drying or forced air. Essential oil composition and quality are greatly influenced by oven drying temperature. About 75.7% of essential oils are lost during oven drying at 60°C than at 30°C (Baydar and Erbas, 2009). In most developing countries such as Egypt, the conventional sun drying technique for agricultural products is traditionally performed by spreading the produce on an open floor/field under the sun for a period of time and until the desired level of moisture content is reached (Kishk et al., 2019). However, the contamination with dust, soil, sand particles, and insects are some problems associated with this method (Sallam et al. 2015; Sreekumar et al., 2008). Besides being labor- and time-intensive method, uncontrolled sun drying is usually accompanied with nutritional degradation, flavor and color changes and reduction of functionality (Rabha et al., 2017). To overcome previous problems, solar drying method could be used to dry agriculture products instead of traditional sun drying method as the drying process takes place in enclosed structures (El-Sebaii et al., 2002). Using solar energy in the drying process reduces the use of fossil fuels (coal, gas, and oil) leading to a reduction in pollutant emissions (Santos et al., 2005). Solar drying as a mean of food preservation has been considered one of the most promising venues for utilization of solar energy (Sekyere et al., 2016). The use of solar dryers significantly reduces drying time and prevents mass losses; furthermore, product quality can be improved compared to traditional sun drying methods. Utilization of solar energy as a reliable energy source to dry foods in Egypt has a great potential, as, the annual daily average solar radiation on a horizontal plane in Egypt is 8 kWm⁻²day⁻¹ and the measured annual average daily sunshine duration is approximately 11 h (El-Beltagy et al., 2007). Thin layer drying is widely used for agricultural

products to prolong their shelf life. Among the wide range of models, thin layer drying models have found widest application because of their ease of use. They do not require evaluation of many models parameters as is common in more complex representations (Kadam et al 2011). Several researches have investigated the drying kinetics of mint leaves and evaluated various mathematical models to describe thin layer drying characteristics (Soysal, 2005; Doymaz, 2006; Özbek and Dadali, 2007; Akpinar, 2010; Kadam et al., 2011). In Egypt, the mint is usually marketed as a whole plant. However, the literature is scarce on the drying kinetics of mint as a whole plant especially in greenhouse dryers. Sallam et al. (2015) studied the drying behavior of the whole mint plant in direct and indirect solar dryers under natural and forced convection modes. They found that results indicated that drying of mint under different operating conditions occurred in the falling rate period, where no constant rate period of drying was observed. As mentioned above, the literature is scarce on the drying kinetics of mint as a whole plant especially in greenhouse solar dryer. Besides, most previous studies used small scale dryers in their investigations. Accordingly, this study aimed to investigate the drying kinetics of mint as a whole plant using pilot scale greenhouse solar dryers considering the effect of the forced convection operation mode (continuous and intervals). In addition, ten mathematical models were used to fit the drying curves of mint.

MATERIALS AND METHODS

In this study, greenhouse dryer used to dry mint plant and compared with the traditional sun drying method. Two greenhouse dryers were built and operated by two modes of forced convection. One unit operated by continuous forced convection where the air pump operated continuously during the drying period, while the other unit operated by the interval mode where the air pump connected with an electronic timer to be operated every 15 minutes (15 min ON/ 15 mint OFF). The performance of two modes compared with the open sun drying.

Greenhouse solar dryer construction

Two identical plastic greenhouse dryers were designed, built and installed on the roof of the Agricultural Engineering Department at Suez Canal University (latitude of 30.62°, longitude 32.27° and 5m above sea level)

during October 2018. As shown in Figs (1 and 2) the geometric shape of the greenhouse type solar dryer was Quonset established on an iron base of gross dimensions (2.0 m long, 1.0 wide, and 0.9 m high). The dryer has a drying chamber with a gross dimension of 2.0 long, 1.0 wide, and 0.1 m high and a door of 0.75 x 0.45 m located at the front side of the dryer for loading, unloading and collecting samples of mint during the drying process. The solar dryers were covered by a single layer of polyethylene sheet of 50 µm thick and with effective transmittance of 91 %. To maintain the durability of the structural frame of plastic greenhouses and prevent pad side effects of wind load on the polyethylene cover, ten tensile compacted plastic wires (2 mm diameter) were tied and fixed throughout the walls. The solar dryers were orientated in the East-West direction to maximize the intensity of the solar radiation. A perforated wire was fixed at 15 cm over the bottom of the greenhouses forming a plenum chamber under the wire netted floor. Each solar dryer is equipped with a centrifugal fan model (SMB-10, USA) with a power of 0.75 hp electric motor and equipped with an inverter to control the fan air flow rate. A PVC pipe with a diameter of 5.08 cm was used to carry out the air from the dryer to the outside. An open window with a surface area of 0.053 m^2 (0.35 m long and 0.15 m wide) was positioned at the top of the opposite side of the suction fan position for air intake through each dryer. Drying air was cycled through the solar dryer which continuously had a hot air heated by solar energy. The drying air was continuously introduced from the top position of the solar dryer and leaves through the bottom position under the drying chamber via the suction fan. The air fan of one greenhouse unit connected with an electronic timer to be operated by the interval mode (15 min ON/ 15 min OFF). The air flow rate was adapted to be $45 \text{ m}^3\text{h}^{-1}$ in both greenhouse dryers.



Fig. (1): Schematic diagram of the solar dryer



Fig. (2): Quonset shape greenhouse type solar dryer and traditional sun drying of mint

Samples preparation and experimental setup

Fresh mint was purchased from the local market in Ismailia, Egypt. Before drying, the foreign materials, as weeds, spoiled and discolored plants were removed. The initial moisture content of mint samples was determined by drying the mint samples (10 g, in duplicate) in an electric oven at 70 °C until reaching a constant weight as recommended by (AOAC, 1990). The average initial moisture content of fresh mint was found to be 85% w.b. Before the experiment, the mint samples were distributed uniformly on six trays with a dimension of 0.5×0.5 m. Each tray loaded by about 800 gm of fresh mint with distribution about 3.2 kgm⁻². The trays used in this study to easily record the weight losses of samples during drying. For traditional sun drying method, two trays with mint samples placed under the open sun (Fig. 2). The other four trays placed in the greenhouse dryers (two trays for each unit. Then, the remained area of the greenhouse dryers was loaded with mint samples

distributed uniformly over the surface of the perforated wire net of each dryer as shown in **Fig. (2)**. The density of mint samples was adapted to be the same as on the trays (3.2 kg m⁻²). The experimental work was run for 10 hours continuously through the period from 7 am to 5 pm, solar time. During the experimental work, an electrical digital balance (BS-Series, China) with an accuracy of 0.001 g was used to determine the mass of wet and dry samples to calculate moisture content. The weight of the samples was measured just before conducting the drying test and periodically (each hour) during the drying process (**Mwithiga and Olwal, 2005**).

Data accusation and measurements

The meteorological data included the solar radiation flux incident on a horizontal surface, wind speed and direction, air temperature and the air relative humidity were obtained from the meteorological station (Vantage Pro 2, Davis, USA) which was located beside the greenhouse dryers. The air temperature and relative humidity inside the dryer were measured periodically during the drying process. Relative humidity was measured using a digital thermo-hygrometer data logger (Prime Capsule/HT-165, Australia) with an accuracy of $(\pm 1\%)$. Air temperature inside the solar dryers was measured by k-type thermocouples. The thermocouples were connected to a data-logger system (Lab-Jack logger, USA) to display and record the data during the experimental work. The output data were recorded every ten minutes and averaged every hour. Three thermocouples were functioned to measure the indoor air temperature for each greenhouse. The inlet and outlet air temperatures were measured using four thermocouples. The velocity of drying air was measured using digital anemometer (MT- 4005, Korea) with measuring range up to 30 ms⁻¹ and accuracy of ± 0.1 ms⁻¹. The air flow rate was adapted to be $45 \text{ m}^3\text{h}^{-1}$ in both greenhouse dryers.

Mathematical modeling of drying curves

Mathematical modeling is essential to predict and simulate the drying behavior. It is also an important tool in dryer's design, contributing to a better understanding of the drying mechanism. The experimental drying data for mint were fitted to ten thin layer drying models listed in **Table** (1) by using nonlinear least squares regression solved by a Quasi-Newton numerical method. The moisture ratio (MR) in these models is defined as:

$$MR = \frac{M_t - M_e}{M_0 - M_e} \tag{1}$$

Where, M_t is moisture content at any time of drying (kg water/kg dry matter), M_e is the equilibrium moisture content (kg water/kg dry matter), and M_0 initial moisture content (kg water/kg dry matter). However, a simplified form of equation 1 for calculation the moisture ratio (in the form of MR=M_t/M₀) was considered in this study for mathematical modeling of the solar drying curves due to the continuous fluctuation of the relative humidity of the drying air during solar drying (**Kishk et al., 2019**). The coefficient of determination (R²), mean relative percent error (P) and root mean square error (RMSE) obtained for these equations were then used to compare the relative goodness of fit of experimental data. These parameters can be calculated as follows:

$$P = \frac{100}{N} \sum_{i=1}^{N} \frac{|MR_{exp,i} - MR_{pre,i}|}{MR_{exp,i}}$$
(2)
$$RMSE = \sqrt{\frac{1}{N} \sum_{i=1}^{N} (MR_{exp,i} - MR_{pre,i})^{2}}$$
(3)

where $MR_{exp,i}$ is the ith experimentally observed moisture ratio, $MR_{pre,i}$ is the ith predicted moisture ratio and N is the number of observations (**Kishk et al., 2019**). The best model describing the drying behavior of mint was chosen as the one with the highest value of R^2 and the lowest values of P and RMSE.

S.N.	Model	Model equation	References		
1	Newton	MR = exp(-kt)	Erbay and Icier (2010)		
2	Page	$MR = exp(-kt^n)$	Gürlek et al. (2009)		
3	Logarithmic	$MR = a \exp(-kt) + c$	Hacihafizoğlu et al. (2008)		
4	Two-term	$MR = a \exp(-k_0 t) + b \exp(-k_1 t)$	Corrêa et al., 2012		
5	Two-term exponential	$MR = a \exp(-kt) + (1 - a) \exp(-kat)$	Sharaf-Elden et al. (1980)		
6	Henderson and Pabis	$MR = a \ exp(-kt)$	Henderson and Pabis		

Table (1): Mathematical models widely used to describe the drying kinetics.

S.N.	Model	Model equation	References	
			(1961)	
7	Modified Henderson and Pabis	$MR = a \exp(-kt) + b \exp(-gt) + c$ $exp(-ht)$	Akpinar (2010)	
8	Wang and Singh	$MR = 1 + at + bt^2$	Wang and Singh (1978)	
9	Approximation of diffusion	$MR = a \exp(-kt) + (1-a) \exp(-kbt)$	Yaldız and Ertekin (2001)	
10	Verma et al.	$MR = a \exp(-kt) + (1-a) \exp(-gt)$	Verma et al. (1985)	

 Table (1): Mathematical models widely used to describe the drying kinetics.

Where a, b, c, and n are drying constants, k drying coefficient (h⁻¹) and t is the time (h)

RESULTS AND DISCUSSION

Weather conditions and temperature data

The weather conditions during open sun and solar drying of mint plant are shown in **Fig. (3)**. During the drying experiments, the temperature and the relative humidity of the ambient air ranged from 22 to 29°C and from 47 to 67%. The solar radiation ranged from 75 to 590 Wm⁻² and the wind speed from 0.21 to 0.92 ms⁻¹ as shown in **Fig. (3)**. As usual, the ambient air temperature and solar radiation reached the highest values between 11:00 AM and 1:00 PM, whereas the relative humidity reached the lowest values during the same period. **Fig. (3)** also show that the temperature values of drying air inside the greenhouse dryers operated by both continuous (CSD) and intervals (ISD) modes were almost the same. The temperature values ranged from 30 to 48°C. The interval mode showed fluctuation in the air temperature inside the greenhouse dryer. When the air fan closed (off mode 15 min) the temperature increased inside the greenhouse dryer.

Drying characteristics of mint

Fresh mint plant used in the drying experiment with initial moisture content of 85 ± 1 w.b. (5.8 Kg water /Kg dry matter). The variation in the weight of the product as a function of time was followed. The changes in the moisture contents per amount of the dry matter of mint with time are shown in **Fig. (4)**.



Fig. (3): Variations in air temperature, relative humidity and solar radiation during drying hours for a typical day in October 2018.



Fig. (4): Variation of moisture content with drying time of mint.

It is clear that the mint in the solar dryer operated under the continuous forced convection dried faster than the mint in the solar dryer operated under interval forced convection and open sun drying. For instance, after 10 hours of continuous drying for mint, the final moisture content of mint in the continuous solar dryer mode was 0.19 (kg water/kg dry matter). While the moisture content of the mint dried in the interval solar dryer and under the open sun was the same (about 0.50 kg water/kg dry matter). Although, the drying air temperature inside both drying units was the same, the continuous mode showed a higher drying rate. This may due to the fact that in the continuous mode the humid air inside the greenhouse dryer continuously left the dryer by the air fan and dry air entered from another side which resulted in higher drying rate. While in the intervals mode the interval time was not enough to carry out the humid air resulted from mint drying resulting in low drying rate in the greenhouse operated by the intervals mode.

The hourly drying rate of mint in the open sun, continuous and interval solar drying modes are presented in **Table (2)**. It is clear from **Table (2)** and Figure 4 that at all drying modes the drying of mint occurred in the falling rate period and no constant rate period was observed. Similar trend was reported by **Sallam et al. (2015)** for whole mint plant and by **Kadam et al. (2011)** and **Doymaz (2006)** for mint leaves. It can be also seen in Table 2 that the drying rate of mint was much higher in the continuous solar drying mode than the other drying modes in the first 5 hours of drying. After that, the drying rate of mint in the continuous mode became less than the other drying methods until the end of the drying period. This may due to that, in the continuous solar dryer the mint dried fast and become dray after 5 hours (0.98 kg water/kg dry matter) resulted in low drying rate at the end of the drying time. On the contrary, the mint in the interval solar drying mode and open sun drying was still at high moisture content (1.5 kg water/kg dry matter).

Mathematical modeling of drying curves

In order to normalize the drying curves, the data involving dry basis moisture content versus time were transformed into a dimensionless parameter called moisture ratio versus time (**Fig. 5**).

Drying	Sun	drying	ying Continues solar drying		Interval solar drying	
time, h	Moisture content	Drying rate	Moisture content	Drying rate	Moisture content	Drying rate
0	5.80	-	5.80	-	5.80	-
1	4.44	1.36	4.14	1.66	4.49	1.31
2	3.42	1.02	3.07	1.07	3.67	0.81
3	2.54	0.88	2.07	1.00	2.81	0.87
4	1.63	0.92	1.37	0.70	1.86	0.95
5	1.49	0.13	0.98	0.39	1.61	0.24
6	1.26	0.23	0.81	0.17	1.38	0.23
7	1.15	0.10	0.67	0.14	1.19	0.19
8	0.85	0.31	0.51	0.16	0.86	0.33
9	0.67	0.18	0.32	0.19	0.66	0.20
10	0.52	0.15	0.19	0.13	0.49	0.17

Table (2): Moisture contents (kg water/kg dry matter) and drying rates (kg water/kg dry matter.h) of mint at specific drying times according to solar and sun drying methods.



Fig. (5): Variation of moisture ratio with drying time of mint.

The moisture content data of continuous solar drying mode and the open sun drying of mint were converted to the most useful moisture ratio expression and then curve fitting computations with the drying time were carried on 10 different thin layer drying models presented in **Table (1)**.

The drying model coefficients and the comparison criteria used to evaluate the goodness of fit, namely the coefficient of determination (\mathbb{R}^2) , the mean relative percent error (P) and the root mean square error (RMSE) for solar drying of mint are tabulated in Table (3). It is clear from the statistical parameters shown in Table (3) that all tested models offered a good description of the experimental data with r^2 higher than 98% except Wang and Singh model. Similar results reported by Sallam et al. (2015). From Table (3), it can be concluded that the Modified Henderson and Pabis model gave the highest R² and lowest P and RMSE values than other models. Therefore, the Modified Henderson and Pabis model could adequately describe the solar drying behavior of mint in the greenhouse solar dryer and open sun drying. There is no universal model reported in the literature as the best drying model to explain thin layer drying behavior of mint under different drying methods. For instance, Sallam et al. (2015) found that the Verma et al. model was the best model described the natural and forced convection solar drying of whole mint plant for the direct and indirect drying. For mint leaves different models reported as the best models under specific drying methods such as Wang and Singh model for indirect forced convection solar drying and open sun (Akpinar, 2010), logarithmic model for heated air-drying (Doymaz, 2006) and two-term model for tunnel dryer (Kadam et al., 2011).

Modified Henderson and Pabis model for the open sun and solar drying of mint can be written based on the estimated constants and coefficients as below:

Original form:

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MR = a \exp(-kt) + b \exp(-gt) + c \exp(-ht)
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For open sun drying:

MR = -15880.9*exp(-0.2828*t) + 12853.3*exp(-0.2834*t) + 3028.7*exp(-0.2803*t)For solar drying:

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MR = 0.6048 * exp(-0.2414 * t) - 108.54 * exp(-1.523 * t) + 107.15 * exp(-1.499 * t)
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In which MR is the moisture ratio and t is the time (hr).

Fig. (6) illustrates the relationship between the experimental moisture ratio and the predicted values by Modified Henderson and Pabis model

for mint drying. Strictly speaking, Modified Henderson and Pabis model provided good conformity between experimental and predicted moisture ratios of mint during drying in both open sun and greenhouse solar dryer.

Model Drying Mode method		Model coefficients and constants	R ²	р	RMSE
Needen	Open Sun	k = 0.2691	0.9877	11.15	0.026
Newton	Solar drying	k = 0.3216	0.9883	12.61	0.024
Page	Open Sun	k =0.2997; n=0.9254	0.9880	07.11	0.023
-	Solar drying	k = 0.3159; n = 1.0136	0.9883	12.68	0.024
Logorithmia	Open Sun	a = 0.972; k = 0.331; c = 0.066	0.9916	07.25	0.019
Logarithmic	Solar drying	a = 1.0359; k = 0.3628; c = 0.0245	0.9899	15.51	0.022
	Open Sun	a = 0.3669; k0 = 0.1420; b = 0.7052; k1 = 0.4496	0.9922	06.25	0.019
Two-term	Solar drying	a = 1.0359; k0 = 0.3323; b = - 191731.18; k1 = 17.098	0.9889	12.68	0.023
Two-term	Open Sun	a = 0.4428; k = 0.4362	0.9902	06.81	0.021
exponential	Solar drying	a = 0.7420; k = 0.3484	0.9885	12.58	0.024
Henderson and	Open Sun	a =0.9650; k=0.2590	0.9863	09.70	0.025
Pabis	Solar drying	a =1.0257; k=0.0836	0.9889	12.65	0.023
Modified Henderson and	Open Sun		0.9962	06.15	0.018
Pabis	Solar drying	a = 0.6048; k = 0.2414; b = -108.54; g = 1.523; c = 107.15; h = 1.499	0.9972	11.57	0.016
Wang and	Open Sun	a = -0.2161; b = 0.0130	0.9708	19.39	0.043
Singh	Solar drying	a = -0.2360; b = 0.0146	0.9651	42.15	0.049
Approximation	Open Sun	a = 1.2364; k = 0.2691; b = 1.000	0.9877	11.15	0.026
of diffusion	Solar drying	a = 0.0083; k = 2.32E-6; b = 141696	0.9888	13.02	0.024
Vormo et el	Open Sun	a = 0.0745; k = 0.0283; g = 0.3137	0.9911	06.52	0.020
verma et al.	Solar drying	a = 1.0272; k = 0.3302; g = 3.310	0.9889	12.65	0.023

 Table (3): Modeling of moisture ratio according to the drying time for open sun and solar drying of mint.



Fig. (6): Relationship between the experimental moisture ratios and the predicted values by Modified Henderson and Pabis model for mint drying

CONCLUSION

In this study, greenhouse dryer used to dry mint plant and compared with the traditional sun drying method. Two greenhouse dryers were built and operated by two modes of forced convection (continuous and intervals). The performance of two modes compared with the open sun drying. The results showed that the drying rate values of mint in the continuous solar drying mode were much higher than the corresponding values of the drying rate of mint in the interval solar drying mode and open sun drying at especially at the first 5 hours of drying. After 10 hours of continuous drying for mint, the final moisture content of mint in the continuous solar dryer mode was 0.19 (kg water/kg dry matter). While the moisture content of the mint dried in the interval solar dryer and under the open sun was the same (about 0.50 kg water/kg dry matter). The drying data were fitted to ten thin layer drying models to explain the drying behavior of mint. The results showed that the Modified Henderson and Pabis model provided good conformity between experimental and predicted moisture ratios of mint during drying in both open sun and greenhouse solar dryer. The results of the study are very useful for commercial scale solar drying of mint and to optimize the drying process and to achieve a superior quality dried product.

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الملخص العربى دراسة تجريبية و نمذجه رياضيه لتجفيف النعناع بالطاقة الشمسية

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أجري هذا البحث بقسم الهندسة الزراعية - كلية الزراعة - جامعة قناة السويس الإسماعيلية، مصر (خط عرض ٥٣٠،٦٢، خط طول ٣٢،٢٧ وارتفاع ٥ متر عن سطح البحر) خلال شهر أكتوبر ٢٠١٨ ويهدف البحث إلي دراسة تأثير نظم تشغيل مختلفة (مستمر و متقطع) على أداء البيوت المحمية المستخدمة كمجففات شمسية والتي تم مقارنتها بالتجفيف الشمسي التقليدي وذلك لتجفيف محصول النعناع. إستخدمت للتجارب صوبتين متماثلتين على شكل نصف اسطواني بمساحة ارضية ٢ م^٢ وتم تغطيتها بطبقة واحدة من البولي ايثيلين.

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تم توجيه المجففات فى إتجاه شرق – غرب (المحور الطولى فى إتجاه الجنوب) وتم توصيل كل مجفف بمروحة طردة مركزية بقدرة ١٠٥٠ حصان مزودة بجهاز تغير سرعات للتحكم فى سرعة تصرف الهواء المطلوبة. فى الجانب المقابل للمروحة يوجد شباك لدخول الهواء حيث يدخل الهواء للصوبة من أعلى ليتم تسخينة بواسطة الطاقة الشمسية و يتم سحبة من أسفل المحصول بواسطة المروحة، تم إستخدام معدل تصرف للمروحة ٤٥ م⁷/ ساعة للتشغيل المستمر و فى التشغيل المتقطع يتم تشغيل المروحة ١٥ دقيقة ثم غلقها ١٥ دقيقة أخرى بواسطة التايمر. تم قياس شدة الإشعاع الشمسى و درجة الحرارة الداخلية و الخارجية و كذلك الرطوبة النسبية داخل و خارج المجفف كذلك تم اختبار ١٠ نماذج رياضية مختلفه لاختيار النموذج الافضل لوصف عملية التجفيف الشمسى للنعناع.

وقد أوضحت النتائج مايلى:

أن معدل تجفيف النعناع فى الصوبه تحت التشغيل المستمر أعلى من معدل تجفيف النعناع فى الصوبه تحت التشغيل المتقطع وكذلك التجفيف الشمسى العادى. حيث أنه بعد ١٠ ساعات من التجفيف المتواصل للنعناع ذو المحتوى الرطوبى الإبتدائى ٥،٩ (كجم ماء/كجم مادة صلبه) وصل المحتوى الرطوبى الرطوبى الإبتدائى ٥،٩ (كجم ماء/كجم مادة صلبه) وصل المحتوى الرطوبى التشغيل المتقطع و فى التجفيف الشمسى العادى . ماء/كجم مادة صلبه) ماء/كجم مادة صلبه) ماء/كجم مادة صلبه) ماء ركجم مادة صلبه) ماء ركجم مادة صلبه) ماء ركجم مادة صلبه) وصل المحتوى الرطوبى الإبتدائى ٥،٩ (كجم ماء/كجم مادة صلبه) ماء/كجم مادة صلبه) ومن المحتوى الرطوبى التشغيل المتقطع و فى التجفيف الشمسى العادى . ماء ماء ماء (كجم مادة صلبه) ماء/كجم مادة صلبه) وفى الصوبه تحت التشغيل المتقطع و فى التجفيف الشمسى العادى الى ٥،٠ (كجم مادة صلبه). وبصورة عامة أعطى المجفف الشمسى بنظام التشغيل المستمر عند معدل تصرف للهواء ٤٥ م⁷/ساعة أفضل النتائج من حيث معدل وزمن التجفيف. كذلك أعطى نموذج هندرسون وبابيس المعدل (model Modified Henderson and Pabis) ماء كذلك أعطى نموذج هندرسون وبابيس المعدل (model Modified التشغيل عامل إلى المتان التخليف.